

**FLUXGATE MAGNETOMETER  
CALIBRATION  
FOR  
  
BEPICOLOMBO  
  
BC-MAG-TR-0085**

**Issue: 1      Revision: 3**

**May 06, 2013**

**Protocol and Analysis of the  
BepiColombo MPO Calibration for  
Sensor BS\_10 & BS\_11  
  
connected to the FM\_1 Electronics**

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## 1 Introduction

This document describes the ground calibration of the BepiColombo MPO-FM1 magnetometer using the Sensors BS\_10 & BS\_11. The calibration was conducted at the Magnetsrode Calibration facility operated by the Institute for Geophysics and extraterrestrial Physics, TU Braunschweig. The tests were executed from April 02 - April 11, 2013.

### Part Identification:

Sensor:	BS_10 (connected to J02, IB)
	BS_11 (connected to J01, OB)
Electronics	MPO FM1

### Key Personnel:

Karl-Heinz Fornaçon:	operating FGM
Ingo Richter:	operating MRode Facility

### General Setup

- Sensor mounted in thermal box. CoC. Box vertical.
- Sensor is operated with thick MPO hat installed
- FM1 Electronics placed in House 2 / Mainroom.
- The EGSE Laptop placed in House 2 / Anteroom.
- The Spacewire Brick placed in House 2 / Anteroom.
- The FM1 Electronics was powered by the Thurlby Power Supply in House 1.  
Voltage: +28V / Current: +0.163A
- DUT parameters Sensor BS\_10:  
Phase: 146  
K1X: 24927  
K1Y: 14331  
K1Z: 56105  
KF: 102  
Relais: on , Excitation: on

- DUT parameters Sensor BS\_11:  
 Phase: 146  
 K1X: 40402  
 K1Y: 22671  
 K1Z: 55926  
 KF: 102  
 Relais: on , Excitation: on
- Position 1: Standard Alignment  
 $X_m = X_c, Y_m = Y_c, Z_m = Z_c$   
 Elevation= 0°. Azimuth= 180°.
- Position 2: Turned Position for XY Offset Measurements  
 $X_m = -X_c, Y_m = -Y_c, Z_m = Z_c$   
 Elevation= 0°. Azimuth= 0°.
- Position 3: Normal Position for Z Offset Measurements  
 $X_m = -Z_c, Y_m = -Y_c, Z_m = -X_c$   
 Elevation=90°. Azimuth= 0°.
- Position 4: Turned Position for Z Offset Measurements  
 $X_m = -Z_c, Y_m = Y_c, Z_m = X_c$   
 Elevation=90°. Azimuth= 180°.
- The sensor pictures were taken before rotating the box to the vertical orientation.
- TEMPCTRL-Parameters for Heating:  
 Field-Active-Time: 25s  
 SOL controlled, Delay after SOL: 8s  
 Max. Heating Time: 20s  
 Heating-Profile: *manual*  
 Heater-Select: automatic  
 Smart\_heat: off
- TEMPCTRL-Parameters for Cooling:  
 Field-Active-Time: 25s  
 SOL controlled, Delay after SOL: 8s  
 Max. Heating Time: 25s  
 Max. Cooling Time: 7s  
 Heating-Profile: *manual*  
 Heater-Select: *automatic*  
 Smart\_heat: *on*
- IP-Adressses:  
 FM1-EGSE: 192.168.124.37  
 MRode-Terminal: 192.168.124.50

REMARKS:

- The Analysis has been performed using a nominal conversion factor of 1 nT/V (nT/ADCcounts).
- The magnetometer was operated always in 2048 nT range with a sampling rate of 128 vectors per second if not stated different.
- **All values (e.g Offsets) given in engineering nanotesla (enT) have to be multiplied with the calculated sensitivities to obtain real nanotesla values.**
- The X-sensor shows non-linearities at fields of  $\pm 2000$  nT. Therefore, only values up to  $\pm 1900$  nT were used for the analysis.
- In open loop mode the X-sensor shows non-linearities at fields of  $\pm 1300$  nT. Therefore, only values up to  $\pm 1300$  nT were used for the analysis.
- In open loop mode the Y-sensor shows non-linearities at fields of  $\pm 1100$  nT. Therefore, only values up to  $\pm 1100$  nT were used for the analysis.
- In open loop mode the Z-sensor shows non-linearities at fields of  $\pm 1700$  nT. Therefore, only values up to  $\pm 1700$  nT were used for the analysis.
- All TEMB frames contain the MPO temperatures in the first three channels:

TEMB-CH0: $T_{\text{ELEC-IB}}$
TEMB-CH1: $T_{\text{IB-1}}$ – Sensor Temperature
TEMB-CH2: $T_{\text{IB-2}}$ – Sensor Temperature
TEMB-CH3: $T_{\text{ELEC-OB}}$
TEMB-CH4: $T_{\text{OB-1}}$ – Sensor Temperature
TEMB-CH5: $T_{\text{OB-2}}$ – Sensor Temperature

- MRode-Terminal software:  
*TERMINAL\_16.vi* using *MPO/EXTRACT\_MPO\_HK\_PACKETS.vi*

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Figure 1: FM1 Electronics in H2, Mainroom

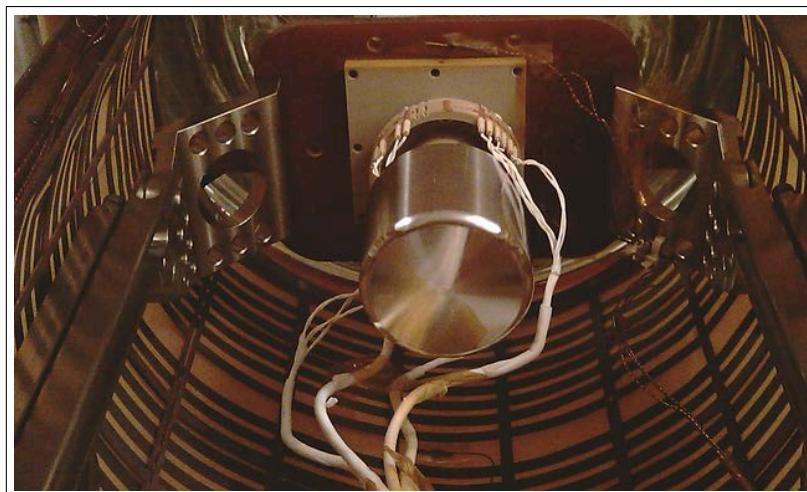


Figure 2: Sensor in Standard Position, POSITION 1, View from South



Figure 3: Sensor in Standard Position, POSITION 1, View from Top

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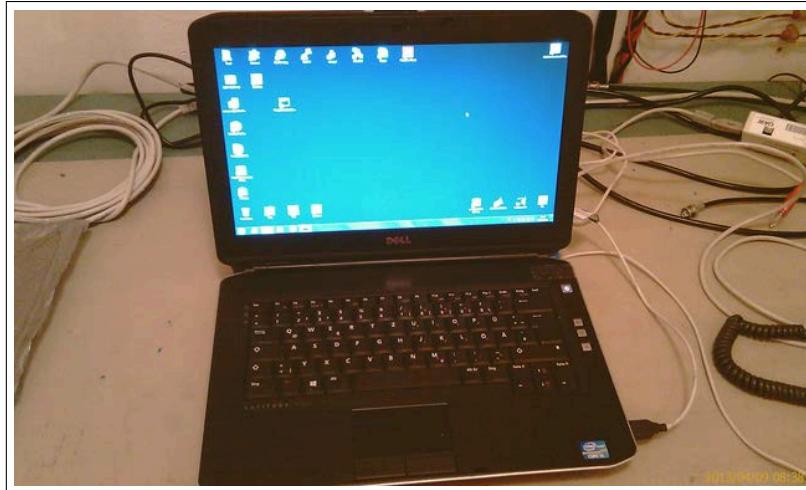


Figure 4: EGSE Laptop in H2, Anteroom

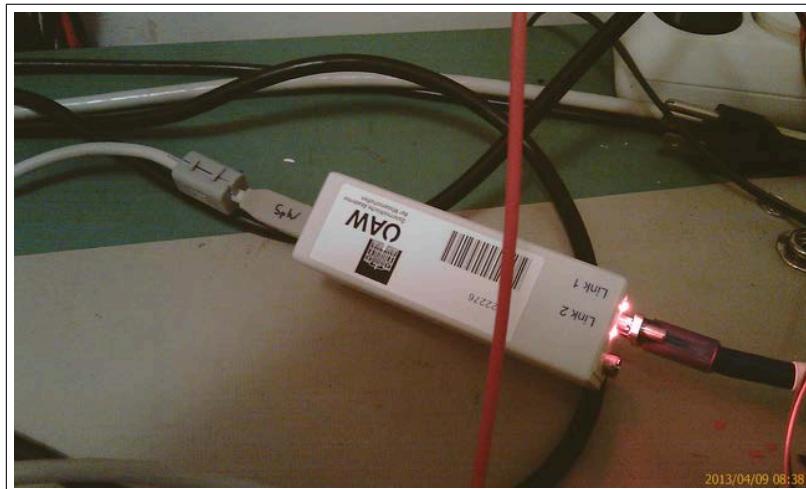


Figure 5: FM1 Brick in H2, Anteroom

## 2 Measurements on April 2, 2013

The FM1 Magnetometer was installed in House 2. Sensor BS\_11 was placed at CoC in the thermal box. Sensor BS\_10 was placed south of the coilsystem inside a small  $\mu$ -Metal can.

Due to lack of time and a needed quick setup the sensor was operated by EGSE control only. No data were stored at the MRode CDRS. The magnetometer was operated in dynamical compensated zerofield conditions.

Over night the sensor measured in normal science mode, 4 Hz sampling rate, 2048 nT range, room temperature, measurements started at about 12:30.

## 3 Measurements on April 3, 2013

The measurement over night was performed without any problem.

### 3.1 Coilsystem Residual Field Check



Figure 6: Overhauser Magnetometer Sensor in Diagonal in Space Orientation, CoC, View from South-West

Prior to the real MPO calibration the residual field of the MCF has been checked using the Overhauser magnetometer. The OVH was placed diagonal in space at CoC. Fields of  $\pm 49000$  nT were applied sequentially to each axis in order to determine the actual residual field:

Component	Applied Field	Measured Modulus	Calc. Residual
$X_c$	+49000 nT	49002 nT	-2.5 nT
	-49000 nT	49007 nT	
$Y_c$	+49000 nT	49002 nT	-1 nT
	-49000 nT	49004 nT	
$Z_c$	+49000 nT	48960 nT	-40 nT
	-49000 nT	49040 nT	

After these initial measurements the residual field was nulled with the offset potentiometers at the Power Amplifiers.

Component	Applied Field	Measured Modulus	Calc. Residual
$X_c$	+49000 nT	49005 nT	0 nT
	-49000 nT	49005 nT	
$Y_c$	+49000 nT	49003 nT	0 nT
	-49000 nT	49003 nT	
$Z_c$	+49000 nT	48993 nT	-7 nT
	-49000 nT	49007 nT	

The z-component could not be nulled exactly, as the offset controlling potentiometer of the Zc-PA reached the limit of its rotation range.

After the removal of the Overhauser magnetometer and shifting the thermal box, with sensor BS\_11 installed, to the default CoC position, the setup was finished.

### 3.2 Calibration Initialisation

Initial reading of the thermistors:

$T_{59}$	=	17.3°C
$T_{ELEC-IB}$	=	26.5°C
$T_{IB-1}$	=	15.7°C
$T_{IB-2}$	=	16.7°C
$T_{ELEC-OB}$	=	27.35°C
$T_{OB-1}$	=	19.9°C
$T_{OB-2}$	=	20.1°C

A first test of the BS\_11 Sensor revealed the correct soldering of the components.

Application of 1000 nT fields in all main axes in Standard orientation yielded (in the default position 1):

$X_m$	=	$X_c$
$Y_m$	=	$Y_c$
$Z_m$	=	$Z_c$

### 3.3 Data

CCD File	Configuration File	Remark
13-04-03\09-22-38.CCR	LIN2000XYZE.MAG	
13-04-03\09-53-35.CCR	OFFSET_200.MAG	
13-04-03\10-07-54.CCR	LIN2000XYZE.MAG	
13-04-03\10-15-00.CCR	LIN2000XYZE.MAG	
13-04-03\10-45-19.CCR	LIN2000XYZE.MAG	
13-04-03\11-15-38.CCR	LIN2000XYZE.MAG	
13-04-03\11-45-56.CCR	LIN2000XYZE.MAG	
13-04-03\12-16-15.CCR	LIN2000XYZE.MAG	
13-04-03\12-47-57.CCR	OFFSET_200.MAG	
13-04-03\12-59-48.CCR	FREQ2000.MAG	
13-04-03\13-45-53.CCR	FREQ2000.MAG	
13-04-03\14-41-31.CCR	FREQ2000.MAG	
13-04-03\15-24-42.CCR	LIN2000XYZE.MAG	
13-04-03\15-55-48.CCR	OFFSET_200.MAG	
13-04-03\16-08-54.CCR	NULL_LANG.MAG	

### 3.4 DC-Analysis at Room Temperature - OB Sensor, Science mode 0

A standard linearity and offset measurement was performed at 17.3°C.

#### 3.4.1 Calibration on 3 Linear Axes

##### Used Files:

CCD File	Configuration File	Remark
13-04-03\09-22-38.CCR	LIN2000XYZE.MAG	

Parameter File: PARAMETER\_LIN\_\_13-04-03\_09-22-38.CPF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Sensor Rotation:

$$\underline{\underline{\rho}} = \begin{pmatrix} +0.999800 & +0.018895 & +0.006519 \\ -0.018810 & +0.999740 & -0.012858 \\ -0.006760 & +0.012733 & +0.999896 \end{pmatrix}$$

Rotation Angles:

$$\begin{aligned} \text{Angle } (X_c, X_m): \quad \lambda_x &= +1^\circ 8'43'' \\ \text{Angle } (Y_c, Y_m): \quad \mu_y &= +1^\circ 18'20'' \\ \text{Angle } (Z_c, Z_m): \quad \nu_z &= +0^\circ 49'34'' \end{aligned}$$

Determinant of Rotation Matrix: 1.00000

Nominal Field Source: FLDS

Fields applied for 24.0 s

Mean Sensor Temperature: 17.2°C

Automatic Coil Correction: used

Earthfield Compensation: X = DYNAMIC  
Y = DYNAMIC  
Z = DYNAMIC

## Offset Treatment:

A polynomial offset trend of order 2 has been fitted and subtracted from the raw data before creating the sensor model.

Mean Coil System Residual + Sensor Offset:  $\underline{B}^{or} = (-0.208, -0.272, -10.561)$  nT

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## Raw Data Quality:

Standard Deviation of used Raw Data Blocks:

[Values in eng nT]	$s_x$	$s_y$	$s_z$
Minimum	0.000	0.342	0.316
Mean	2.383	0.407	0.676
Maximum	3.318	1.087	0.892

## Calibration Parameter:

$$\text{Transfermatrix: } \underline{\underline{\phi}} = \underline{\underline{R}}_{\text{nom}} \underline{\underline{\omega}} \underline{\underline{\sigma}} = \begin{pmatrix} +0.972083 & +0.018824 & +0.006445 \\ -0.021899 & +0.995935 & -0.012713 \\ -0.005695 & +0.012883 & +0.988644 \end{pmatrix}$$

$$\text{Reduced Transfermatrix: } \tilde{\underline{\underline{\phi}}} = \underline{\underline{\omega}} \underline{\underline{\sigma}} = \begin{pmatrix} +0.972339 & +0.000000 & +0.000000 \\ -0.003598 & +0.996196 & +0.000000 \\ +0.000923 & +0.000198 & +0.988747 \end{pmatrix}$$

$$\text{Sensitivity: } \underline{\underline{\sigma}} = \begin{pmatrix} +0.972339 & +0.000000 & +0.000000 \\ +0.000000 & +0.996189 & +0.000000 \\ +0.000000 & +0.000000 & +0.988747 \end{pmatrix}$$

$$\text{Misalignment: } \underline{\underline{\omega}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ -0.003701 & +1.000007 & +0.000000 \\ +0.000950 & +0.000199 & +1.000000 \end{pmatrix}$$

Sensor Misalignment Angles:

$$\begin{aligned} \xi_{x,y} &= +89^\circ 47'17'' \\ \xi_{x,z} &= +90^\circ 3'16'' \\ \xi_{y,z} &= +90^\circ 0'42'' \end{aligned}$$

## Model Quality:

Standard Deviation, Maximum and Minimum Error of Calculated Model:

[Values in nT]	$X$	$Y$	$Z$
Standard Deviation	0.051	0.068	0.067
Maximum Error	0.121	0.120	0.176
Minimum Error	-0.124	-0.183	-0.147

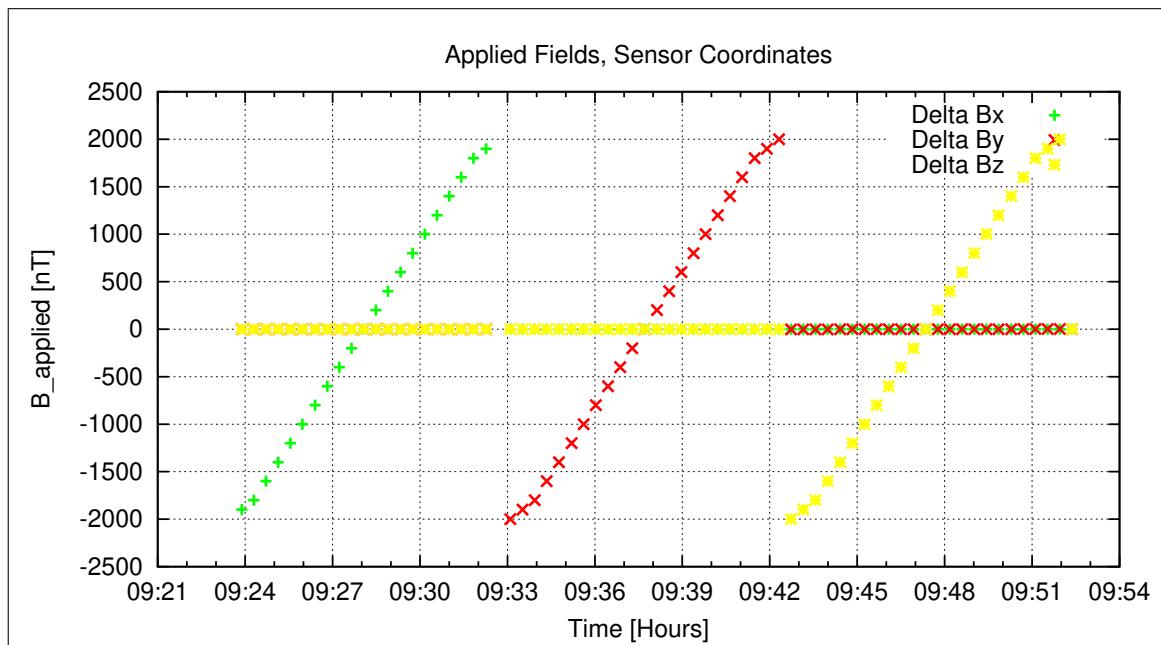


Figure 7: Applied Fields

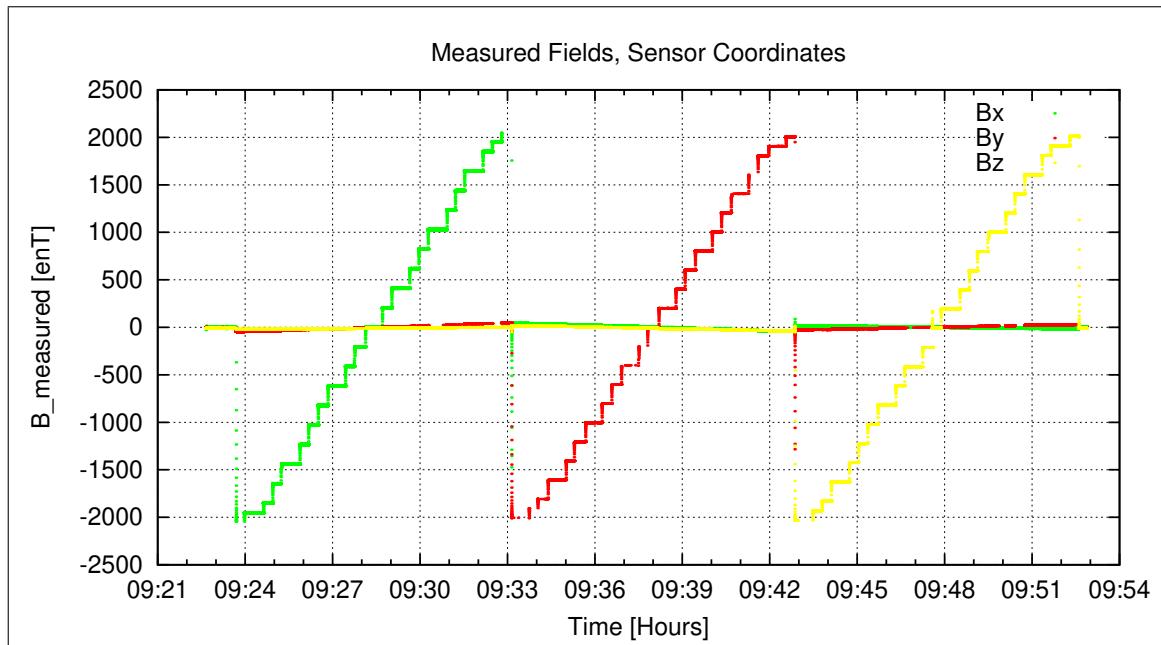


Figure 8: Measured Data

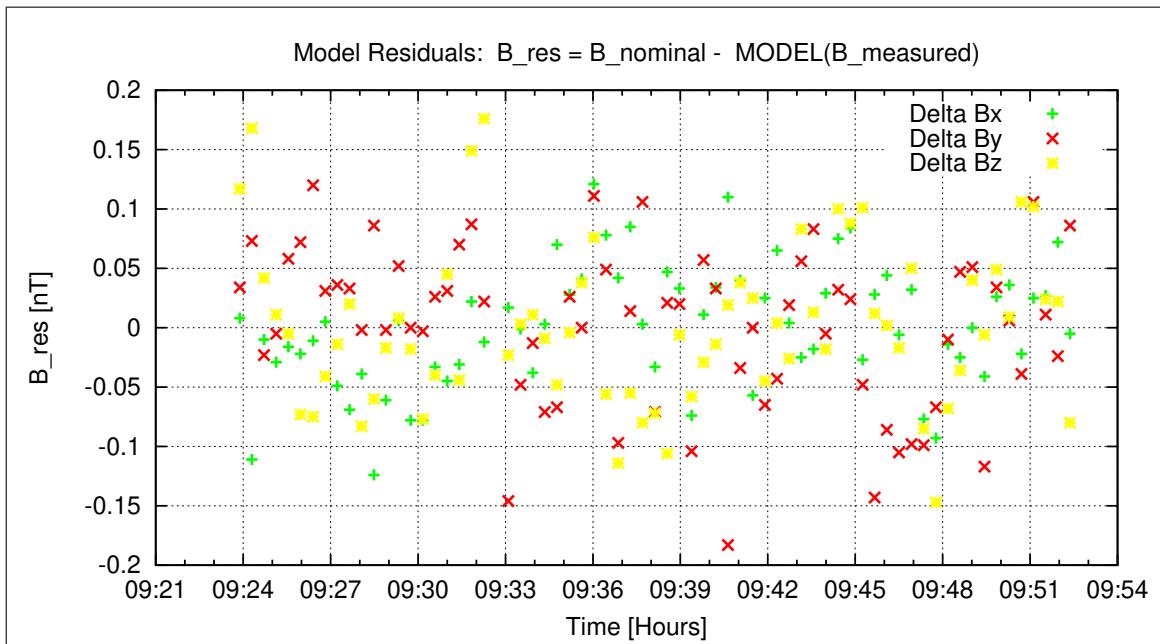


Figure 9: Model Quality - Differences of applied field and modelled measurement data

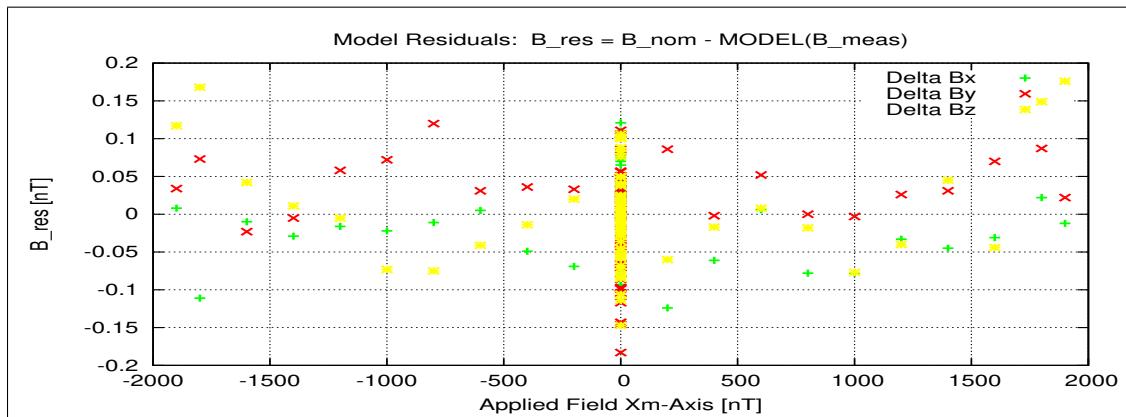


Figure 10: RESIDUALS vs FLD X

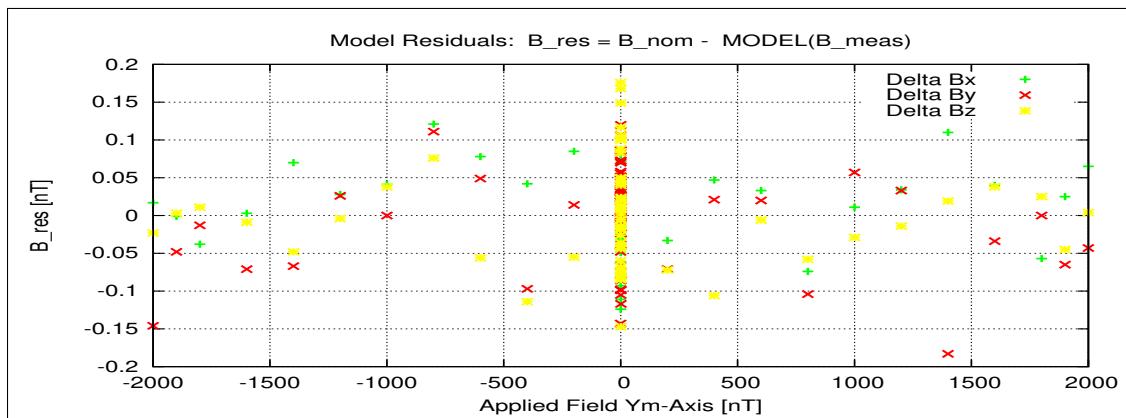


Figure 11: RESIDUALS vs FLD Y

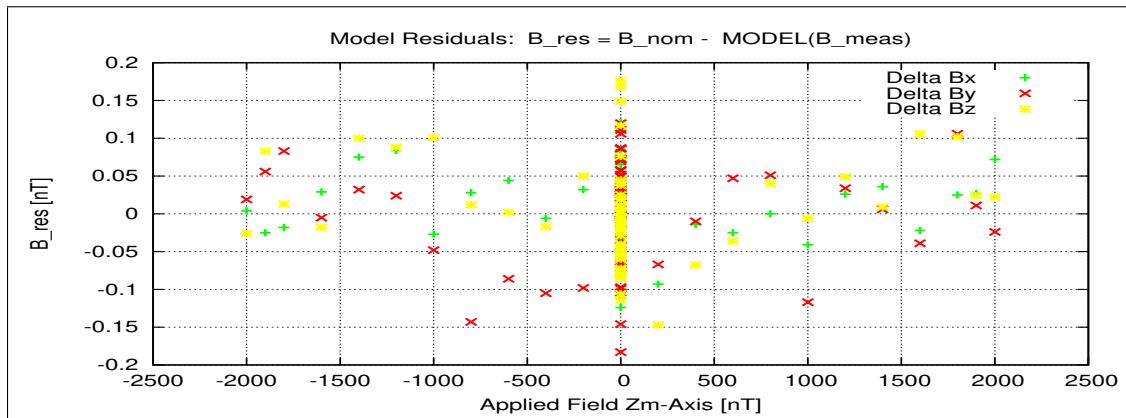


Figure 12: RESIDUALS vs FLD Z

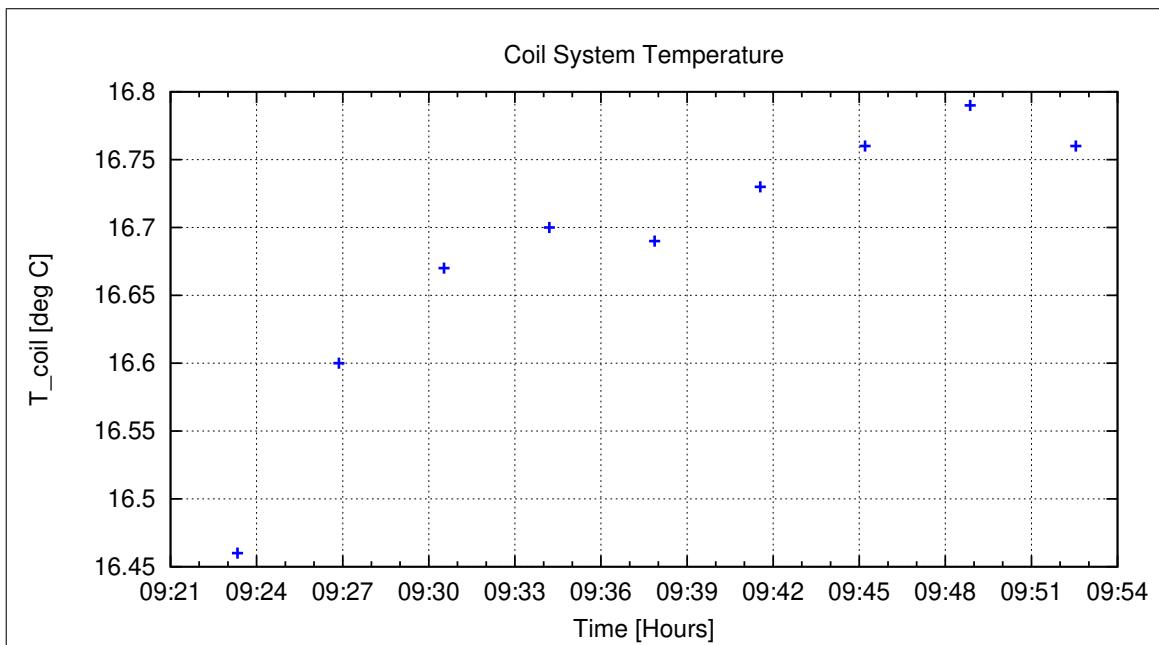


Figure 13: Coil System Temperature

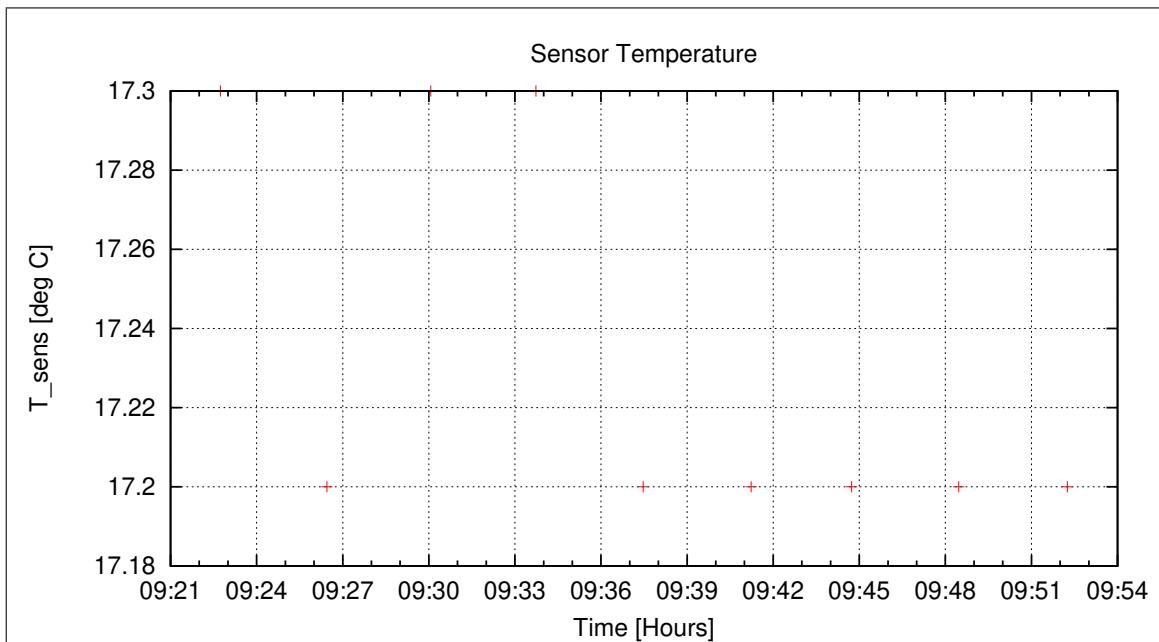


Figure 14: Sensor Temperature

### 3.4.2 OFFSET Calculation

In this section the instrument offsets and the residual field of the Coil System will be evaluated. Measurements at two orientations for each component act as input for the offset calculation. From the "normal" (0-degrees) and "turned" (180-degrees) orientations the offsets and residual fields can be derived:

$$\begin{aligned} B_{\text{off}} &= \frac{B_{\text{normal}} + B_{\text{turned}}}{2} \\ B_{\text{res}} &= \frac{B_{\text{normal}} - B_{\text{turned}}}{2} \end{aligned}$$

#### Used Offset Measurements:

CCD File	Configuration File	Remark
13-04-03\09-53-35.CCR	OFFSET_200.MAG	

Parameter File: OFF\_PARAMETER\_\_13-04-03-09-53-35.OPF

**Calibration Parameter:**

Sensor Offsets:	Component	Offset [enT]	Standard deviation [enT]
	X	0.10	0.097
	Y	-0.14	0.091
	Z	0.65	0.081

Residual Field of the Coil System:	Component	$B_{\text{res}}$ [enT]
	X	-0.44
	Y	0.17
	Z	0.66

Remark: Residual field is given in actual DUT coordinates, not in coil-coordinates!

Afterwards the thermal system was started and the box was cooled down to -70°C starting at 10:15. The initial pressure of the N<sub>2</sub>-bottle was 85 bar, 35 kg of LN<sub>2</sub> were available.

### **3.5 DC-Analysis at very low Temperature - OB Sensor**

Linearity and offset measurements were performed at  $T_{59} = -71^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

### 3.6 AC-Analysis at very low Temperature - OB Sensor, Science mode 0

A frequency measurement was performed at -70°C.

#### Setup:

- Sensor mounted in thermal box. CoC. Box vertical.
- Sensor rotated to:  
Elevation= 45°  
Azimuth= 126°
- Field applied on  $Y_c$ .
- No attenuator

#### 3.6.1 Frequency Measurements

This section is dedicated to the frequency behavior of the instrument. The analysis of the performed AC measurements allows to calculate the actual sampling frequency  $f_s$  of the instrument and the frequency response (amplitude vs. frequency). The measurements have been performed with the sensor placed at CoC in a diagonal in space orientation. The AC-fields have been applied on the  $Y_c$  axis only. Using this setup it can be guaranteed that only one frequency is applied at a time and no beat effects occur.

#### Used Frequency Measurements:

CCD File	Configuration File	Remark
13-04-03\12-59-48.CCR	FREQ2000.MAG	

Parameter File: FREQ\_PARAMETER\_\_13-04-03-12-59-48.FPF

**Calibration Parameter:**Sampling Frequency:

Component	$f_s$ [Hz]	Standard deviation [Hz]
X	127.9989	0.000066
Y	127.9988	0.000058
Z	127.9990	0.000056
Mean Sampling Frequency	127.9989	0.000138

3 dB Corner Frequency:

Component	$f_{3\text{dB}}$ [Hz]
X	64.59
Y	64.02
Z	55.45

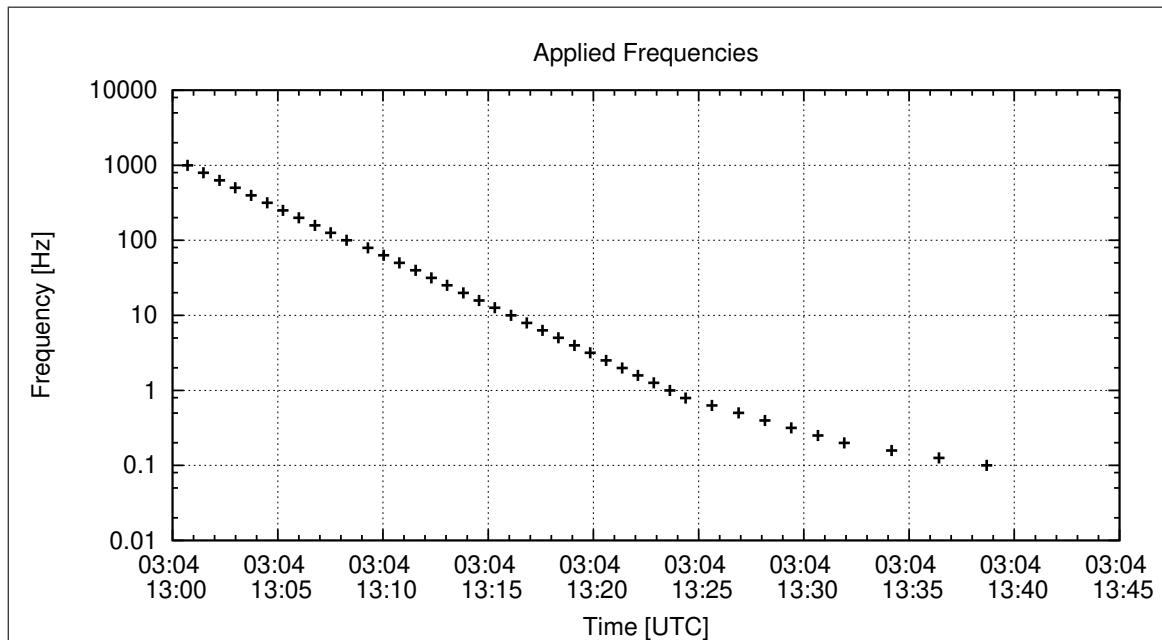
Applied Frequencies and Measured Amplitudes

Figure 15: Applied Frequencies for AC Analysis

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Applied Frequency [Hz]	Bx [enT]	By [enT]	Bz [enT]
1000.000	1.93	1.77	0.69
794.000	10.30	9.61	4.11
631.000	15.74	14.81	6.97
501.000	23.35	22.14	11.64
398.000	18.89	18.03	10.37
316.000	37.04	35.01	21.00
251.000	46.26	44.23	29.94
199.000	105.65	100.40	71.59
158.000	54.24	52.31	43.02
126.000	61.87	59.36	49.76
100.000	148.72	144.04	133.77
79.400	340.65	326.34	298.36
63.100	442.44	422.76	387.03
50.100	514.93	494.05	471.04
39.800	561.95	541.63	541.95
31.600	589.20	569.67	588.78
25.100	603.14	583.57	610.07
19.900	609.00	588.76	613.88
15.800	609.33	588.29	608.45
12.600	610.46	588.61	603.77
10.000	608.93	586.51	597.48
7.900	607.11	584.29	592.19
6.310	608.06	584.89	590.83
5.010	606.56	583.25	587.84
3.980	606.81	583.34	587.07
3.160	607.81	584.21	587.37
2.510	606.75	583.14	585.94
1.990	606.46	582.83	585.40
1.580	608.15	584.44	586.87
1.260	607.69	583.97	586.31
1.000	608.11	584.37	586.64
0.790	607.53	583.80	586.04
0.631	608.56	584.78	587.01
0.501	608.41	584.63	586.85
0.398	608.01	584.25	586.42
0.316	608.20	584.43	586.58
0.251	608.72	584.93	587.11
0.199	608.78	584.98	587.16
0.158	609.30	585.49	587.62
0.126	608.88	585.04	587.21
0.100	609.90	586.07	588.19

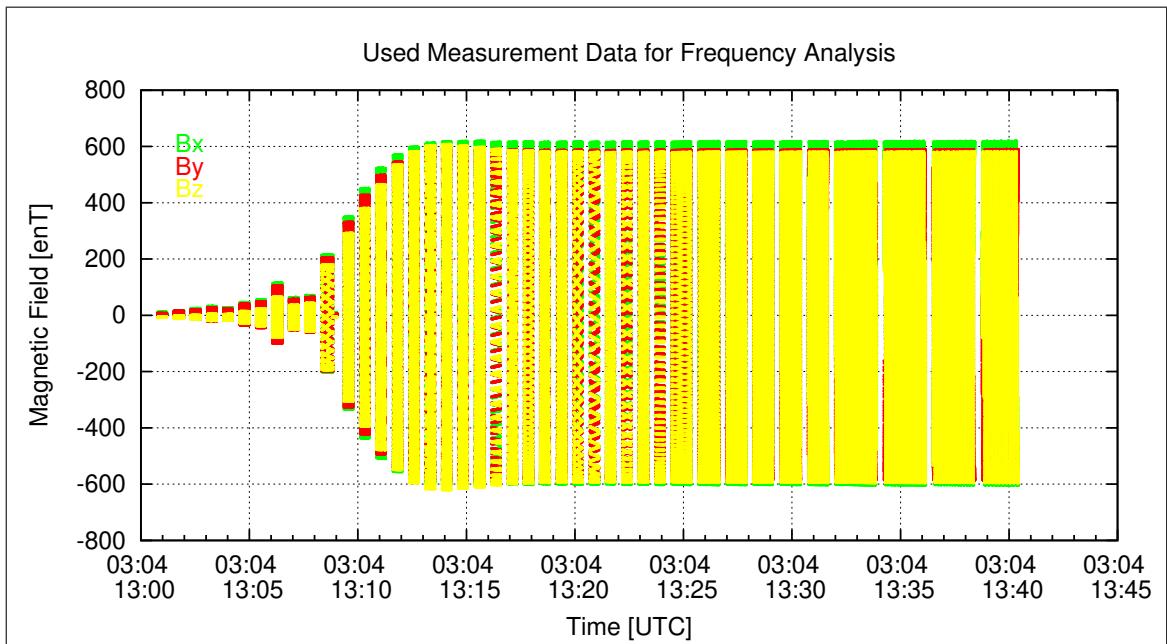


Figure 16: Used packets of Measured data for the Frequency analysis

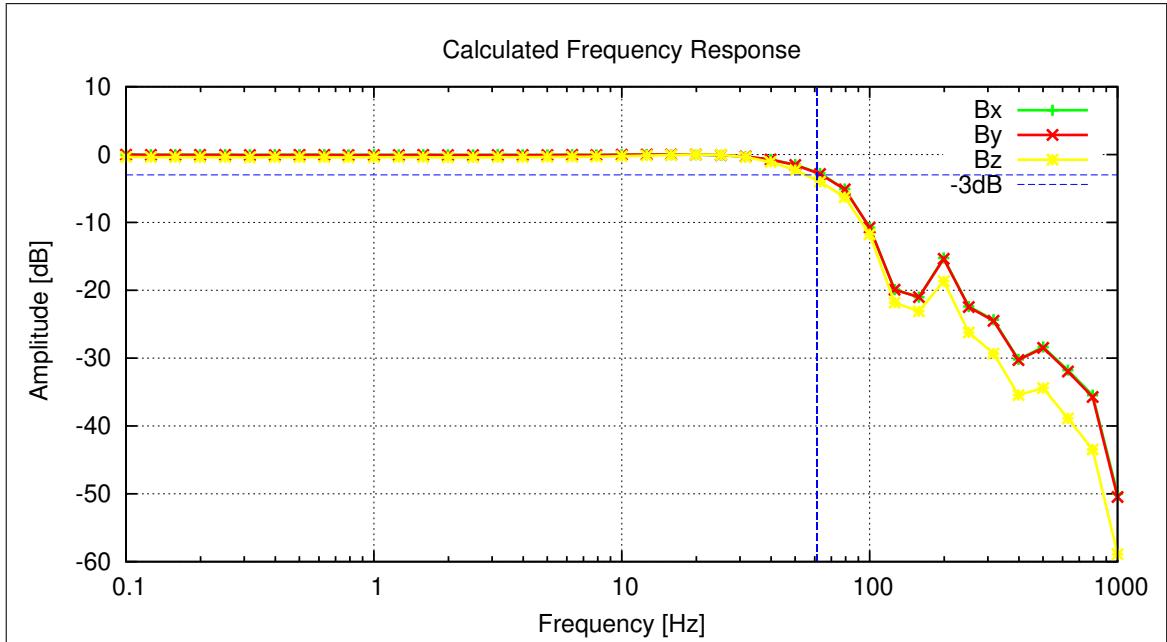


Figure 17: Calculated Frequency Response

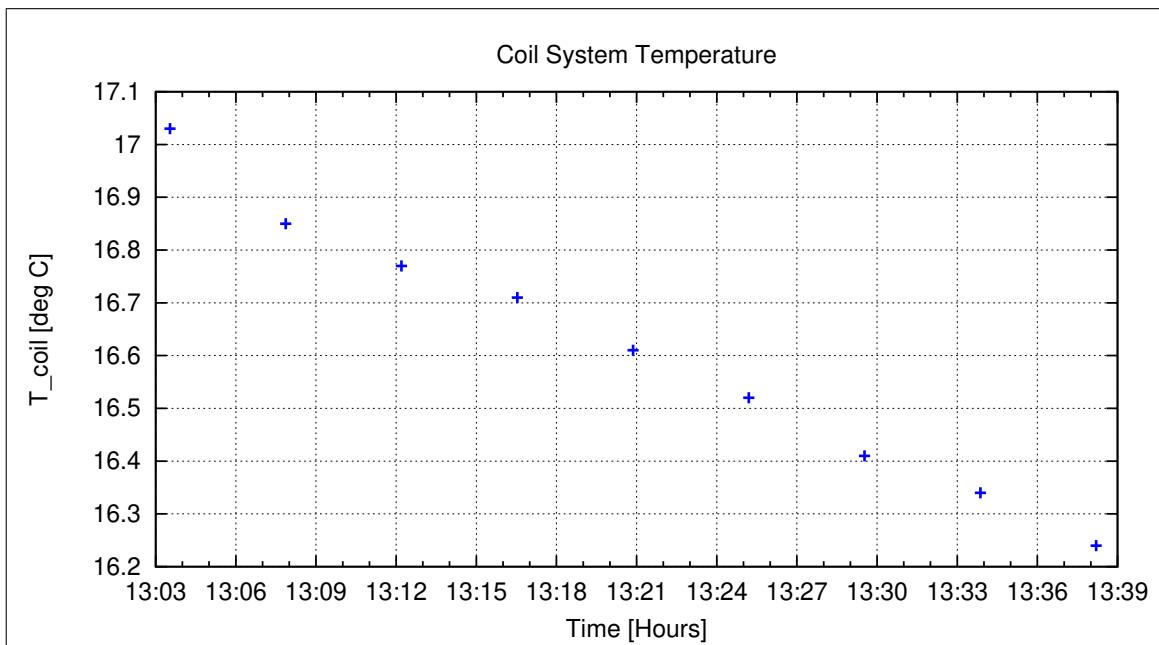


Figure 18: Coil System Temperature

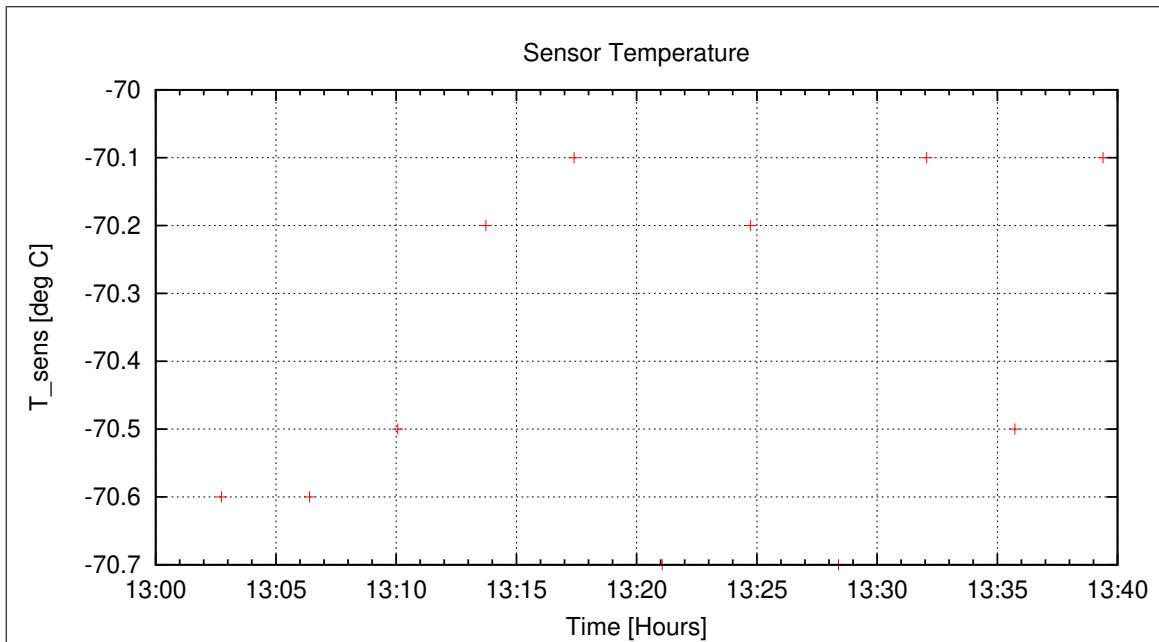


Figure 19: Sensor Temperature

### 3.7 AC-Analysis at very low Temperature - OB Sensor, Cal mode 4, open loop

A frequency measurement was performed at -70°C.

#### Setup:

- Sensor mounted in thermal box. CoC. Box vertical.
- Sensor rotated to:  
Elevation= 45°  
Azimuth= 126°
- Field applied on  $Y_c$ .
- No attenuator

#### 3.7.1 Frequency Measurements

This section is dedicated to the frequency behavior of the instrument. The analysis of the performed AC measurements allows to calculate the actual sampling frequency  $f_s$  of the instrument and the frequency response (amplitude vs. frequency). The measurements have been performed with the sensor placed at CoC in a diagonal in space orientation. The AC-fields have been applied on the  $Y_c$  axis only. Using this setup it can be guaranteed that only one frequency is applied at a time and no beat effects occur.

#### Used Frequency Measurements:

CCD File	Configuration File	Remark
13-04-03\14-41-31.CCR	FREQ2000.MAG	

Parameter File: FREQ\_PARAMETER\_\_13-04-03-14-41-31.FPF

**Calibration Parameter:**Sampling Frequency:

Component	$f_s$ [Hz]	Standard deviation [Hz]
X	127.9989	0.000019
Y	127.9990	0.001444
Z	127.9988	0.000024
Mean Sampling Frequency	127.9989	0.000103

3 dB Corner Frequency:

Component	$f_{3\text{dB}}$ [Hz]
X	58.34
Y	58.29
Z	54.47

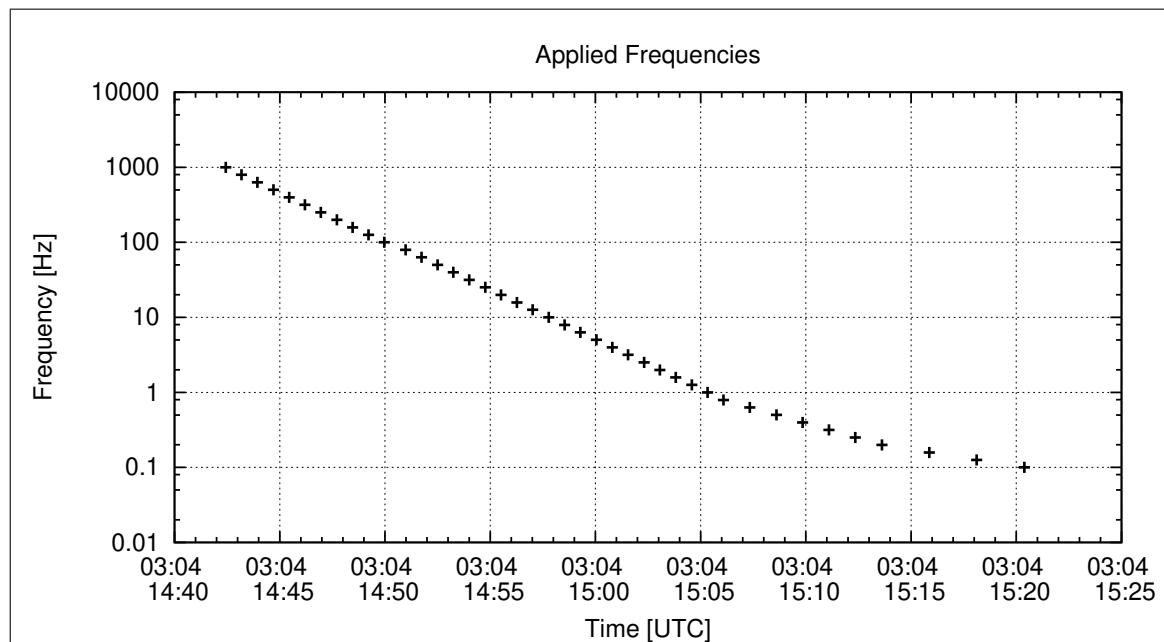
Applied Frequencies and Measured Amplitudes

Figure 20: Applied Frequencies for AC Analysis

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Applied Frequency [Hz]	Bx [enT]	By [enT]	Bz [enT]
1000.000	1.94	1.77	0.66
794.000	10.33	9.59	4.04
631.000	16.53	15.50	7.29
501.000	24.24	22.84	11.94
398.000	19.51	18.53	10.63
316.000	36.05	34.35	21.58
251.000	46.83	44.84	30.68
199.000	102.85	98.44	73.06
158.000	50.73	48.85	39.72
126.000	65.18	62.56	53.23
100.000	152.32	146.33	131.15
79.400	110.79	106.08	99.16
63.100	430.62	414.14	397.73
50.100	501.72	482.62	472.95
39.800	478.17	461.86	481.30
31.600	363.37	349.57	350.24
25.100	604.13	581.36	585.98
19.900	563.38	542.37	548.66
15.800	624.38	600.89	609.36
12.600	632.59	608.80	618.30
10.000	634.45	610.58	620.71
7.900	636.31	612.41	622.95
6.310	549.54	528.85	538.13
5.010	640.68	616.61	627.58
3.980	640.26	616.19	627.24
3.160	641.32	617.21	628.33
2.510	640.31	616.25	627.39
1.990	616.40	593.22	603.95
1.580	640.80	616.73	627.90
1.260	641.36	617.26	628.44
1.000	613.35	590.29	601.07
0.790	642.64	618.49	629.71
0.631	641.81	617.70	628.91
0.501	641.86	617.75	628.94
0.398	467.42	449.82	457.86
0.316	642.21	618.07	629.29
0.251	489.19	470.72	479.17
0.199	344.90	332.03	338.07
0.158	567.47	545.98	555.76
0.126	549.68	528.87	538.26
0.100	643.28	619.12	630.30

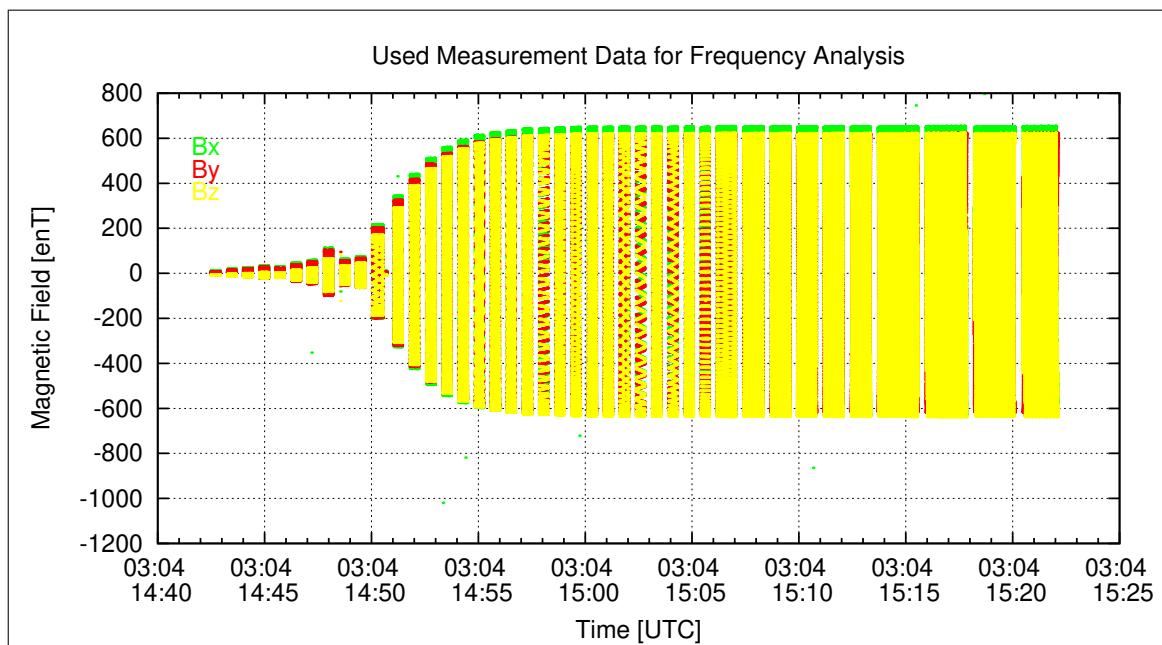


Figure 21: Used packets of Measured data for the Frequency analysis

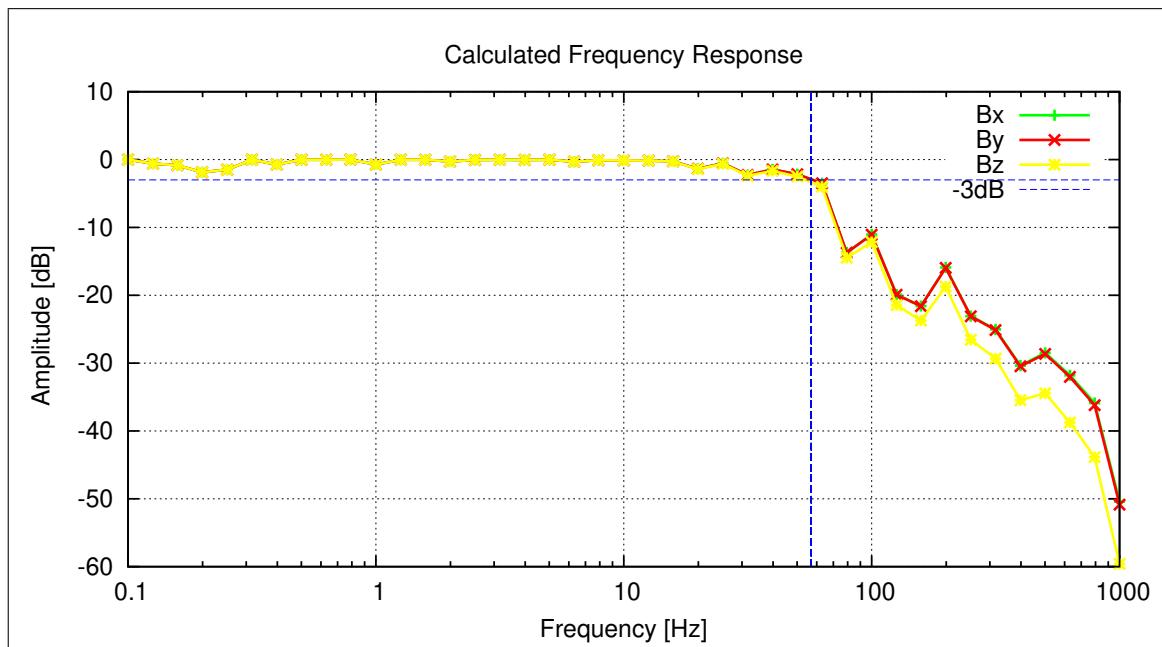


Figure 22: Calculated Frequency Response

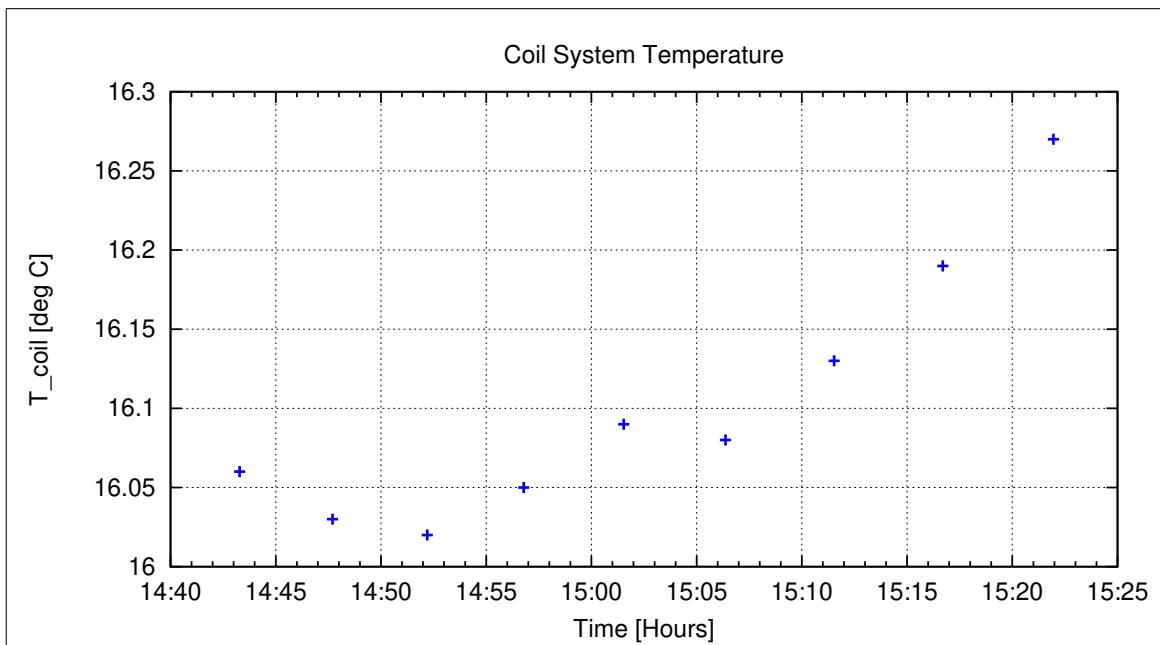


Figure 23: Coil System Temperature

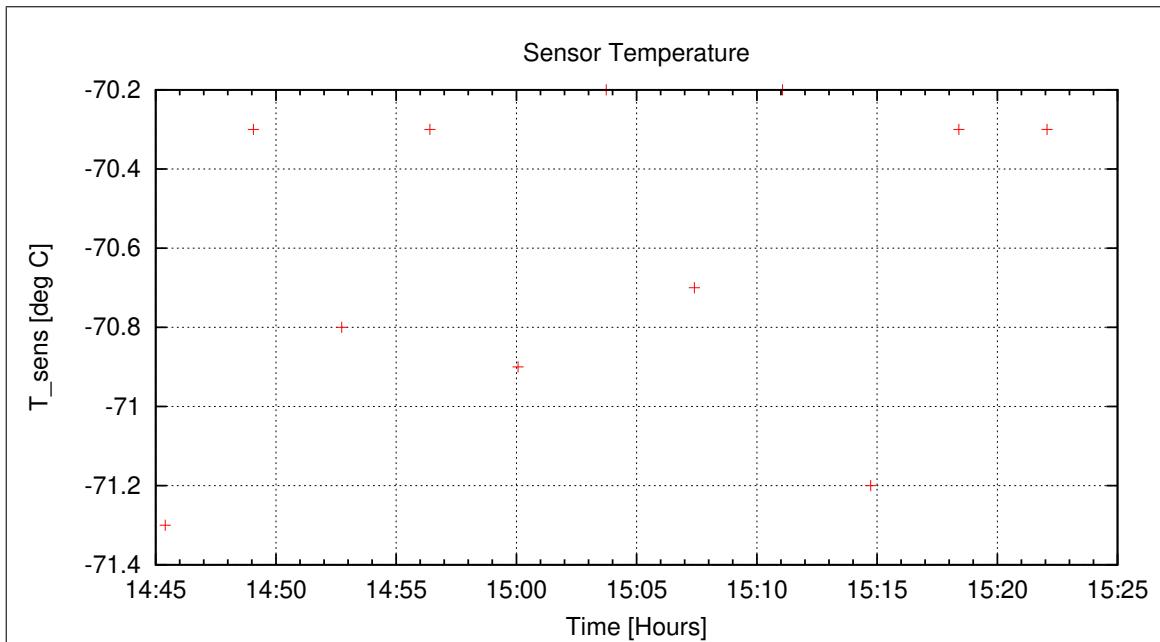


Figure 24: Sensor Temperature

Afterwards the thermal system was switched off for smooth heating up to -20°C.

Zerofield measurements (open loop, cal mode 4) in dynamically compensated earthfield conditions were conducted during the night. Measurements started at 16:08.

## 4 Measurements on April 4, 2013

The measurements over night were conducted without any problem. At 06:37 the temperature indicated by  $T_{59}$  was  $-21^\circ$ . The MPO-sensor temperatures sensors showed the same temperature.

### 4.1 Data

CCD File	Configuration File	Remark
13-04-04\06-41-24.CCR	LIN2000XYZE.MAG	
13-04-04\07-18-40.CCR	LIN2000XYZE.MAG	
13-04-04\07-54-10.CCR	OFFSET_200.MAG	
13-04-04\08-08-11.CCR	LIN2000XYZE.MAG	
13-04-04\08-39-48.CCR	OFFSET_200.MAG	
13-04-04\08-50-42.CCR	LIN2000XYZE.MAG	
13-04-04\09-21-00.CCR	LIN2000XYZE.MAG	
13-04-04\09-51-19.CCR	LIN2000XYZE.MAG	
13-04-04\10-21-37.CCR	LIN2000XYZE.MAG	
13-04-04\10-26-52.CCR	OFFSET_200.MAG	
13-04-04\10-51-43.CCR	LIN2000XYZE.MAG	
13-04-04\11-22-26.CCR	OFFSET_200.MAG	
13-04-04\11-33-17.CCR	LIN2000XYZE.MAG	
13-04-04\12-03-52.CCR	LIN2000XYZE.MAG	
13-04-04\12-34-10.CCR	LIN2000XYZE.MAG	
13-04-04\13-05-27.CCR	OFFSET_200.MAG	
13-04-04\13-14-59.CCR	FREQ2000.MAG	
13-04-04\14-11-50.CCR	FREQ2000.MAG	
13-04-04\14-55-20.CCR	LIN2000XYZE.MAG	
13-04-04\15-26-56.CCR	OFFSET_200.MAG	
13-04-04\15-40-25.CCR	NULL_LANG.MAG	

## 4.2 DC-Analysis at Low Temperature - OB Sensor

Linearity and offset measurements were performed at  $T_{59} = -21^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

Afterwards the system was heated up to  $T_{59} = +30^\circ$ .

## 4.3 DC-Analysis at moderate Temperature - OB Sensor

Linearity and offset measurements were performed at  $T_{59} = +30^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

Afterwards the system was heated up to  $T_{59} = +80^\circ$ .

## 4.4 DC-Analysis at high Temperature - OB Sensor

Linearity and offset measurements were performed at  $T_{59} = +80^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

## 4.5 AC-Analysis at high Temperature - OB Sensor

The sensor was rotated to the diagonal in space orientation and the usual AC measurements were conducted at  $T_{59} = +80^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

Afterward the sensor was rotated back to the standard orientation (POS1). The thermal system was switched off for smooth cooling during the night. Measurements in dynamically compensated zerofield conditions , starting at 15:40, were conducted during the night and the weekend in cal mode 0.

## 5 Measurements on April 5, 2013

No personnel around today. Zerofield measurements continued.

### 5.1 Data

CCD File	Configuration File	Remark
13-04-05\15-40-58.CCR	NULL_LANG.MAG	

## 6 Measurements on April 6, 2013

No personnel around today. Zerofield measurements continued.

### 6.1 Data

CCD File	Configuration File	Remark
13-04-06\15-41-30.CCR	NULL_LANG.MAG	

## 7 Measurements on April 7, 2013

No personnel around today. Zerofield measurements continued.

### 7.1 Data

CCD File	Configuration File	Remark
13-04-07\15-42-17.CCR	NULL_LANG.MAG	

## 8 Measurements on April 8, 2013

The zerofield measurements were stopped at 06:20.  $T_{59}$  showed 18.1°C. It showed up that MPO stopped sending data on April 7. Reason unknown. After reboot, the instrument worked properly again.

Additionally the Opto-Isolator of the MRode GPIB bus did not work anymore. Therefore, it was decided to couple all GPIB devices directly to the MRode-Controller, although a higher noise level was expected this way. But there was no change to do it in a different way, as the GPIB Bus is essential for controlling the field generation devices.

During the GPIB analysis the thermal system was already activated. The goal temperature was set to  $T_{59} = +130^\circ$ .

### 8.1 Data

CCD File	Configuration File	Remark
13-04-08\06-43-09.CCR	NULL_LANG.MAG	
13-04-08\08-29-20.CCR	LIN2000XYZE.MAG	
13-04-08\08-59-25.CCR	LIN2000XYZE.MAG	
13-04-08\09-30-44.CCR	OFFSET_200.MAG	
13-04-08\09-40-37.CCR	FREQ2000.MAG	
13-04-08\10-31-48.CCR	FREQ2000.MAG	
13-04-08\11-15-40.CCR	LIN2000XYZE.MAG	
13-04-08\11-46-06.CCR	OFFSET_200.MAG	
13-04-08\11-55-12.CCR	LIN2000XYZE.MAG	
13-04-08\12-25-15.CCR	LIN2000XYZE.MAG	
13-04-08\12-55-19.CCR	LIN2000XYZE.MAG	
13-04-08\13-25-22.CCR	LIN2000XYZE.MAG	
13-04-08\13-56-15.CCR	OFFSET_200.MAG	
13-04-08\14-06-16.CCR	FREQ2000.MAG	
13-04-08\15-02-45.CCR	LIN2000XYZE.MAG	
13-04-08\15-06-16.CCR	LIN2000XYZE.MAG	
13-04-08\15-36-36.CCR	OFFSET_200.MAG	
13-04-08\15-46-19.CCR	FREQ2000.MAG	
13-04-08\16-34-53.CCR	NULL.MAG	
13-04-08\22-35-12.CCR	NULL.MAG	

## 8.2 DC-Analysis at very high Temperature - OB Sensor

Linearity and offset measurements were performed at  $T_{59} = +130^\circ\text{C}$  in cal mode 4 and cal mode 0 starting at 08:30.

Thermal Analysis: refer to section 12.

## 8.3 AC-Analysis at very high Temperature - OB Sensor

The sensor was rotated to the diagonal in space orientation and the usual AC measurements were conducted at  $T_{59} = +130^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

Afterwards the thermal box was heated up to the final temperature of  $+180^\circ\text{C}$ .

## 8.4 DC-Analysis at highest Temperature - OB Sensor

Linearity and offset measurements were performed at  $T_{59} = +180^\circ\text{C}$  in cal mode 4 and cal mode 0 starting at 08:30.

Thermal Analysis: refer to section 12.

## 8.5 AC-Analysis at highest Temperature - OB Sensor

The sensor was rotated to the diagonal in space orientation and the usual AC measurements were conducted at  $T_{59} = +180^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 12.

Afterwards the thermal system was switched off to let the temperature fall smoothly. Over night zerofield measurements in dynamically compensated earthfield conditions were conducted in cal mode 0. The measurements started at 16:34. Sensor alignment: Standard, Azimuth = $180^\circ$ , Elevation= $0^\circ$ .

## 9 Measurements on April 9, 2013

The measurements overnight were conducted smoothly. At 06:32 the box temperature was about  $T_{59} = +71^\circ\text{C}$ .

The box was opened and the OB sensor was removed.

The BS\_11 = OB calibration finished at 06:45.

### 9.1 Data

CCD File	Configuration File	Remark
13-04-09\04-35-30.CCR	NULL.MAG	
13-04-09\06-32-42.CCR	NULL.MAG	
		Change to IB Sensor
13-04-09\07-22-11.CCR	LIN2000XYZE.MAG	
13-04-09\07-52-14.CCR	LIN2000XYZE.MAG	
13-04-09\08-22-17.CCR	LIN2000XYZE.MAG	
13-04-09\08-52-20.CCR	LIN2000XYZE.MAG	
13-04-09\09-22-23.CCR	LIN2000XYZE.MAG	
13-04-09\09-52-27.CCR	LIN2000XYZE.MAG	
13-04-09\10-23-29.CCR	OFFSET_200.MAG	
13-04-09\10-34-40.CCR	LIN2000XYZE.MAG	
13-04-09\11-05-13.CCR	OFFSET_200.MAG	
13-04-09\11-14-46.CCR	OFFSET_200.MAG	
13-04-09\11-24-12.CCR	LIN2000XYZE.MAG	
13-04-09\11-54-15.CCR	LIN2000XYZE.MAG	
13-04-09\12-26-36.CCR	FREQ2000.MAG	
13-04-09\13-08-27.CCR	OFFSET_200.MAG	
13-04-09\13-18-15.CCR	OFFSET_200.MAG	
13-04-09\13-27-51.CCR	FREQ2000.MAG	
13-04-09\14-12-36.CCR	LIN2000XYZE.MAG	
13-04-09\14-53-47.CCR	NULL.MAG	
13-04-09\20-54-03.CCR	NULL.MAG	

The IB sensor BS\_10 was installed in the thermal box. The box was erected to the vertical orientation and shifted to CoC.

Cooling of the system down to  $-20^{\circ}\text{C}$  started at 07:22.

## 9.2 DC-Analysis at Low Temperature - IB Sensor, cal mode 0

Linearity and offset measurements were performed at  $T_{59} = -20^{\circ}\text{C}$  in cal mode 0.

### 9.2.1 Calibration on 3 Linear Axes

#### Used Files:

CCD File	Configuration File	Remark
13-04-09\09-52-27.CCR	LIN2000XYZE.MAG	

Parameter File: PARAMETER\_LIN\_\_13-04-09\_09-52-27.CPF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Sensor Rotation:

$$\underline{\underline{\rho}} = \begin{pmatrix} +0.999974 & +0.003127 & +0.006434 \\ -0.003132 & +0.999995 & +0.000706 \\ -0.006432 & -0.000726 & +0.999979 \end{pmatrix}$$

Rotation Angles:

$$\begin{aligned} \text{Angle } (X_c, X_m): \quad \lambda_x &= +0^\circ 24'36'' \\ \text{Angle } (Y_c, Y_m): \quad \mu_y &= +0^\circ 11'2'' \\ \text{Angle } (Z_c, Z_m): \quad \nu_z &= +0^\circ 22'15'' \end{aligned}$$

Determinant of Rotation Matrix: 1.00000

Nominal Field Source: SOLARTRON

Fields applied for 24.0 s

Mean Sensor Temperature: -30.6°C

Automatic Coil Correction: used

Earthfield Compensation: X = DYNAMIC  
Y = DYNAMIC  
Z = DYNAMIC

## Offset Treatment:

A polynomial offset trend of order 2 has been fitted and subtracted from the raw data before creating the sensor model.

Mean Coil System Residual + Sensor Offset:  $\underline{B}^{or} = (-3.954, -0.950, -11.069)$  nT

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## Raw Data Quality:

Standard Deviation of used Raw Data Blocks:

[Values in eng nT]	$s_x$	$s_y$	$s_z$
Minimum	0.000	0.376	0.242
Mean	2.315	0.449	0.452
Maximum	2.860	1.274	1.210

## Calibration Parameter:

$$\text{Transfermatrix: } \underline{\phi} = \underline{\underline{R}}_{\text{nom}} \underline{\underline{\omega}} \underline{\underline{\sigma}} = \begin{pmatrix} +0.976259 & +0.003130 & +0.006347 \\ -0.010380 & +0.988528 & +0.000696 \\ -0.007349 & +0.005271 & +0.986472 \end{pmatrix}$$

$$\text{Reduced Transfermatrix: } \tilde{\underline{\phi}} = \underline{\underline{\omega}} \underline{\underline{\sigma}} = \begin{pmatrix} +0.976314 & +0.000000 & +0.000000 \\ -0.007321 & +0.988529 & +0.000000 \\ -0.001075 & +0.005989 & +0.986493 \end{pmatrix}$$

$$\text{Sensitivity: } \underline{\sigma} = \begin{pmatrix} +0.976314 & +0.000000 & +0.000000 \\ +0.000000 & +0.988501 & +0.000000 \\ +0.000000 & +0.000000 & +0.986474 \end{pmatrix}$$

$$\text{Misalignment: } \underline{\omega} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ -0.007499 & +1.000028 & +0.000000 \\ -0.001101 & +0.006058 & +1.000019 \end{pmatrix}$$

Sensor Misalignment Angles:

$$\begin{aligned} \xi_{x,y} &= +89^\circ 34'13'' \\ \xi_{x,z} &= +89^\circ 56'22'' \\ \xi_{y,z} &= +90^\circ 20'48'' \end{aligned}$$

## Model Quality:

Standard Deviation, Maximum and Minimum Error of Calculated Model:

[Values in nT]	$X$	$Y$	$Z$
Standard Deviation	0.130	0.170	0.163
Maximum Error	0.280	0.460	0.445
Minimum Error	-0.225	-0.244	-0.287

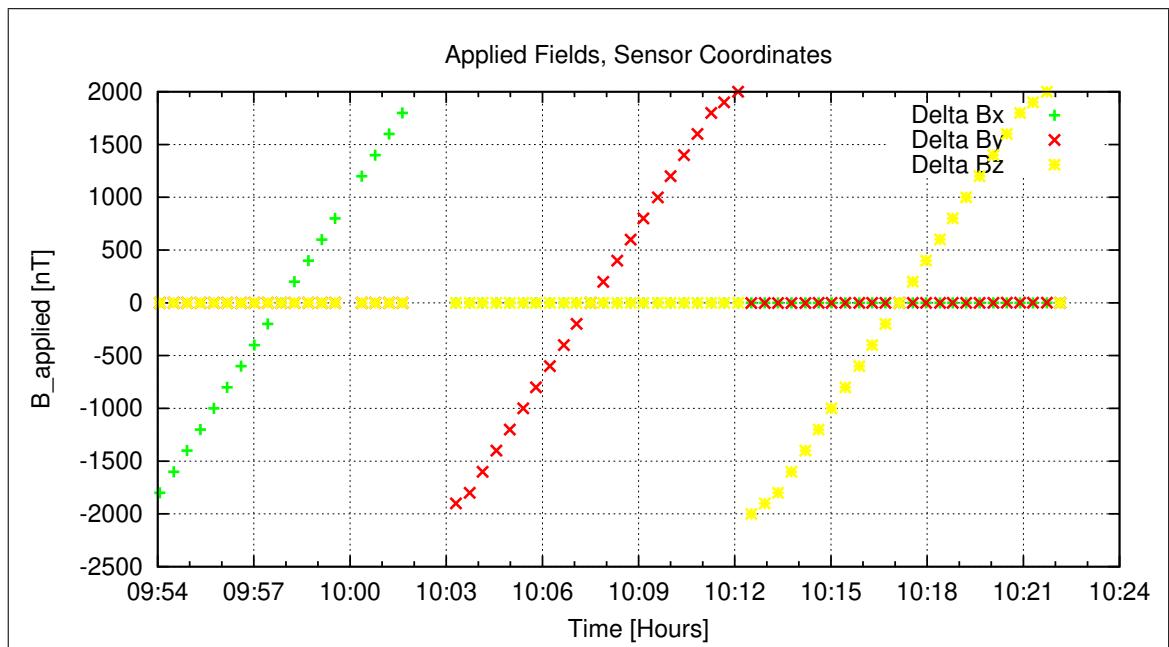


Figure 25: Applied Fields

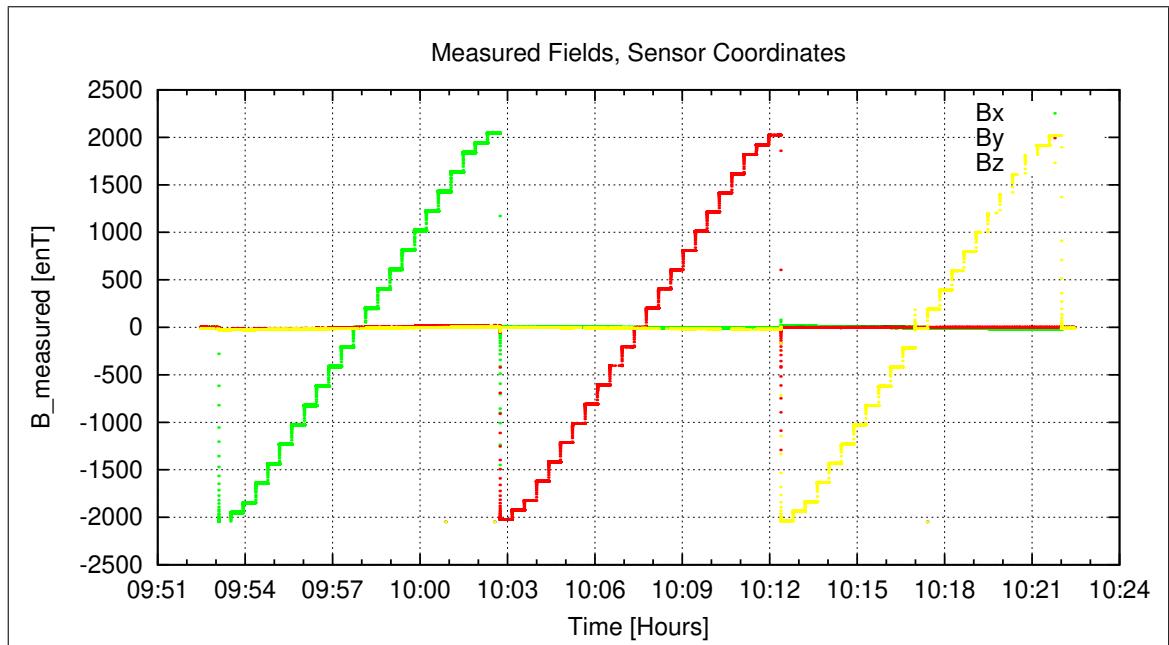


Figure 26: Measured Data

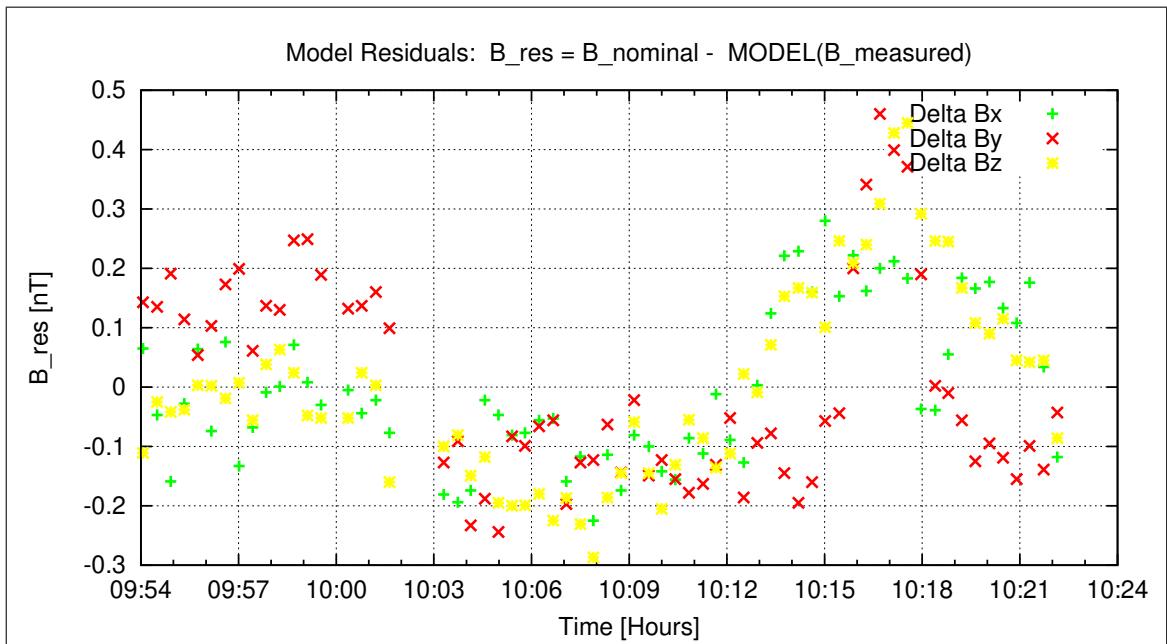


Figure 27: Model Quality - Differences of applied field and modelled measurement data

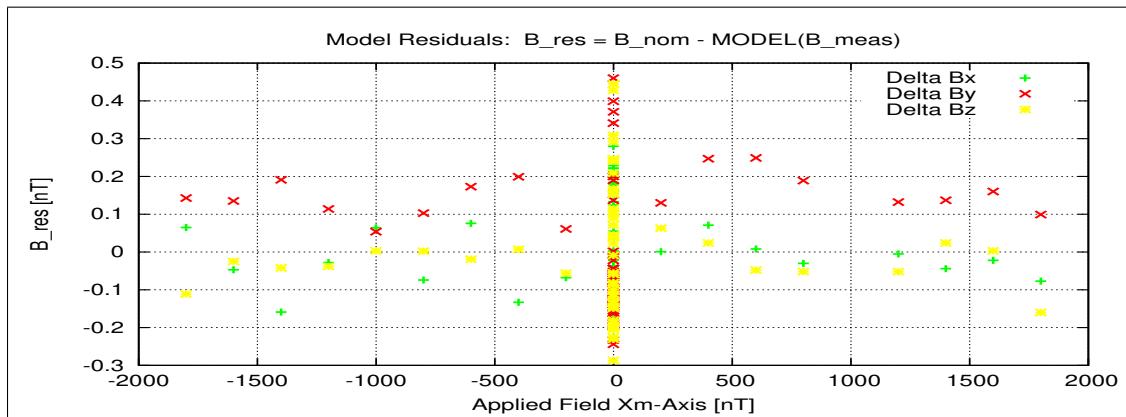


Figure 28: RESIDUALS vs FLD X

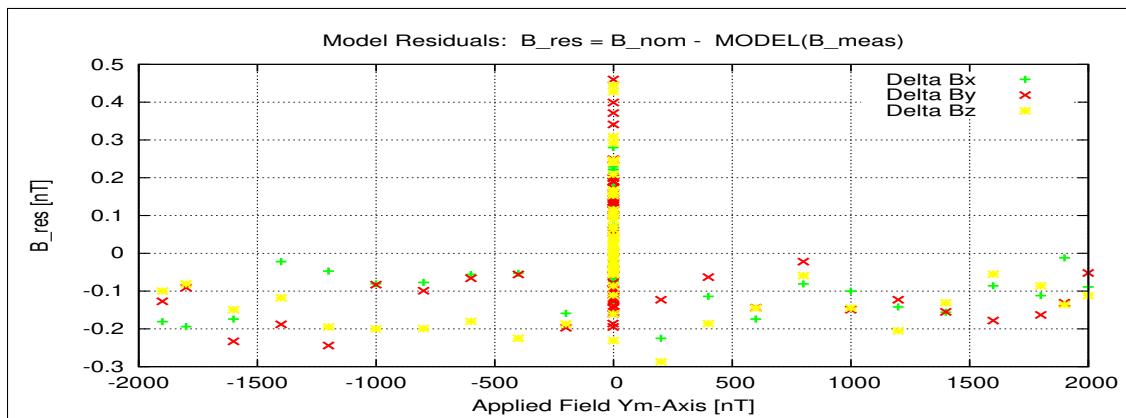


Figure 29: RESIDUALS vs FLD Y

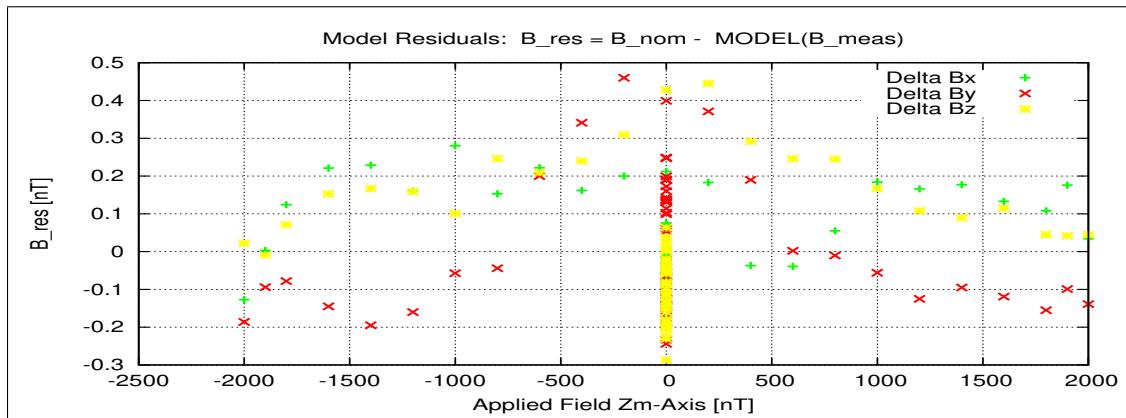


Figure 30: RESIDUALS vs FLD Z

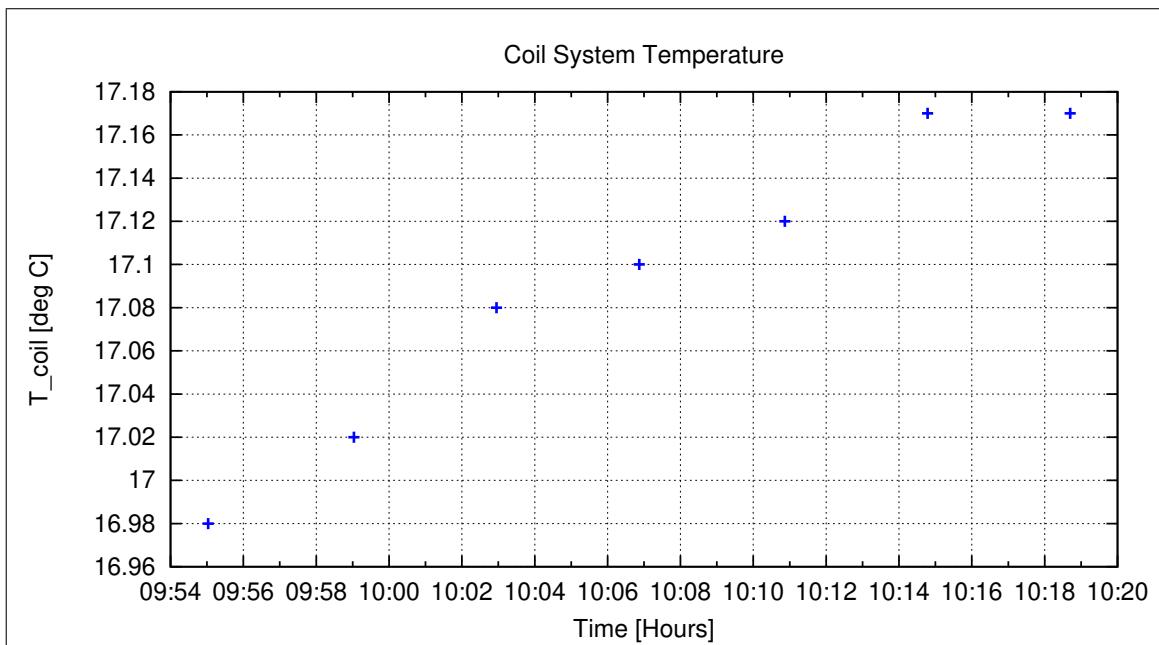


Figure 31: Coil System Temperature

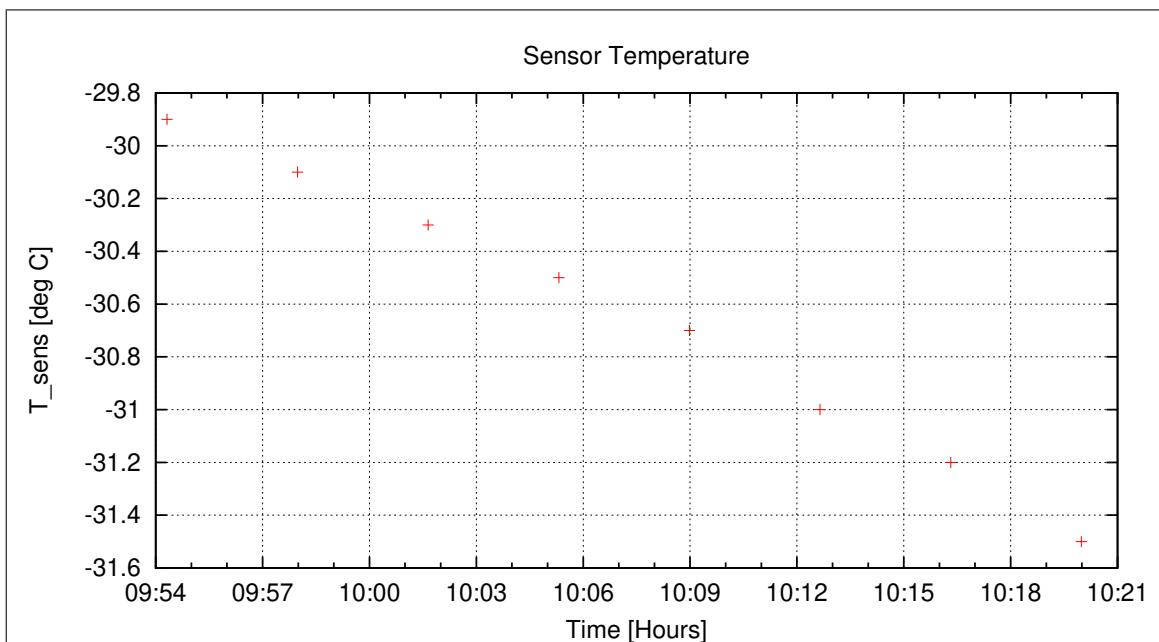


Figure 32: Sensor Temperature

### 9.2.2 OFFSET Calculation

In this section the instrument offsets and the residual field of the Coil System will be evaluated. Measurements at two orientations for each component act as input for the offset calculation. From the "normal" (0-degrees) and "turned" (180-degrees) orientations the offsets and residual fields can be derived:

$$\begin{aligned} B_{\text{off}} &= \frac{B_{\text{normal}} + B_{\text{turned}}}{2} \\ B_{\text{res}} &= \frac{B_{\text{normal}} - B_{\text{turned}}}{2} \end{aligned}$$

#### Used Offset Measurements:

CCD File	Configuration File	Remark
13-04-09\11-14-46.CCR	OFFSET_200.MAG	

Parameter File: OFF\_PARAMETER\_\_13-04-09-11-14-46.OPF

**Calibration Parameter:**

	Component	Offset [enT]	Standard deviation [enT]
Sensor Offsets:	X	-0.64	0.111
	Y	-0.78	0.104
	Z	-0.38	0.100

Residual Field of the Coil System:

	Component	$B_{\text{res}}$ [enT]
	X	-2.07
	Y	-0.46
	Z	2.01

Remark: Residual field is given in actual DUT coordinates, not in coil-coordinates!

Thermal Analysis: refer to section 13.

### 9.3 DC-Analysis at Low Temperature - IB Sensor, cal mode 4

Linearity and offset measurements were performed at  $T_{59} = -20^{\circ}\text{C}$  in cal mode 4.

#### 9.3.1 Calibration on 3 Linear Axes

##### Used Files:

CCD File	Configuration File	Remark
13-04-09\10-34-40.CCR	LIN2000XYZE.MAG	

Parameter File: PARAMETER\_LIN\_\_13-04-09\_10-34-40.CPF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Sensor Rotation:

$$\underline{\rho} = \begin{pmatrix} +0.999707 & +0.023539 & +0.005617 \\ -0.023561 & +0.999715 & +0.003876 \\ -0.005524 & -0.004007 & +0.999977 \end{pmatrix}$$

Rotation Angles:

$$\begin{aligned} \text{Angle } (X_c, X_m): \quad \lambda_x &= +1^\circ 23'12'' \\ \text{Angle } (Y_c, Y_m): \quad \mu_y &= +1^\circ 22'6'' \\ \text{Angle } (Z_c, Z_m): \quad \nu_z &= +0^\circ 23'28'' \end{aligned}$$

Determinant of Rotation Matrix: 1.00000

Nominal Field Source: FLDS

Fields applied for 25.0 s

Mean Sensor Temperature: -32.9°C

Automatic Coil Correction: used

Earthfield Compensation: X = DYNAMIC  
Y = DYNAMIC  
Z = DYNAMIC

## Offset Treatment:

A polynomial offset trend of order 2 has been fitted and subtracted from the raw data before creating the sensor model.

Mean Coil System Residual + Sensor Offset:  $\underline{B}^{or} = (-2.786, -1.095, -10.723)$  nT

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## Raw Data Quality:

Standard Deviation of used Raw Data Blocks:

[Values in eng nT]	$s_x$	$s_y$	$s_z$
Minimum	1.638	0.191	0.000
Mean	2.299	0.391	0.478
Maximum	2.952	2.520	1.822

## Calibration Parameter:

$$\begin{aligned}
 \text{Transfermatrix: } \underline{\phi} &= \underline{\underline{R}}_{\text{nom}} \underline{\underline{\omega}} \underline{\underline{\sigma}} = \begin{pmatrix} +0.976121 & +0.023140 & +0.005394 \\ -0.020240 & +0.980345 & +0.003723 \\ -0.013290 & +0.006444 & +0.960428 \end{pmatrix} \\
 \text{Reduced Transfermatrix: } \tilde{\underline{\phi}} &= \tilde{\underline{\underline{\omega}}} \underline{\underline{\sigma}} = \begin{pmatrix} +0.976385 & +0.000000 & +0.000000 \\ +0.002795 & +0.980584 & +0.000000 \\ -0.007885 & +0.010374 & +0.960450 \end{pmatrix} \\
 \text{Sensitivity: } \underline{\sigma} &= \begin{pmatrix} +0.976385 & +0.000000 & +0.000000 \\ +0.000000 & +0.980580 & +0.000000 \\ +0.000000 & +0.000000 & +0.960365 \end{pmatrix} \\
 \text{Misalignment: } \underline{\omega} &= \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.002863 & +1.000004 & +0.000000 \\ -0.008076 & +0.010579 & +1.000089 \end{pmatrix}
 \end{aligned}$$

Sensor Misalignment Angles:

$$\begin{aligned}
 \xi_{x,y} &= +90^\circ 9'51'' \\
 \xi_{x,z} &= +89^\circ 32'8'' \\
 \xi_{y,z} &= +90^\circ 36'27''
 \end{aligned}$$

## Model Quality:

Standard Deviation, Maximum and Minimum Error of Calculated Model:

[Values in nT]	$X$	$Y$	$Z$
Standard Deviation	0.124	0.222	0.129
Maximum Error	0.325	0.249	0.309
Minimum Error	-0.320	-0.800	-0.357

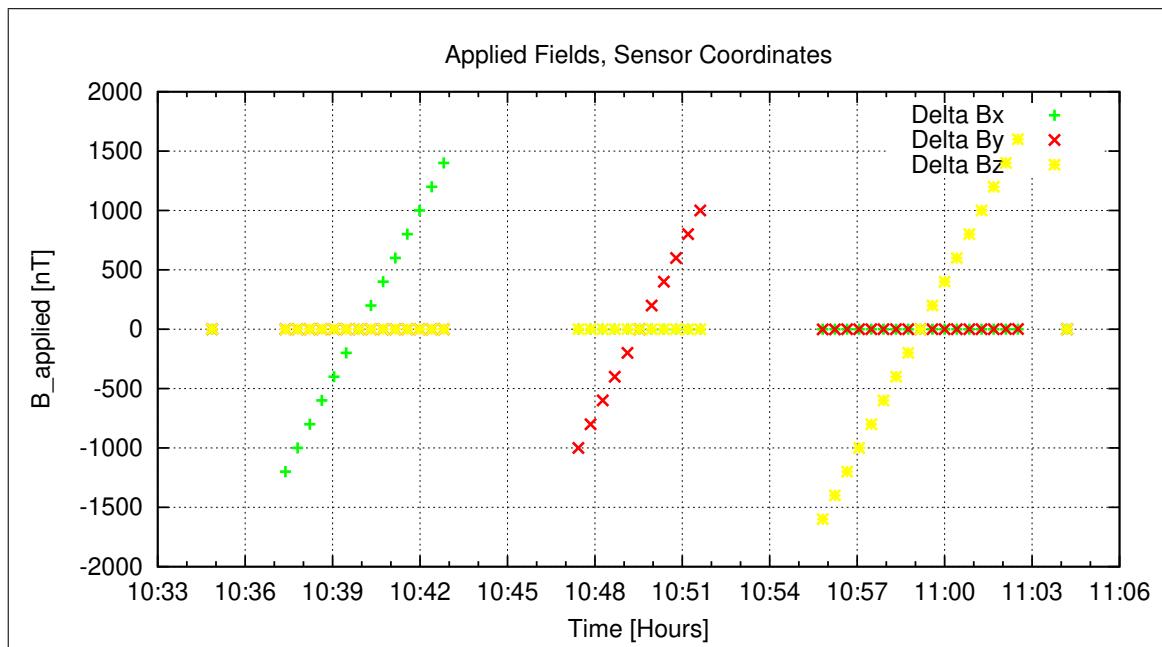


Figure 33: Applied Fields

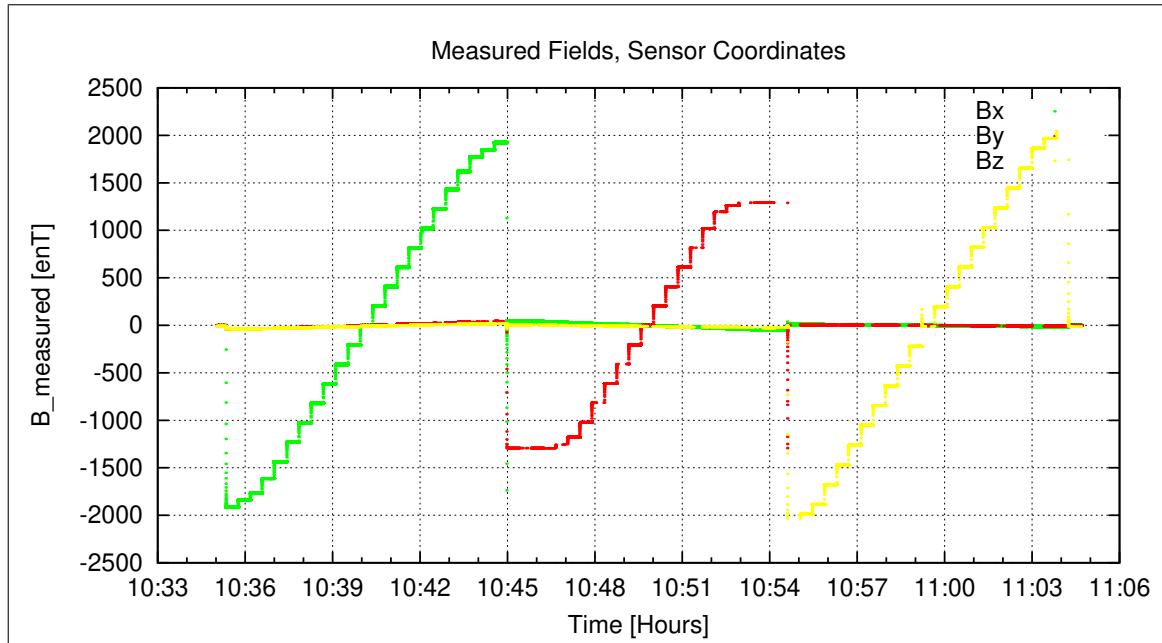


Figure 34: Measured Data

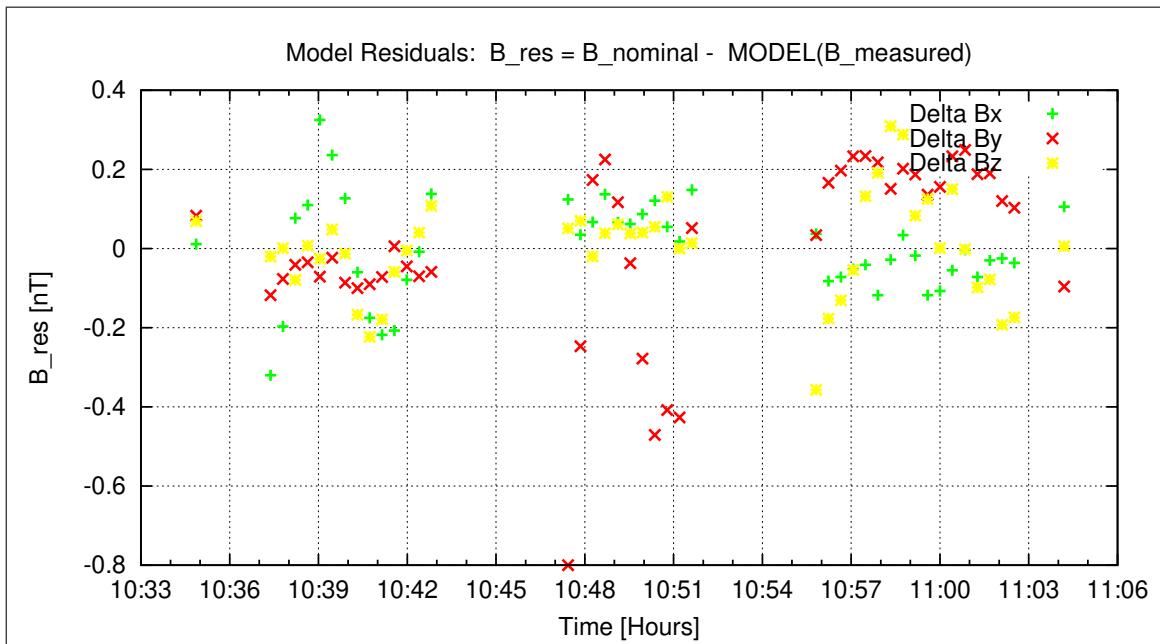


Figure 35: Model Quality - Differences of applied field and modelled measurement data

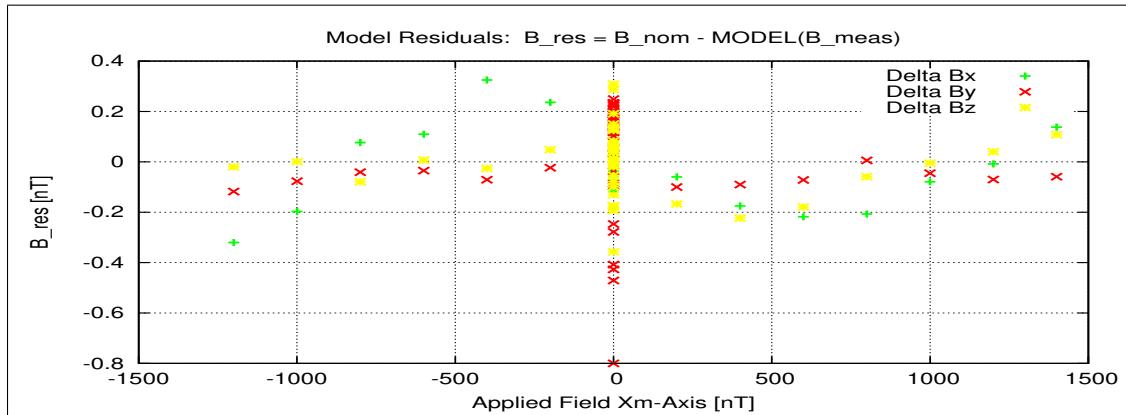


Figure 36: RESIDUALS vs FLD X

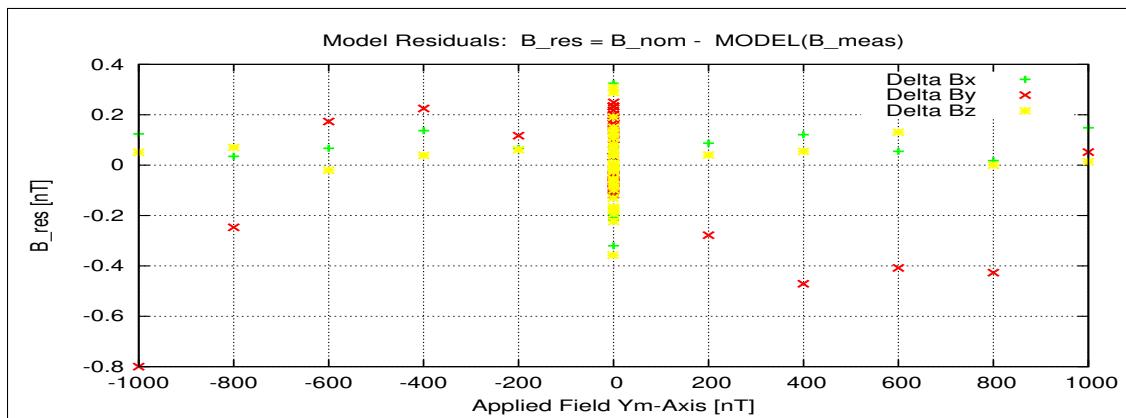


Figure 37: RESIDUALS vs FLD Y

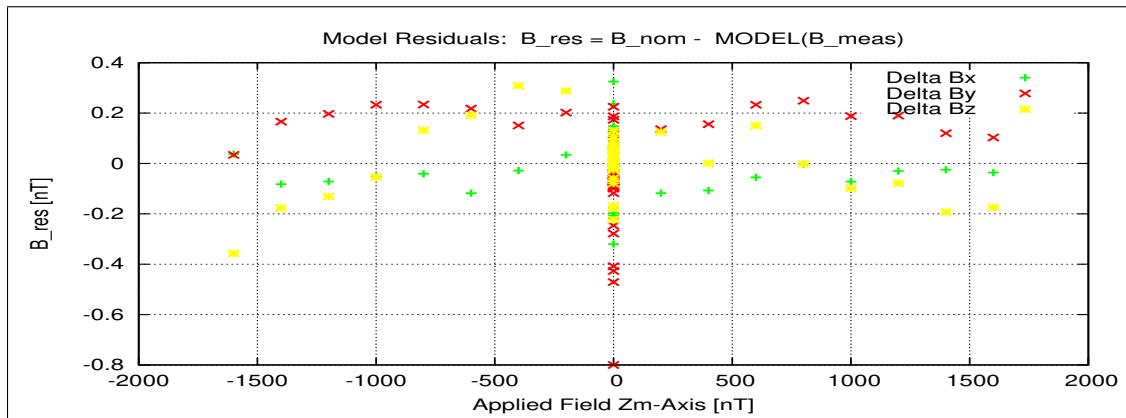


Figure 38: RESIDUALS vs FLD Z

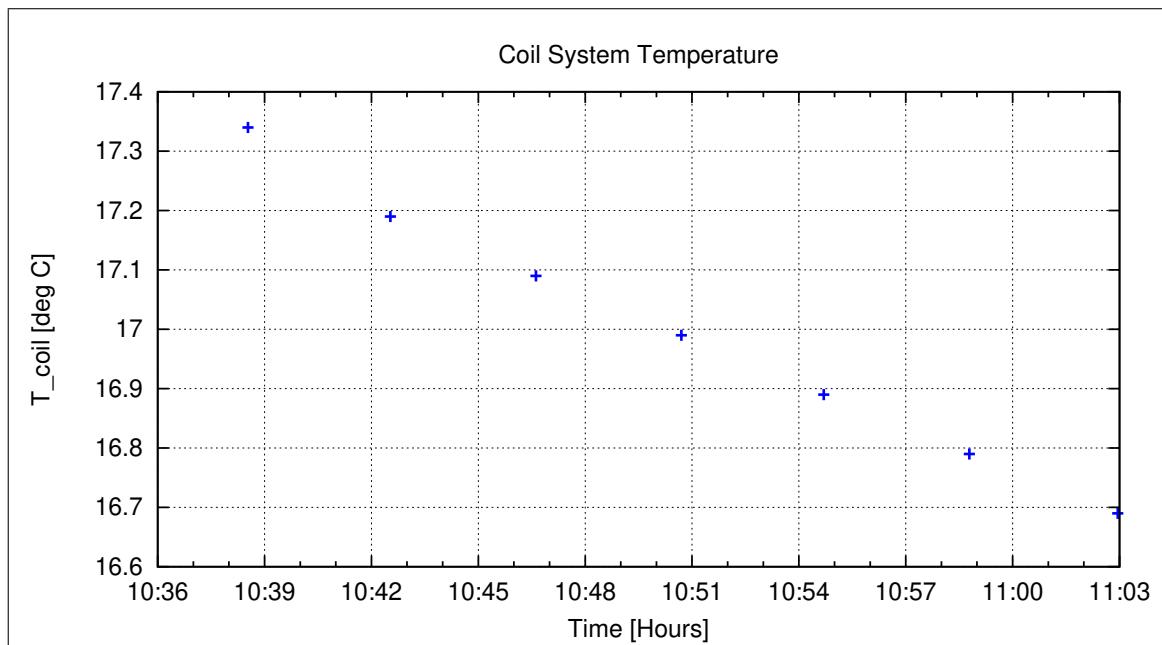


Figure 39: Coil System Temperature

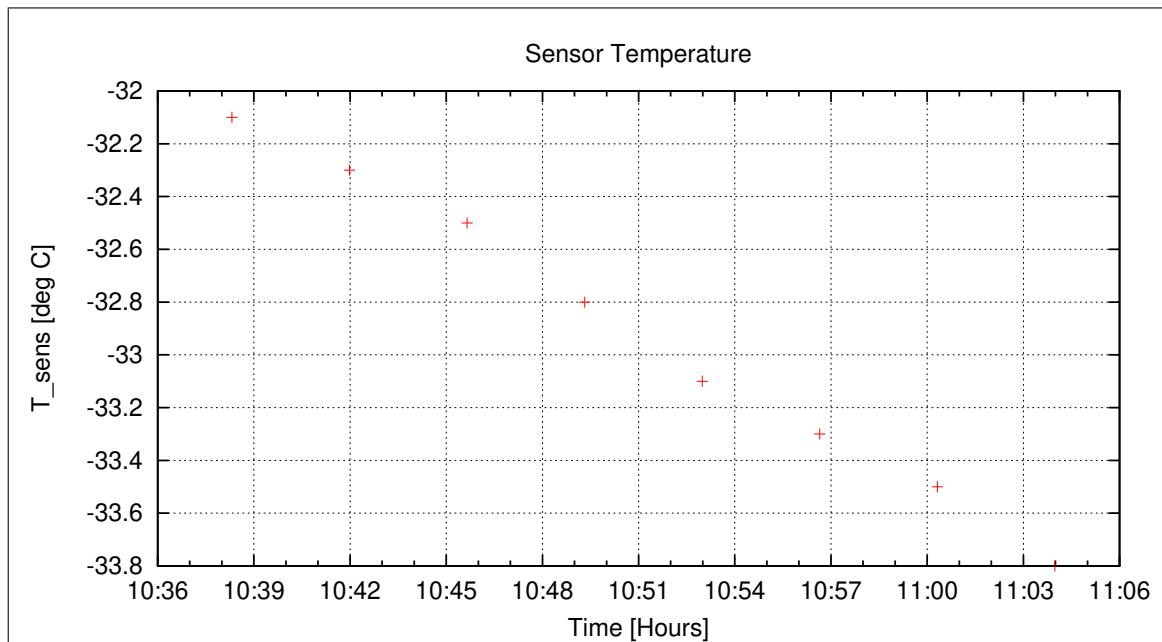


Figure 40: Sensor Temperature

### 9.3.2 OFFSET Calculation

In this section the instrument offsets and the residual field of the Coil System will be evaluated. Measurements at two orientations for each component act as input for the offset calculation. From the "normal" (0-degrees) and "turned" (180-degrees) orientations the offsets and residual fields can be derived:

$$\begin{aligned} B_{\text{off}} &= \frac{B_{\text{normal}} + B_{\text{turned}}}{2} \\ B_{\text{res}} &= \frac{B_{\text{normal}} - B_{\text{turned}}}{2} \end{aligned}$$

#### Used Offset Measurements:

CCD File	Configuration File	Remark
13-04-09\11-05-13.CCR	OFFSET_200.MAG	

Parameter File: OFF\_PARAMETER\_\_13-04-09-11-05-13.OPF

**Calibration Parameter:**

	Component	Offset [enT]	Standard deviation [enT]
Sensor Offsets:	X	-0.70	0.088
	Y	-0.79	0.101
	Z	-0.29	0.097

	Component	$B_{\text{res}}$ [enT]
Residual Field of the Coil System:	X	-2.06
	Y	-0.60
	Z	2.09

Remark: Residual field is given in actual DUT coordinates, not in coil-coordinates!

Thermal Analysis: refer to section 13.

Afterwards the system was cooled down up to  $T_{59} = -70^\circ$ .

#### 9.4 DC-Analysis at very low Temperature - IB Sensor

Linearity and offset measurements were performed at  $T_{59} = -70^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 13.

## 9.5 AC-Analysis at very low Temperature - IB Sensor, cal mode 0

A frequency measurement was performed at -70°C.

### Setup:

- Sensor mounted in thermal box. CoC. Box vertical.
- Sensor rotated to:  
Elevation= 45°  
Azimuth= 126°
- Field applied on  $Y_c$ .
- No attenuator

### 9.5.1 Frequency Measurements

This section is dedicated to the frequency behavior of the instrument. The analysis of the performed AC measurements allows to calculate the actual sampling frequency  $f_s$  of the instrument and the frequency response (amplitude vs. frequency). The measurements have been performed with the sensor placed at CoC in a diagonal in space orientation. The AC-fields have been applied on the  $Y_c$  axis only. Using this setup it can be guaranteed that only one frequency is applied at a time and no beat effects occur.

#### Used Frequency Measurements:

CCD File	Configuration File	Remark
13-04-09\12-26-36.CCR	FREQ2000.MAG	

Parameter File: FREQ\_PARAMETER\_\_13-04-09-12-26-36.FPF

**Calibration Parameter:**Sampling Frequency:

Component	$f_s$ [Hz]	Standard deviation [Hz]
X	127.9995	0.000100
Y	127.9979	0.000104
Z	127.9998	0.000768
Mean Sampling Frequency	127.9991	0.001029

3 dB Corner Frequency:

Component	$f_{3\text{dB}}$ [Hz]
X	66.93
Y	65.62
Z	55.63

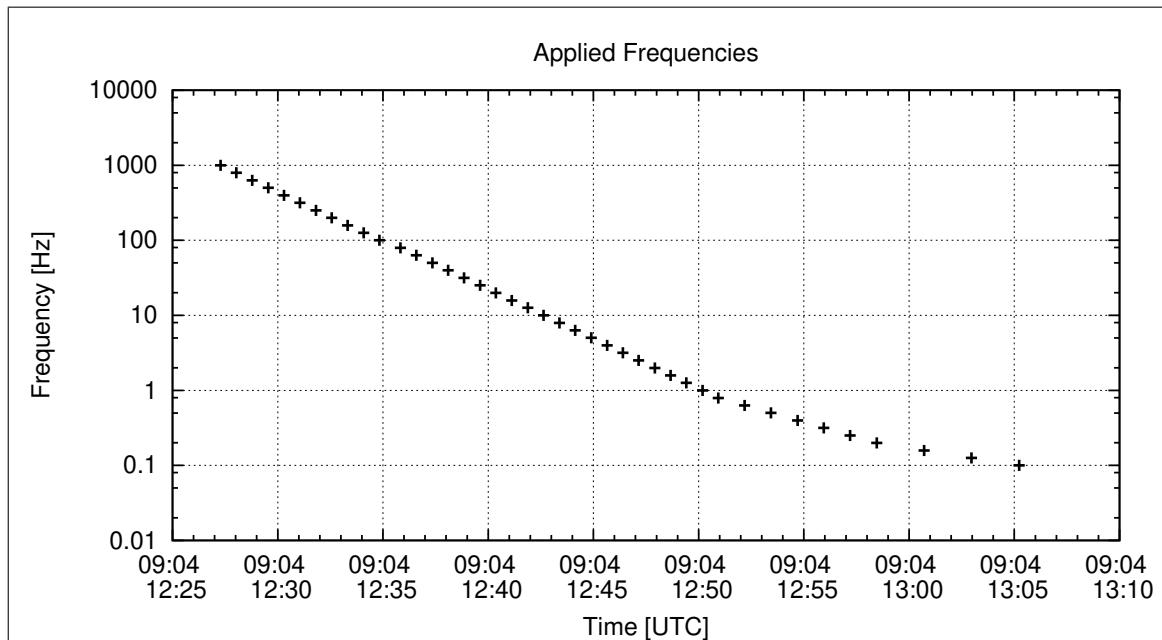
Applied Frequencies and Measured Amplitudes

Figure 41: Applied Frequencies for AC Analysis

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Applied Frequency [Hz]	Bx [enT]	By [enT]	Bz [enT]
1000.000	1.75	1.73	0.65
794.000	9.77	9.75	3.94
631.000	14.97	15.01	6.11
501.000	22.69	22.82	11.39
398.000	18.64	18.76	10.21
316.000	38.87	37.93	20.91
251.000	45.98	46.00	29.75
199.000	111.79	108.81	71.31
158.000	56.12	55.59	42.55
126.000	61.36	61.02	48.96
100.000	160.41	158.02	137.96
79.400	359.88	349.71	294.00
63.100	469.32	453.74	380.80
50.100	546.55	529.59	464.21
39.800	592.13	578.12	533.62
31.600	613.77	603.51	578.31
25.100	623.00	615.22	600.10
19.900	622.22	615.62	602.77
15.800	619.18	613.02	598.53
12.600	612.13	604.57	589.20
10.000	611.92	605.81	586.46
7.900	606.86	600.69	579.65
6.310	607.76	601.50	579.19
5.010	603.74	597.45	574.43
3.980	606.09	599.75	576.08
3.160	601.83	595.50	571.64
2.510	606.75	600.34	576.06
1.990	605.51	599.12	574.73
1.580	605.52	599.09	574.61
1.260	605.68	599.24	574.69
1.000	607.14	600.70	576.05
0.790	605.42	598.98	574.38
0.631	605.63	599.21	574.58
0.501	604.94	598.52	573.91
0.398	606.96	600.54	575.84
0.316	602.16	595.79	571.27
0.251	608.72	602.26	577.45
0.199	608.18	601.74	576.95
0.158	609.52	603.10	578.20
0.126	606.59	600.19	575.44
0.100	606.65	600.26	575.47

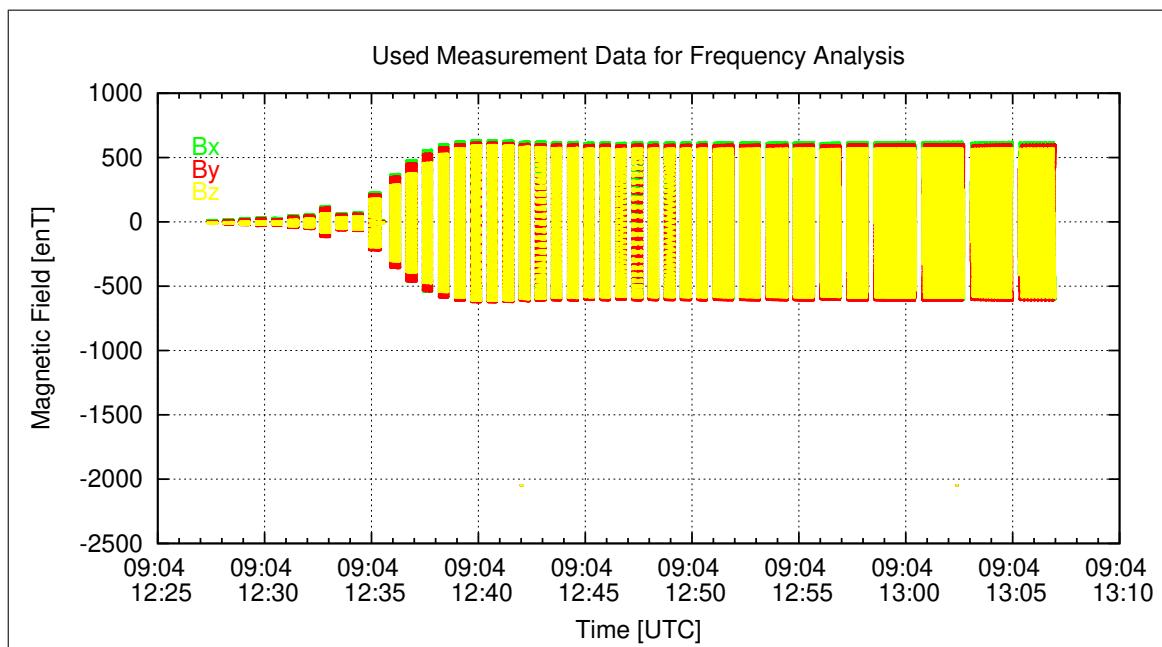


Figure 42: Used packets of Measured data for the Frequency analysis

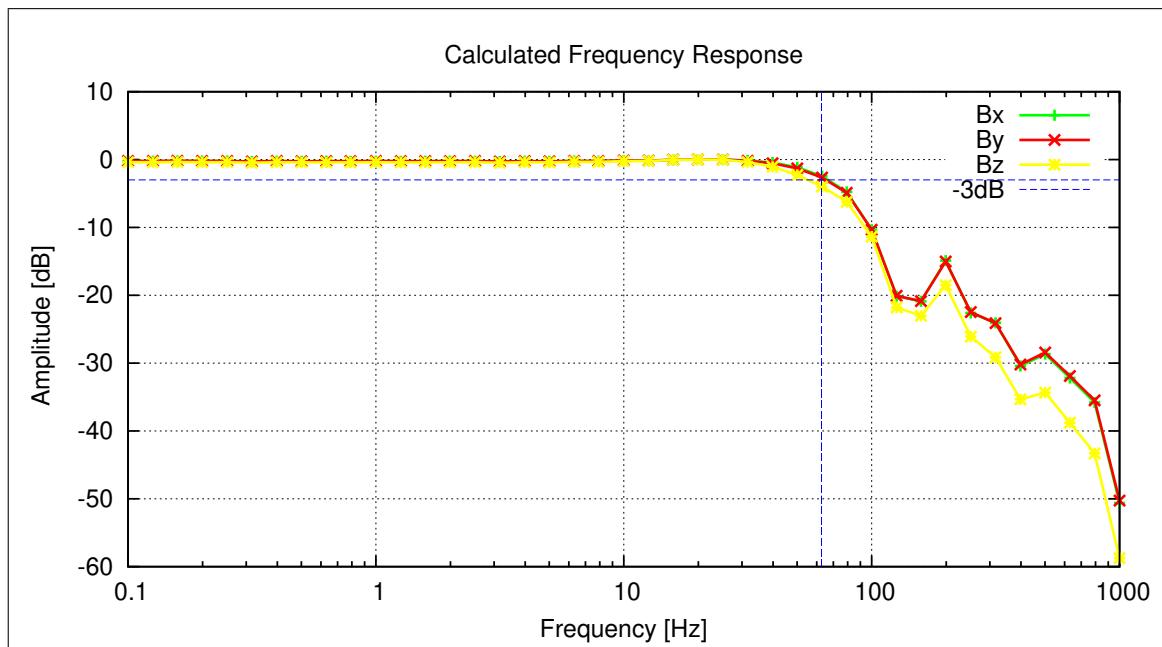


Figure 43: Calculated Frequency Response

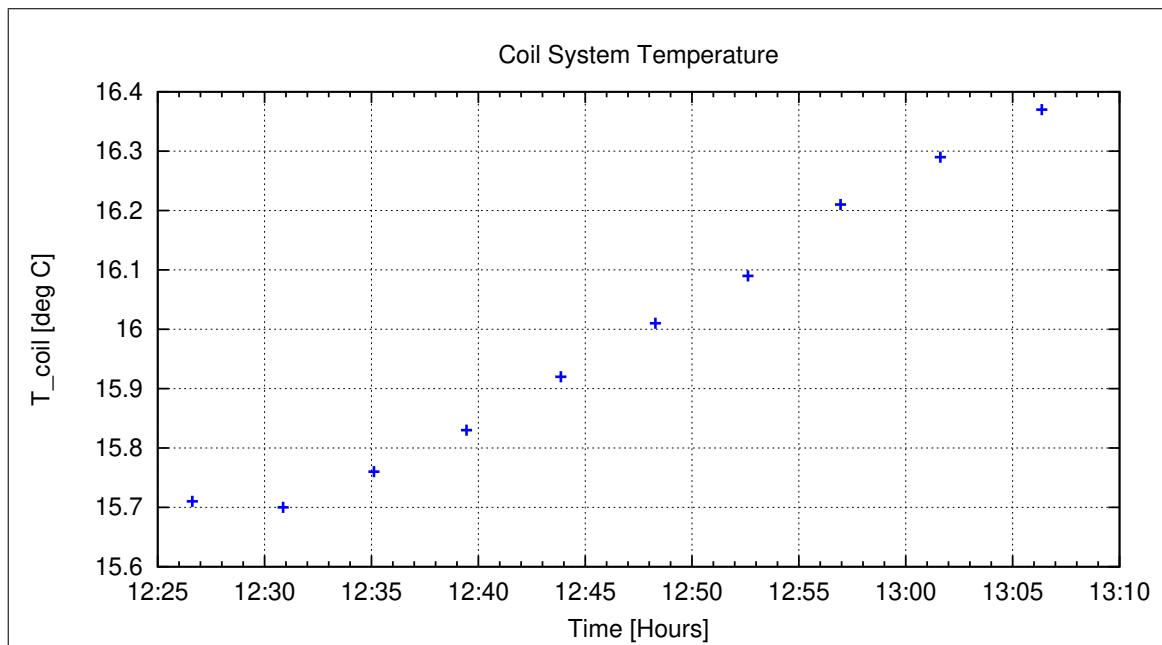


Figure 44: Coil System Temperature

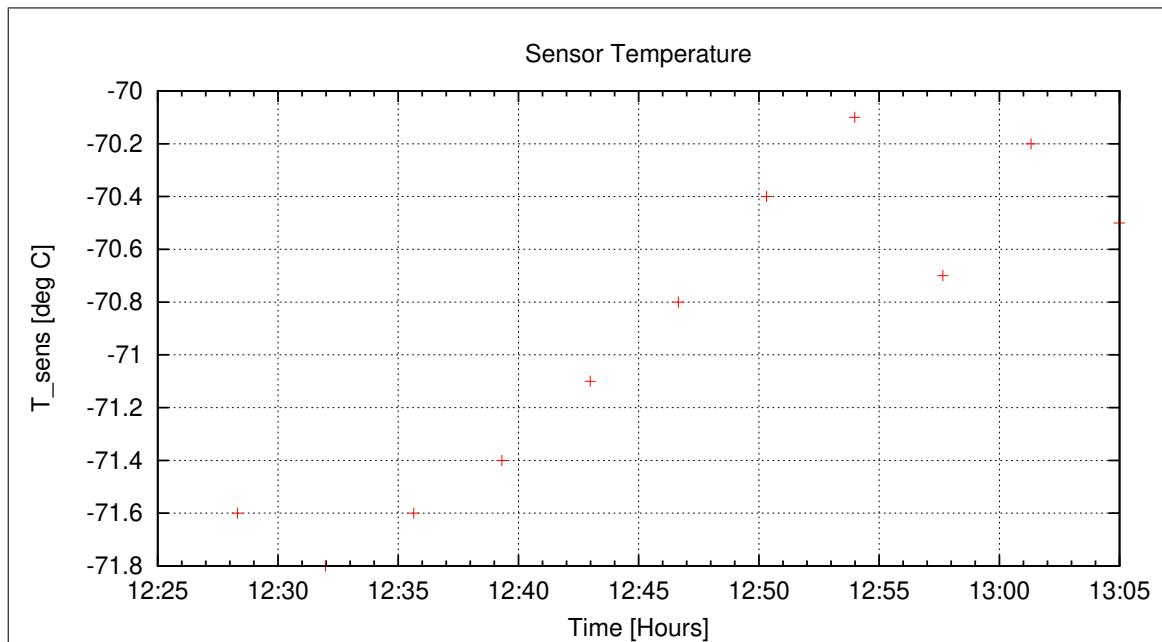


Figure 45: Sensor Temperature

## 9.6 AC-Analysis at very low Temperature - IB Sensor, cal mode 4

A frequency measurement was performed at -70°C.

### Setup:

- Sensor mounted in thermal box. CoC. Box vertical.
- Sensor rotated to:  
Elevation= 45°  
Azimuth= 126°
- Field applied on  $Y_c$ .
- No attenuator

### 9.6.1 Frequency Measurements

This section is dedicated to the frequency behavior of the instrument. The analysis of the performed AC measurements allows to calculate the actual sampling frequency  $f_s$  of the instrument and the frequency response (amplitude vs. frequency). The measurements have been performed with the sensor placed at CoC in a diagonal in space orientation. The AC-fields have been applied on the  $Y_c$  axis only. Using this setup it can be guaranteed that only one frequency is applied at a time and no beat effects occur.

#### Used Frequency Measurements:

CCD File	Configuration File	Remark
13-04-09\13-27-51.CCR	FREQ2000.MAG	

Parameter File: FREQ\_PARAMETER\_\_13-04-09-13-27-51.FPF

**Calibration Parameter:**Sampling Frequency:

Component	$f_s$ [Hz]	Standard deviation [Hz]
X	127.9989	0.000082
Y	127.9985	0.000084
Z	127.9989	0.000075
Mean Sampling Frequency	127.9988	0.000263

3 dB Corner Frequency:

Component	$f_{3\text{dB}}$ [Hz]
X	58.25
Y	58.38
Z	54.46

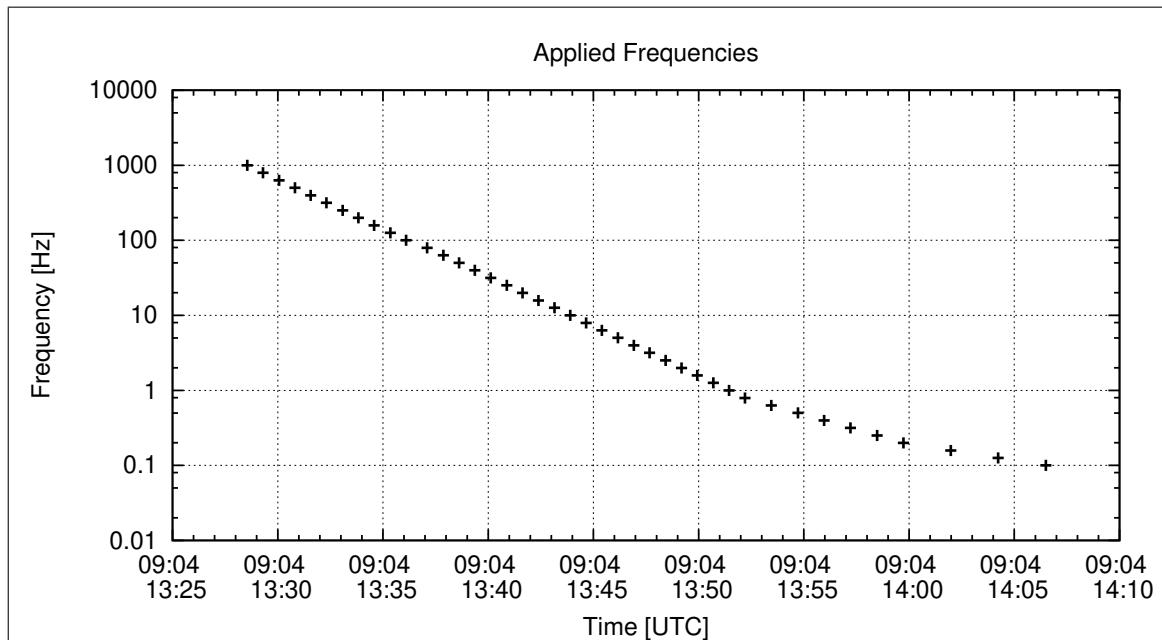
Applied Frequencies and Measured Amplitudes

Figure 46: Applied Frequencies for AC Analysis

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Applied Frequency [Hz]	Bx [enT]	By [enT]	Bz [enT]
1000.000	1.81	1.87	0.67
794.000	9.91	10.20	4.04
631.000	16.17	16.60	7.32
501.000	24.15	24.69	12.07
398.000	19.53	19.89	10.72
316.000	36.29	36.82	21.76
251.000	49.52	50.07	32.29
199.000	104.41	105.27	73.73
158.000	54.73	55.04	41.53
126.000	66.51	66.77	53.69
100.000	152.14	152.01	129.35
79.400	339.62	340.05	300.02
63.100	440.17	440.43	399.99
50.100	513.53	513.25	475.90
39.800	563.29	563.11	529.00
31.600	596.19	595.86	564.80
25.100	618.32	617.90	589.09
19.900	633.19	632.69	605.47
15.800	641.46	640.91	614.80
12.600	646.25	645.68	620.31
10.000	646.92	646.33	621.55
7.900	651.80	651.18	626.62
6.310	650.84	650.22	625.95
5.010	652.41	651.77	627.62
3.980	654.41	651.36	629.71
3.160	653.65	653.00	629.01
2.510	653.75	653.09	629.16
1.990	654.21	653.54	629.65
1.580	656.19	655.53	631.58
1.260	652.68	651.99	628.23
1.000	653.78	653.08	629.30
0.790	656.51	655.82	631.99
0.631	655.29	654.60	630.85
0.501	657.59	656.91	633.03
0.398	657.66	656.97	633.08
0.316	654.58	653.90	630.12
0.251	656.20	655.49	631.65
0.199	656.72	655.98	632.18
0.158	656.96	655.70	632.46
0.126	657.43	656.68	632.95
0.100	658.19	657.42	633.70

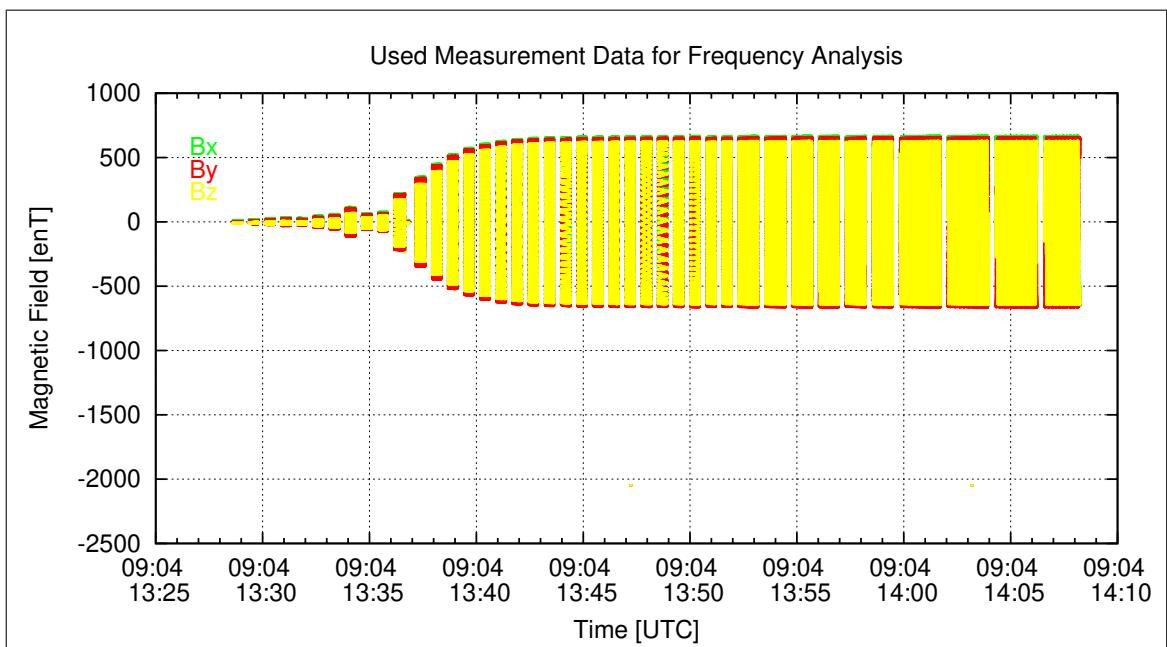


Figure 47: Used packets of Measured data for the Frequency analysis

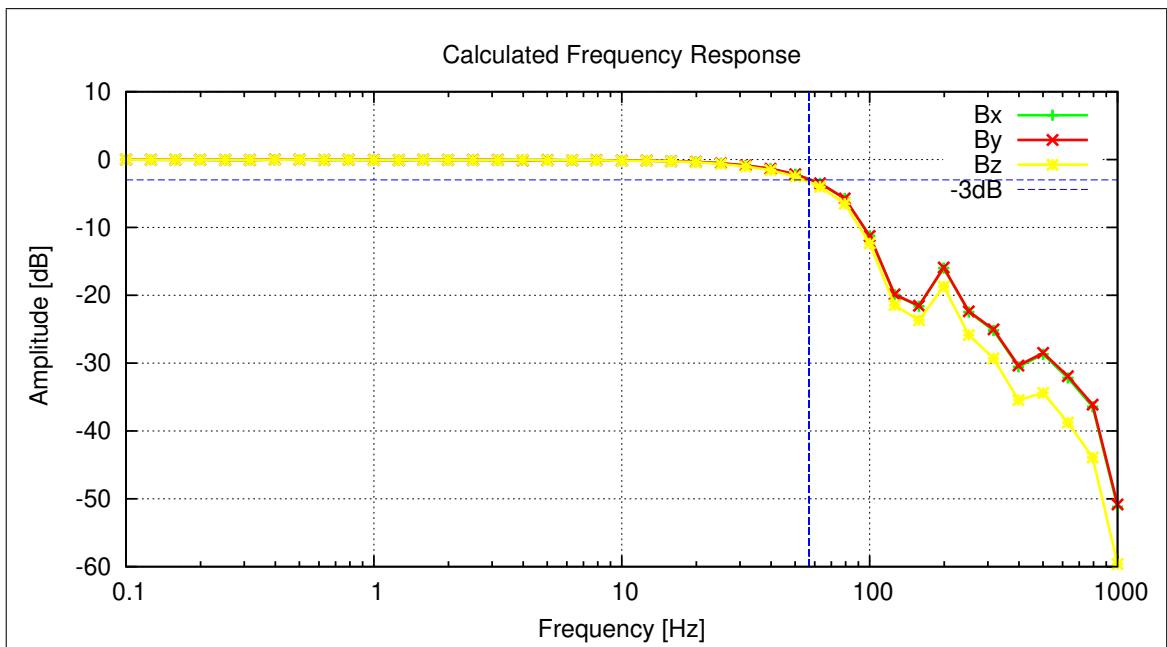


Figure 48: Calculated Frequency Response

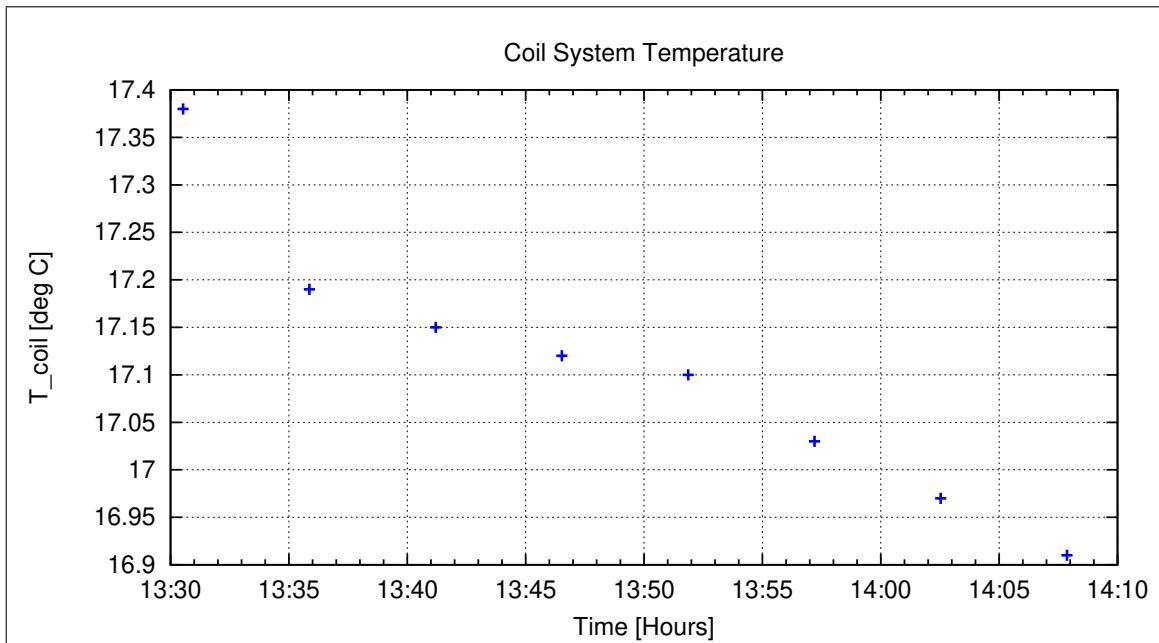


Figure 49: Coil System Temperature

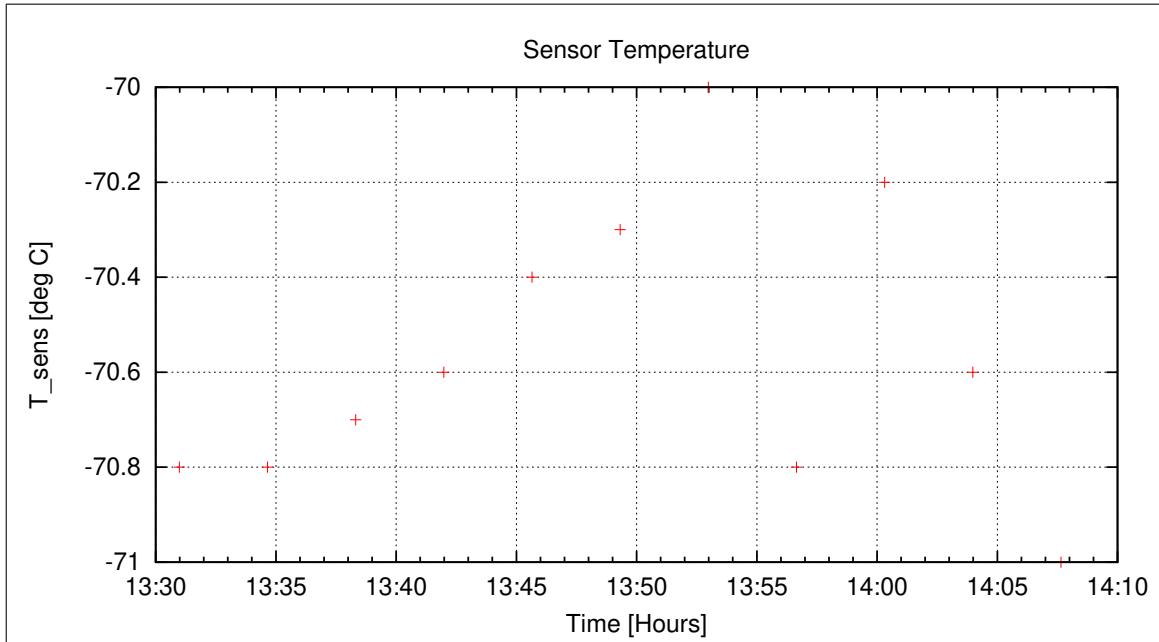


Figure 50: Sensor Temperature

After finishing these measurements the sensor was rotated back to normal orientation and the thermal system was switched off. The temperature will increase smoothly over night.

Over night zerofield measurements in dynamically compensated earthfield conditions were conducted. The IB sensor (at CoC) was operated in the fixed 64 nT range, the OB sensor (in the  $\mu$ -metal shield outside the coilsystem) was set to the 512 nT range.

Measurements started at 14:53.

## 10 Measurements on April 10, 2013

At 06:28 the system was inspected. The measurements have been performing flawlessly during the night. The box temperature has reached a level of  $-14^{\circ}\text{C}$ .

The measurements were stopped and the thermal system was reactivated.  
Temperature goal:  $T_{59} = +30^{\circ}\text{C}$ .

The operating range of the magnetometer has been set back to 2048 nT.

### 10.1 Data

CCD File	Configuration File	Remark
13-04-10\02-54-22.CCR	NULL.MAG	
13-04-10\06-27-43.CCR	NULL.MAG	
13-04-10\06-28-37.CCR	LIN2000XYZE.MAG	
13-04-10\06-58-41.CCR	LIN2000XYZE.MAG	
13-04-10\07-28-44.CCR	LIN2000XYZE.MAG	
13-04-10\07-59-38.CCR	OFFSET_200.MAG	
13-04-10\08-09-57.CCR	OFFSET_200.MAG	
13-04-10\08-18-43.CCR	LIN2000XYZE.MAG	
13-04-10\10-16-52.CCR	LIN2000XYZE.MAG	
13-04-10\10-46-56.CCR	LIN2000XYZE.MAG	
13-04-10\11-17-00.CCR	LIN2000XYZE.MAG	
13-04-10\11-47-03.CCR	LIN2000XYZE.MAG	
13-04-10\12-16-47.CCR	LIN2000XYZE.MAG	
13-04-10\12-17-18.CCR	OFFSET_200.MAG	
13-04-10\12-26-40.CCR	FREQ2000.MAG	
13-04-10\13-11-42.CCR	LIN2000XYZE.MAG	
13-04-10\13-47-06.CCR	OFFSET_200.MAG	
13-04-10\13-56-47.CCR	FREQ2000.MAG	
13-04-10\14-44-30.CCR	NULL_STATISCH.MAG	

## 10.2 DC-Analysis at moderate Temperature - IB Sensor

Linearity and offset measurements were performed at  $T_{59} = +30^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 13.

It turned out that the magnetometer thermistor T\_SENS\_2 shows temperatures being a few degrees to high. Furthermore the value is not stable and jumps by a few degrees. While T\_SENS\_1 showed stable  $22^\circ\text{C}$ , T\_SENS\_2 showed values between 39 and  $48^\circ\text{C}$ .

The instrument was switched off, connectors were swapped, and electronics was rebooted. It showed up that the suspicious value belongs physically to the thermistor T\_SENS\_2 and does not be influenced by the electronics. The sensors were toggled to the nominal connection state. Probably there is a connection problem in the test cable leading from the sensor to the electronics. As this does not really hamper the calibration we decided to proceed with the measurements and to investigate the cable in the institute later.

Afterwards the system was heated up to  $T_{59} = +80^\circ\text{C}$  starting at 10:16.

## 10.3 DC-Analysis at high Temperature - IB Sensor

Linearity and offset measurements were performed at  $T_{59} = +80^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 13.

## 10.4 AC-Analysis at high Temperature - IB Sensor

The sensor was rotated to the diagonal in space orientation and the usual AC measurements were conducted at  $T_{59} = +80^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 13.

Afterward the sensor was rotated back to the standard orientation (POS1).

The thermal system was switched off for smooth cooling during the night. Measurements in fixed compensated zerofield conditions, starting at 14:44, were conducted during the night in cal mode 0. Data were sampled with 128 Hz.

## 11 Measurements on April 11, 2013

At 06:30 the system was inspected. The measurements have been performing flawlessly during the night. The box temperature has dropped to  $T_{59} = +39.4^\circ\text{C}$ .

The measurements were stopped and the thermal system was reactivated. Temperature goal  $T_{59} = +130^\circ\text{C}$ .

### 11.1 Data

CCD File	Configuration File	Remark
13-04-11\06-36-24.CCR	LIN2000XYZE.MAG	
13-04-11\07-06-27.CCR	LIN2000XYZE.MAG	
13-04-11\07-36-30.CCR	LIN2000XYZE.MAG	
13-04-11\08-06-33.CCR	LIN2000XYZE.MAG	
13-04-11\08-37-21.CCR	OFFSET_200.MAG	
13-04-11\08-46-10.CCR	FREQ2000.MAG	
13-04-11\09-31-53.CCR	LIN2000XYZE.MAG	
13-04-11\10-11-50.CCR	OFFSET_200.MAG	
13-04-11\10-20-53.CCR	FREQ2000.MAG	
13-04-11\11-05-33.CCR	LIN2000XYZE.MAG	
13-04-11\11-35-36.CCR	LIN2000XYZE.MAG	
13-04-11\12-05-40.CCR	LIN2000XYZE.MAG	
13-04-11\12-35-43.CCR	LIN2000XYZE.MAG	
13-04-11\13-06-41.CCR	LIN2000XYZE.MAG	
13-04-11\13-37-03.CCR	OFFSET_200.MAG	
13-04-11\13-45-45.CCR	FREQ2000.MAG	
13-04-11\14-42-54.CCR	LIN2000XYZE.MAG	
13-04-11\14-47-36.CCR	LIN2000XYZE.MAG	
13-04-11\15-18-03.CCR	OFFSET_200.MAG	
13-04-11\15-26-22.CCR	FREQ2000.MAG	

### 11.2 DC-Analysis at very high Temperature - IB Sensor

Linearity and offset measurements were performed at  $T_{59} = +130^\circ\text{C}$  in cal mode 4 and cal mode 0 starting at 08:06.

Thermal Analysis: refer to section 13.

### 11.3 AC-Analysis at very high Temperature - IB Sensor

The sensor was rotated to the diagonal in space orientation and the usual AC measurements were conducted at  $T_{59} = +130^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 13.

Afterwards the thermal box was heated up to the final temperature of  $+180^\circ\text{C}$ .

### 11.4 DC-Analysis at highest Temperature - IB Sensor

Linearity and offset measurements were performed at  $T_{59} = +180^\circ\text{C}$  in cal mode 4 and cal mode 0 starting at 13:06.

Thermal Analysis: refer to section 13.

### 11.5 AC-Analysis at highest Temperature - IB Sensor

The sensor was rotated to the diagonal in space orientation and the usual AC measurements were conducted at  $T_{59} = +180^\circ\text{C}$  in cal mode 4 and cal mode 0.

Thermal Analysis: refer to section 13.

Afterwards the thermal system was switched off to let the temperature fall smoothly. Over night and for the next days zerofield measurements in fixed compensated earthfield conditions were conducted in science mode.

Sensor alignment: Standard, Azimuth = $180^\circ$ , Elevation= $0^\circ$ .

Data collection by EGSE only.

The measurements started at 16:16.

From the calibration point of view the campaign for the IB sensor is finished now.

## 12 Combined Measurements from April 3 – 9, 2013

### 12.1 Thermal-Analysis - OB Sensor, cal mode 0

#### 12.1.1 Temperature Calibration on Linear Axes

##### Used Temperature Measurements:

Calibration Parameter File	Remark
PARAMETER_TEMPLIN__13-04-03_09-22-38.CPF	
PARAMETER_TEMPLIN__13-04-03_12-16-15.CPF	
PARAMETER_TEMPLIN__13-04-04_08-08-11.CPF	
PARAMETER_TEMPLIN__13-04-04_09-51-19.CPF	
PARAMETER_TEMPLIN__13-04-04_14-55-20.CPF	
PARAMETER_TEMPLIN__13-04-08_08-29-20.CPF	
PARAMETER_TEMPLIN__13-04-08_15-06-16.CPF	

Thermal Parameter File: THERMAL\_PARAMETER\_\_13-04-03-09-22-38.TPF

**Facility Parameter:**Nominal Sensor Setup  $B_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} B_{\text{c}}$ 

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Initial Sensor Rotation:

$$\underline{\underline{R}} = \begin{pmatrix} +0.999800 & +0.018895 & +0.006519 \\ -0.018810 & +0.999740 & -0.012858 \\ -0.006760 & +0.012733 & +0.999896 \end{pmatrix}$$

Initial Rotation Angles:

$$\begin{aligned} \text{Rotation @ X: } \lambda_x &= +1^\circ 8'43'' \\ \text{Rotation @ Y: } \mu_y &= +1^\circ 18'20'' \\ \text{Rotation @ Z: } \nu_z &= +0^\circ 49'34'' \end{aligned}$$

Determinant of Rotation Matrix: 1.0000

Nominal Field Source: FLDS

Automatic Coil correction: used

Used Sensor-Temperature-Channel:  $T_{59}$

## Temperature Profile

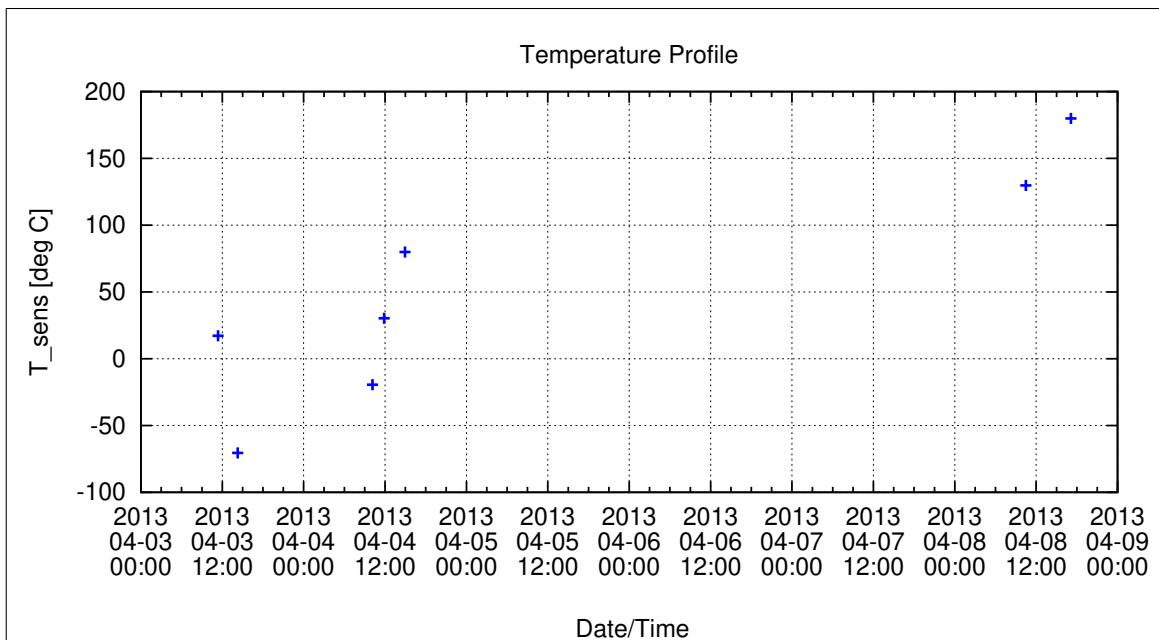


Figure 51: Temperature Profile

**Calibration Parameter:**Sensitivity  $\sigma_i$  vs. Temperature:

$$\sigma_i(T) = \sum_{k=0}^n \sigma_{k,i} T^k \quad [1, {}^\circ\text{C}], i=\{\text{x,y,z}\}$$

	$\sigma_{0,i}$	$\sigma_{1,i}$	$\sigma_{2,i}$	$\sigma_{3,i}$	$\sigma_{4,i}$	$\sigma_{5,i}$
$\sigma_x$	9.72692E-1	-1.80180E-5				
$\sigma_y$	9.96420E-1	-1.56674E-5				
$\sigma_z$	9.89066E-1	-1.96816E-5				

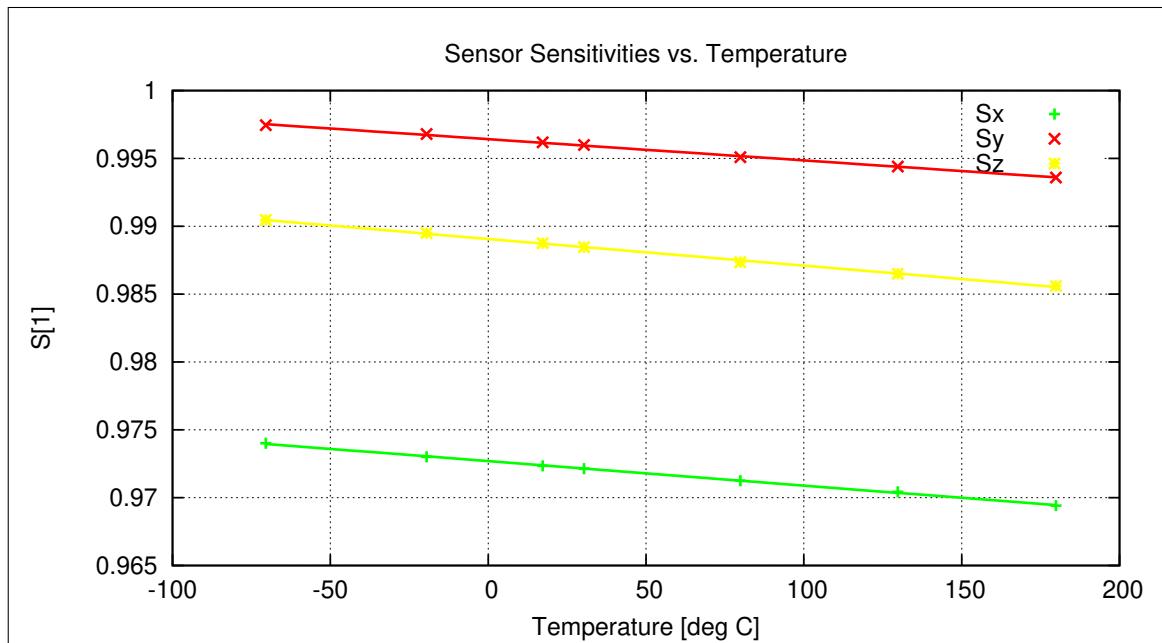


Figure 52: Temperature dependence of Sensitivities

Misalignment Angles  $\xi_{ij}$  vs. Temperature:

$$\xi_{ij}(T) = \sum_{k=0}^n \xi_{k,ij} T^k \quad [\text{deg, } ^\circ\text{C}], \text{ ij} = \{\text{xy}, \text{xz}, \text{yz}\}$$

	$\xi_{0,ij}$	$\xi_{1,ij}$	$\xi_{2,ij}$	$\xi_{3,ij}$	$\xi_{4,ij}$	$\xi_{5,ij}$
$\xi_{xy}$	8.9789E+1	-1.7948E-5				
$\xi_{xz}$	9.0056E+1	4.5473E-5				
$\xi_{yz}$	9.0013E+1	-1.1504E-4				

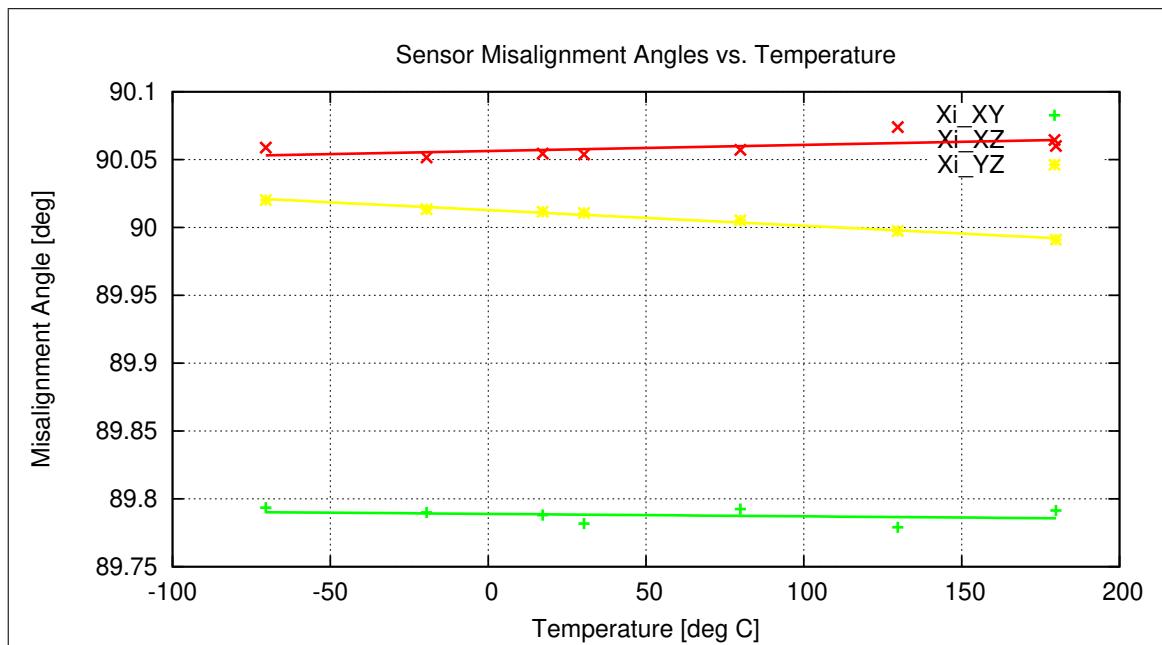


Figure 53: Temperature dependence of Misalignment Angles

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Offset & Residual MCF Field  $\underline{B}^{or} = \underline{B}^{off} + \underline{B}^{res}$  vs. Temperature:

$$\underline{B}^{or}(T) = \sum_{k=0}^n \underline{B}_k^{or} T^k \quad [\text{enT}, {}^\circ\text{C}]$$

	$\underline{B}_0^{or}$	$\underline{B}_1^{or}$	$\underline{B}_2^{or}$	$\underline{B}_3^{or}$	$\underline{B}_4^{or}$	$\underline{B}_5^{or}$
$B_x^{or}$	-1.038E+0	5.086E-3	1.028E-4	-8.062E-7		
$B_y^{or}$	4.990E-1	4.459E-4	2.056E-4	-9.631E-7		
$B_z^{or}$	-9.215E+0	-4.711E-3	-1.042E-4	8.416E-7		

Model Quality:

Minimum and maximum errors of the calculated Model vs. Temperature:

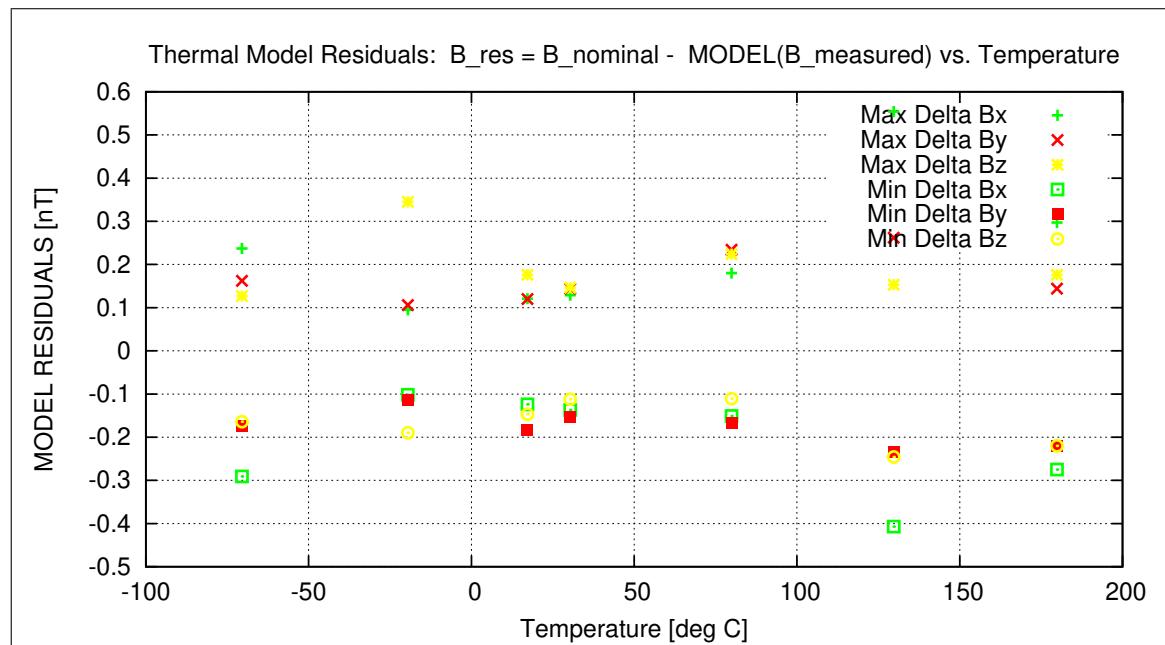


Figure 54: Residuals of Thermal Model

Sensor Rotation during Test:

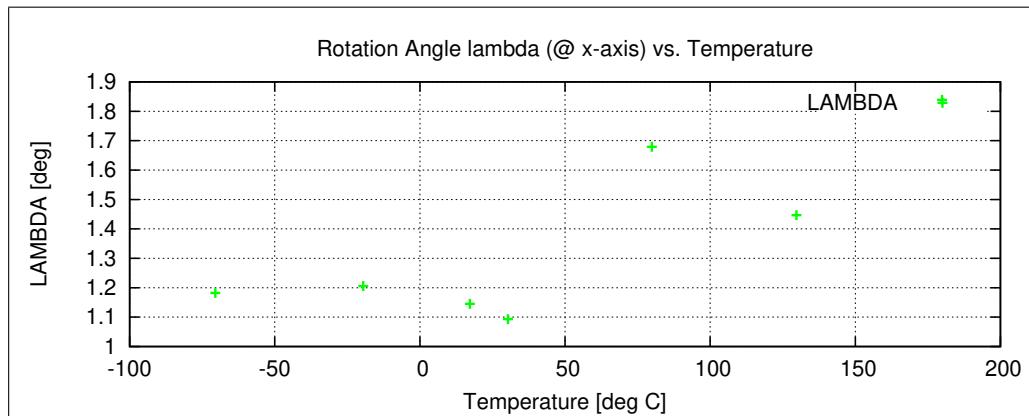


Figure 55: Rotation @ X-Axis

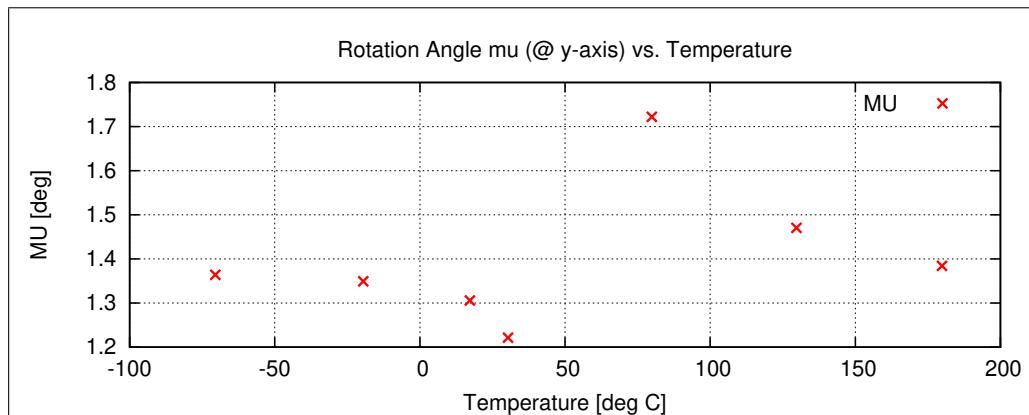


Figure 56: Rotation @ Y-Axis

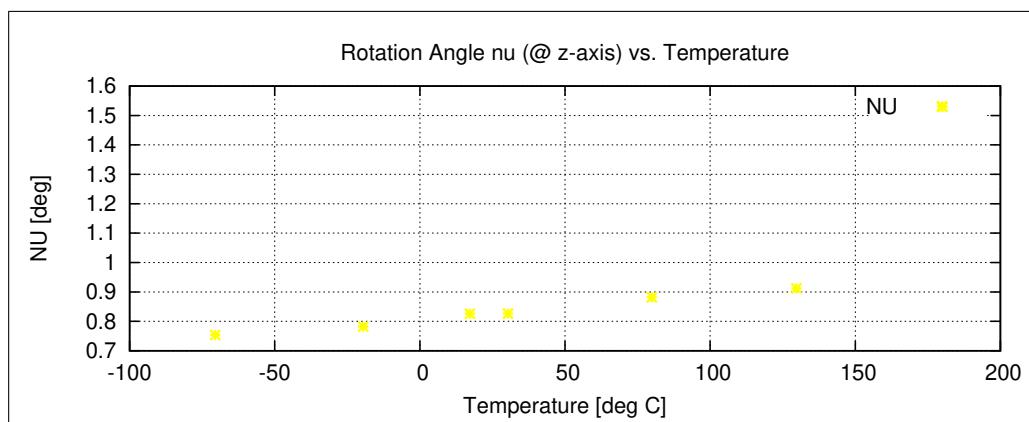


Figure 57: Rotation @ Z-Axis

**12.1.2 Temperature Calibration of the Sensor Offset****Used Temperature Measurements:**

Calibration Parameter File	Remark
OFF_PARAMETER__13-04-03-09-53-35.OPF	
OFF_PARAMETER__13-04-03-12-47-57.OPF	
OFF_PARAMETER__13-04-04-08-39-48.OPF	
OFF_PARAMETER__13-04-04-10-26-52.OPF	
OFF_PARAMETER__13-04-04-15-26-56.OPF	
OFF_PARAMETER__13-04-08-09-30-44.OPF	
OFF_PARAMETER__13-04-08-15-36-36.OPF	

Thermal Parameter File: THERMAL\_OFF\_PARAMETER\_\_13-04-03-09-53-35.TOF

**Facility Parameter:**Nominal Sensor Setup  $B_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} B_{\text{c}}$ 

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

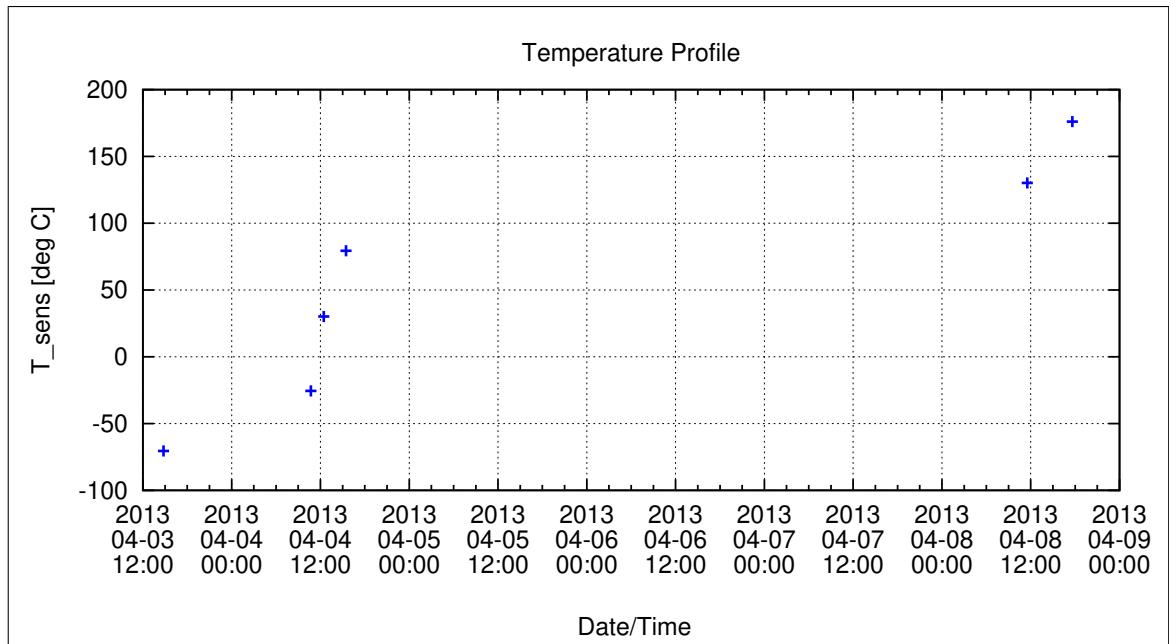
Sensor Temperature Channel: T<sub>59</sub>Coil System Temperature Channel: T<sub>29</sub>**Temperature Profile**

Figure 58: Temperature Profile

**Calibration Parameter:**Sensor Offset  $B_{\text{off}}$  vs. Temperature:

$$B_{\text{off},i}(T) = \sum_{k=0}^n B_{\text{off},k,i} T^k \quad [\text{enT}, \text{ } ^\circ\text{C}], i=\{\text{x,y,z}\}$$

	$B_{\text{off},0,i}$	$B_{\text{off},1,i}$	$B_{\text{off},2,i}$	$B_{\text{off},3,i}$	$B_{\text{off},4,i}$	$B_{\text{off},5,i}$
$B_{\text{off},x}$	-1.81567E-1	2.66715E-3	6.76985E-5	-4.57147E-7		
$B_{\text{off},y}$	1.12886E+0	-2.66713E-3	8.93650E-5	-2.48924E-7		
$B_{\text{off},z}$	1.32950E+0	1.18837E-3	-1.17584E-5	1.39437E-7		

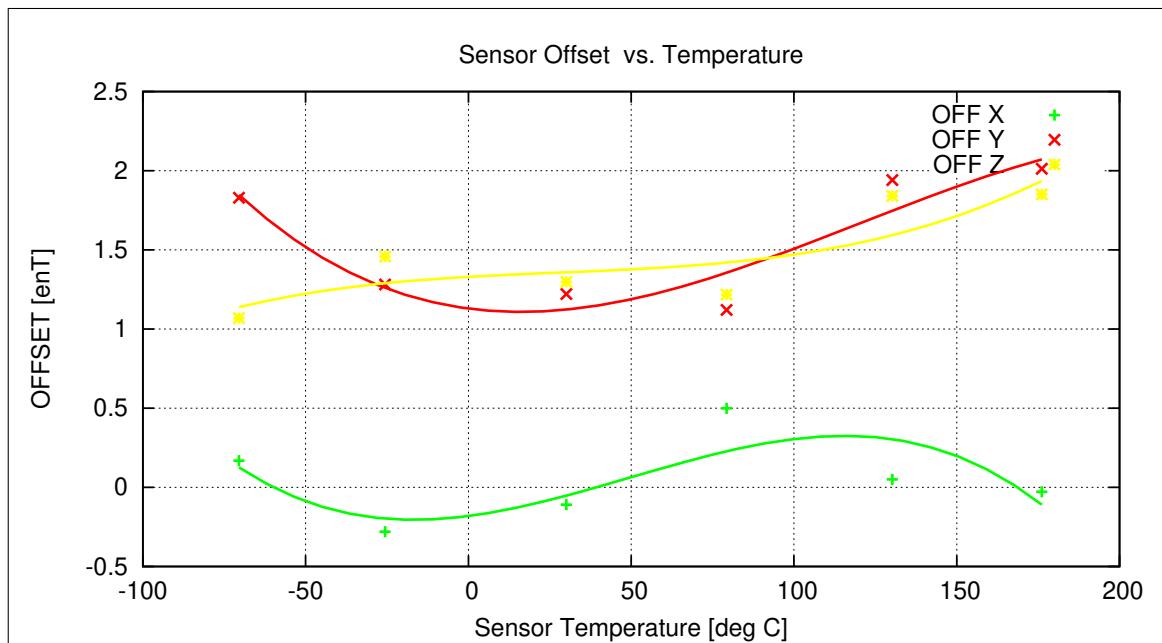


Figure 59: Temperature dependence of Sensor Offsets

## Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the offset measurements.

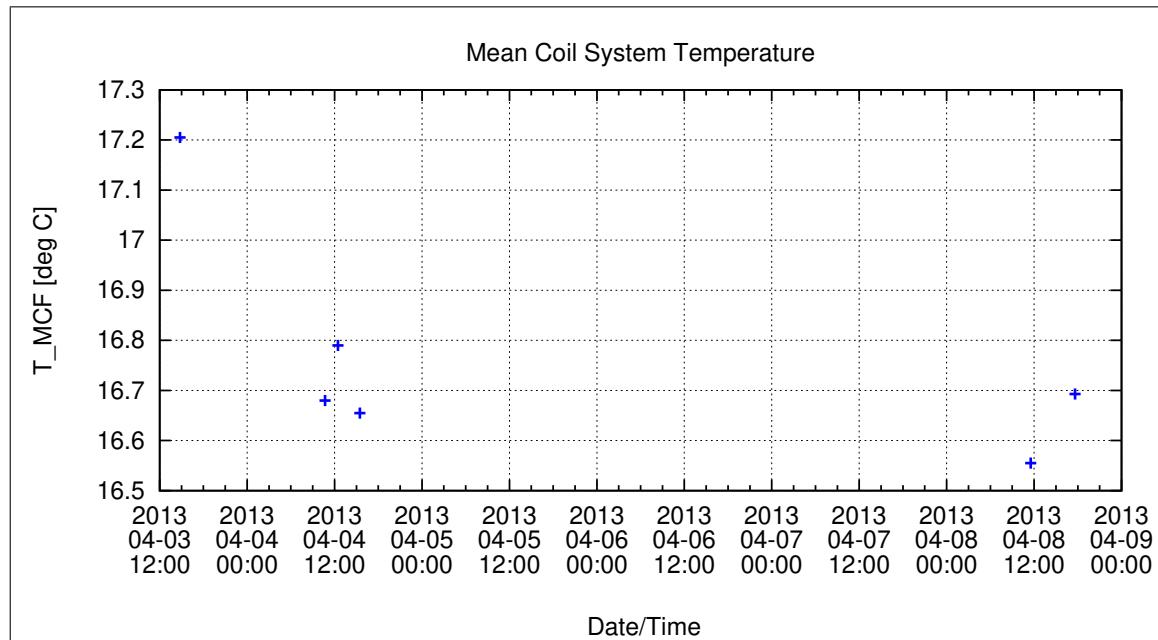


Figure 60: Coil System Temperature during Thermal Measurements

Coil System Residual Field:

The following graph shows the three components of the Coil System Residual field during the whole measurement. Axes designators are related to the actual DUT coordinate system and NOT to Coil System coordinates.

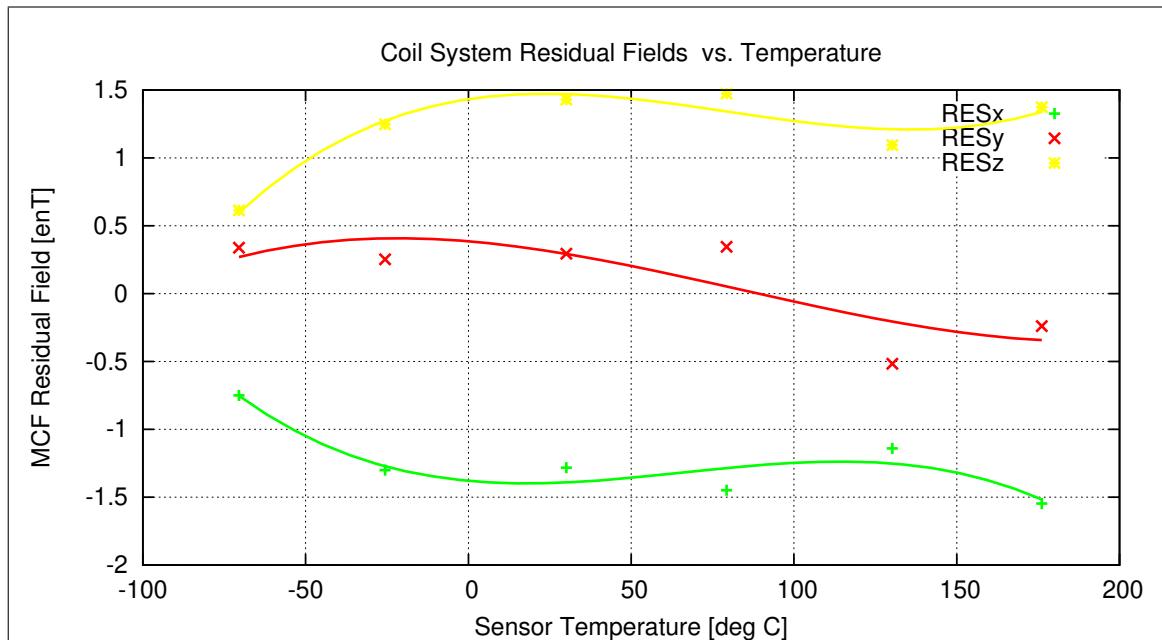


Figure 61: Coil System Residual Fields during Thermal Measurements

**Remark:**

The axes designation for this graph is given as follows (rf. to setup defined in chapter 1):

$$\begin{aligned} X_m &= X_c \\ Y_m &= Y_c \\ Z_m &= -X_c \end{aligned}$$

**12.1.3 Temperature Calibration of the AC Transfer Function****Used Temperature Measurements:**

Calibration Parameter File	Remark
FREQ_PARAMETER__13-04-03-12-59-48.FPF	
FREQ_PARAMETER__13-04-04-14-11-50.FPF	
FREQ_PARAMETER__13-04-08-09-40-37.FPF	
FREQ_PARAMETER__13-04-08-15-46-19.FPF	

Thermal Parameter File: THERMAL\_AC\_PARAMETER\_\_13-04-03-12-59-48.TAF

### Facility Parameter:

Nominal Sensor Setup: Diagonal in Space inside Thermal Box.

Sensor Temperature Channel: T<sub>59</sub>

Coil System Temperature Channel: T<sub>29</sub>

### Temperature Profile

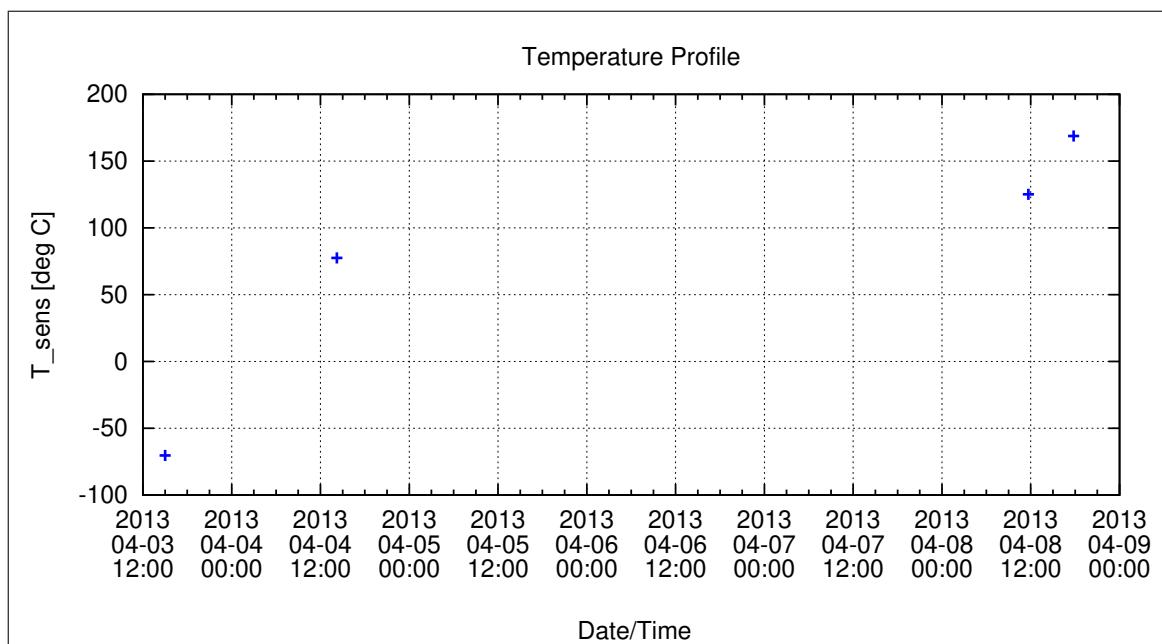


Figure 62: Temperature Profile

## Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the AC measurements.

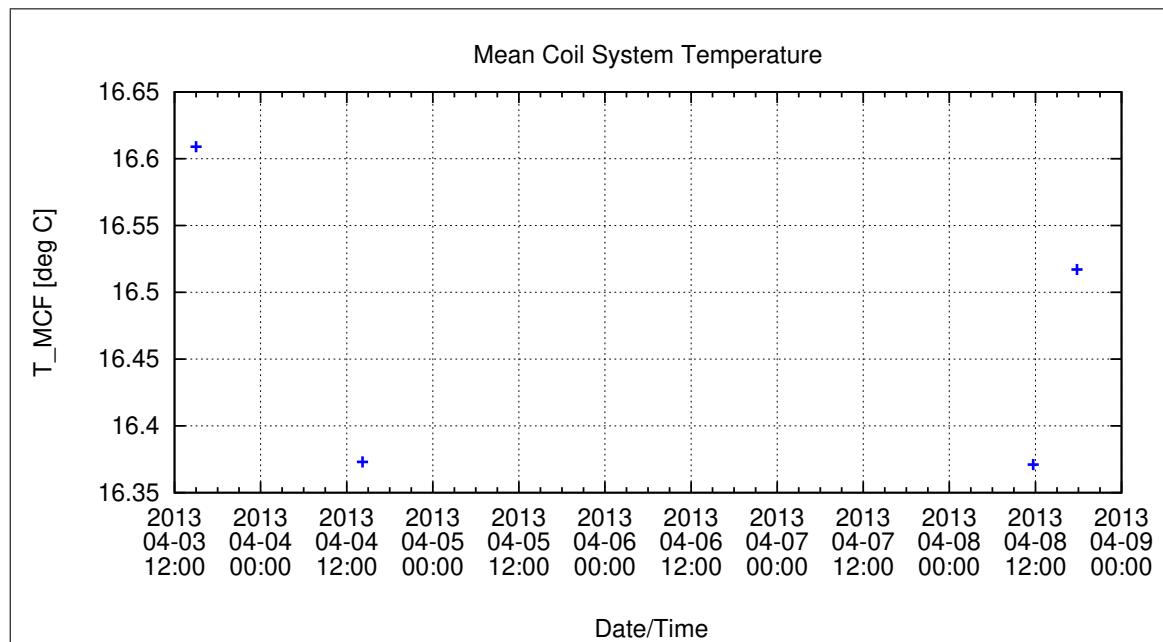


Figure 63: Coil System Temperature during Thermal AC Measurements

**Calibration Parameter:**-3dB Corner Frequency  $f_{3\text{dB}}$  vs. Temperature:

$$f_{3\text{dB},i}(T) = \sum_{k=0}^n f_{3\text{dB},k,i} T^k \quad [\text{Hz}, \text{ } ^\circ\text{C}], \ i=\{\text{x,y,z}\}$$

	$f_{3\text{dB},0,i}$	$f_{3\text{dB},1,i}$	$f_{3\text{dB},2,i}$	$f_{3\text{dB},3,i}$	$f_{3\text{dB},4,i}$	$f_{3\text{dB},5,i}$
$f_{3\text{dB},x}$	5.82762E+1	-7.55338E-2				
$f_{3\text{dB},y}$	5.67012E+1	-9.12999E-2				
$f_{3\text{dB},z}$	5.37114E+1	-2.50266E-2				

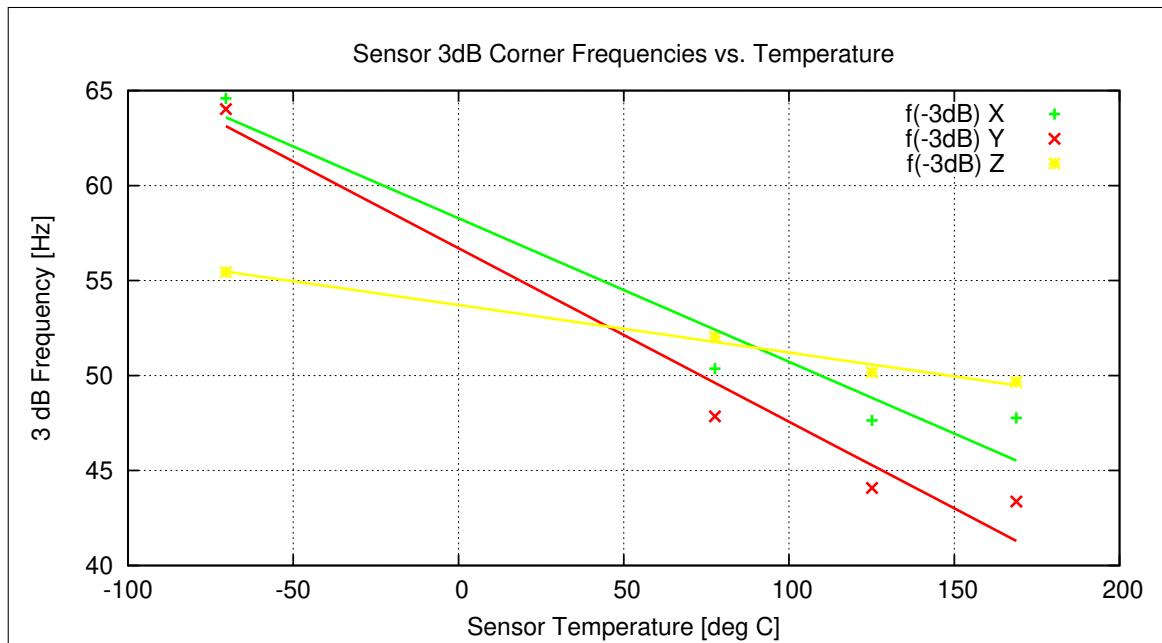


Figure 64: Temperature dependence of 3dB Corner Frequency

Instrument Sampling Frequency:

The following graph shows the calculated sampling frequencies vs. the actual sensor temperature.

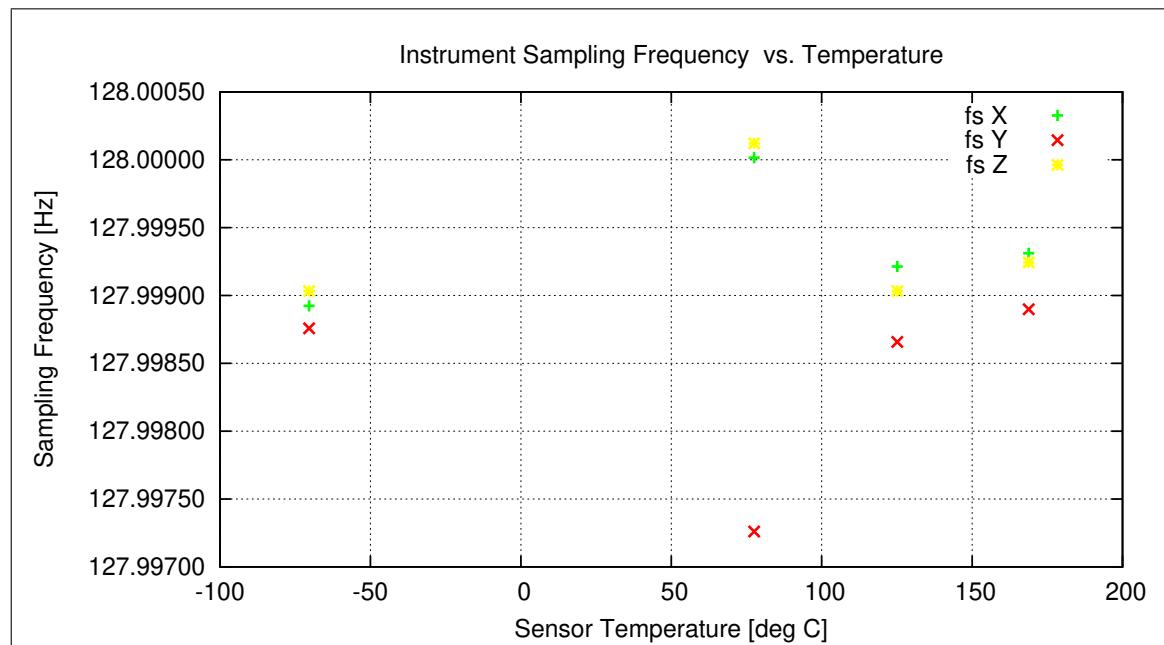


Figure 65: Instrument Sampling Frequency versus Sensor Temperature

Mean Samplerate: 127.999039 Hz.

Mean Standard Deviation of Samplerate: 0.000122 Hz.

## 12.2 Thermal-Analysis - OB Sensor, cal mode 4

### 12.2.1 Temperature Calibration on Linear Axes

#### Used Temperature Measurements:

Calibration Parameter File	Remark
PARAMETER_TEMPLIN__13-04-03_15-24-42.CPF	
PARAMETER_TEMPLIN__13-04-04_07-18-40.CPF	
PARAMETER_TEMPLIN__13-04-04_10-51-43.CPF	
PARAMETER_TEMPLIN__13-04-04_12-34-10.CPF	
PARAMETER_TEMPLIN__13-04-08_11-15-40.CPF	
PARAMETER_TEMPLIN__13-04-08_13-25-22.CPF	

Thermal Parameter File: THERMAL\_PARAMETER\_\_13-04-03-15-24-42.TPF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Initial Sensor Rotation:

$$\underline{\underline{R}} = \begin{pmatrix} +0.999400 & +0.033623 & +0.008371 \\ -0.033527 & +0.999374 & -0.011332 \\ -0.008747 & +0.011044 & +0.999901 \end{pmatrix}$$

Initial Rotation Angles:

$$\text{Rotation @ X: } \lambda_x = +1^\circ 59'8''$$

$$\text{Rotation @ Y: } \mu_y = +2^\circ 1'41''$$

$$\text{Rotation @ Z: } \nu_z = +0^\circ 48'26''$$

Determinant of Rotation Matrix: 1.0000

Nominal Field Source: SOLARTRON

Automatic Coil correction: used

Used Sensor-Temperature-Channel:  $T_{59}$

## Temperature Profile

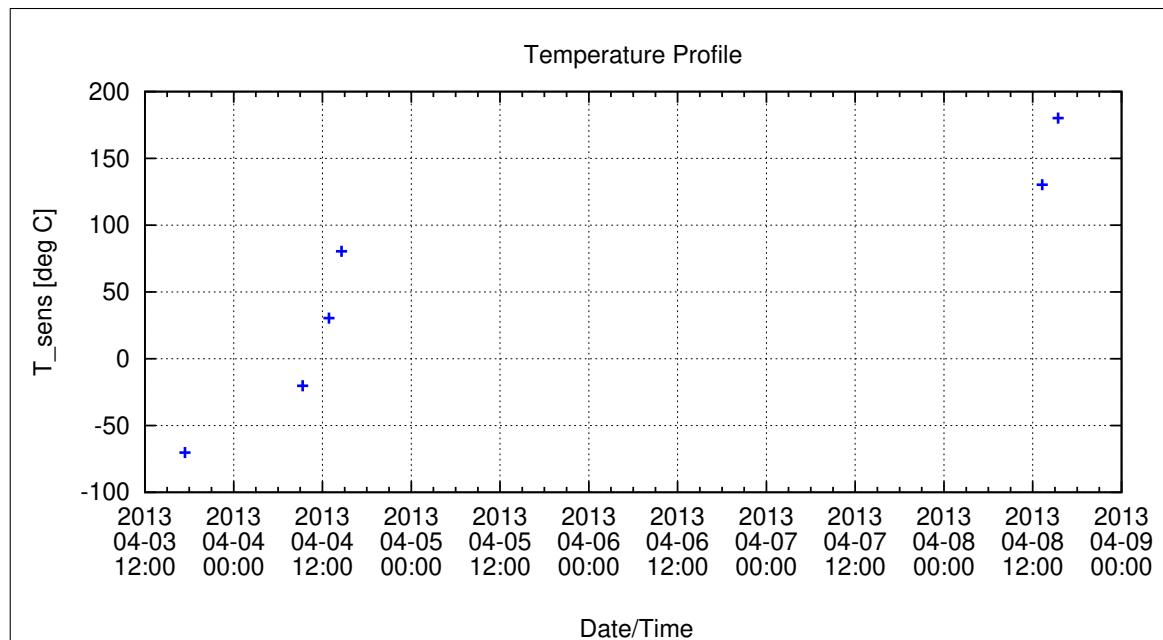


Figure 66: Temperature Profile

**Calibration Parameter:**Sensitivity  $\sigma_i$  vs. Temperature:

$$\sigma_i(T) = \sum_{k=0}^n \sigma_{k,i} T^k \quad [1, {}^\circ\text{C}], \quad i=\{\text{x,y,z}\}$$

	$\sigma_{0,i}$	$\sigma_{1,i}$	$\sigma_{2,i}$	$\sigma_{3,i}$	$\sigma_{4,i}$	$\sigma_{5,i}$
$\sigma_x$	9.97312E-1	8.41537E-4	-2.34026E-6			
$\sigma_y$	1.01904E+0	9.92588E-4	-2.21768E-6			
$\sigma_z$	9.81879E-1	6.63730E-4	-1.40862E-6			

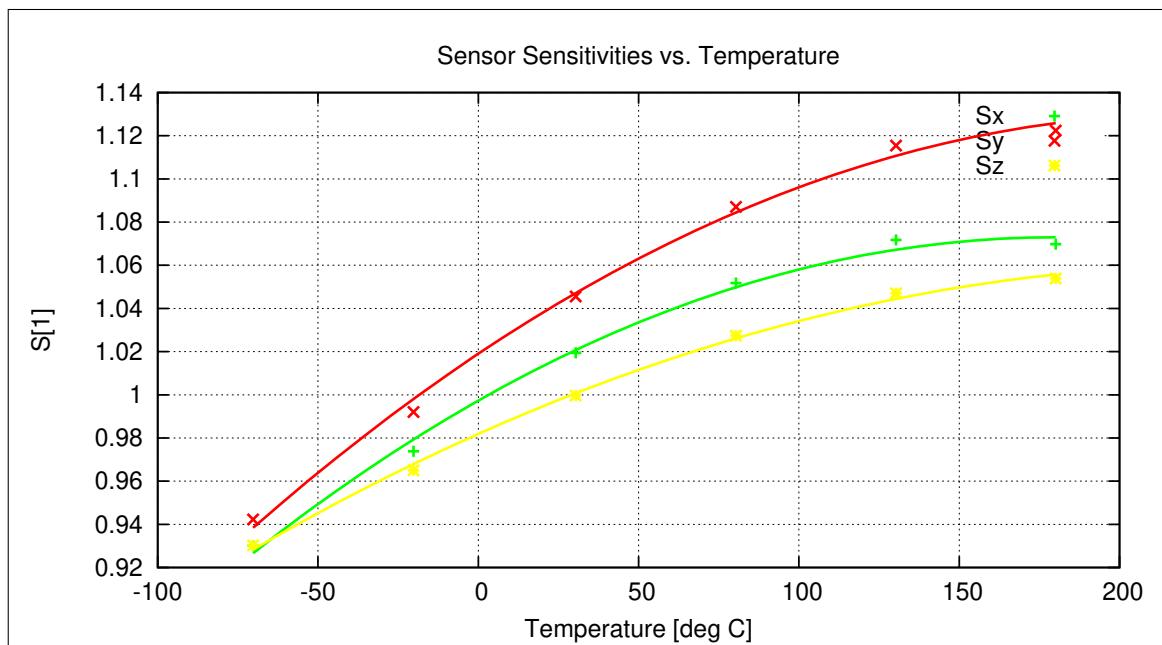


Figure 67: Temperature dependence of Sensitivities

Misalignment Angles  $\xi_{ij}$  vs. Temperature:

$$\xi_{ij}(T) = \sum_{k=0}^n \xi_{k,ij} T^k \quad [\text{deg, } ^\circ\text{C}], \text{ ij} = \{\text{xy}, \text{xz}, \text{yz}\}$$

	$\xi_{0,ij}$	$\xi_{1,ij}$	$\xi_{2,ij}$	$\xi_{3,ij}$	$\xi_{4,ij}$	$\xi_{5,ij}$
$\xi_{xy}$	9.0578E+1	1.4757E-3	-5.1834E-6			
$\xi_{xz}$	8.9782E+1	-4.0098E-4	2.5339E-6			
$\xi_{yz}$	9.0109E+1	-4.8477E-4	5.5736E-7			

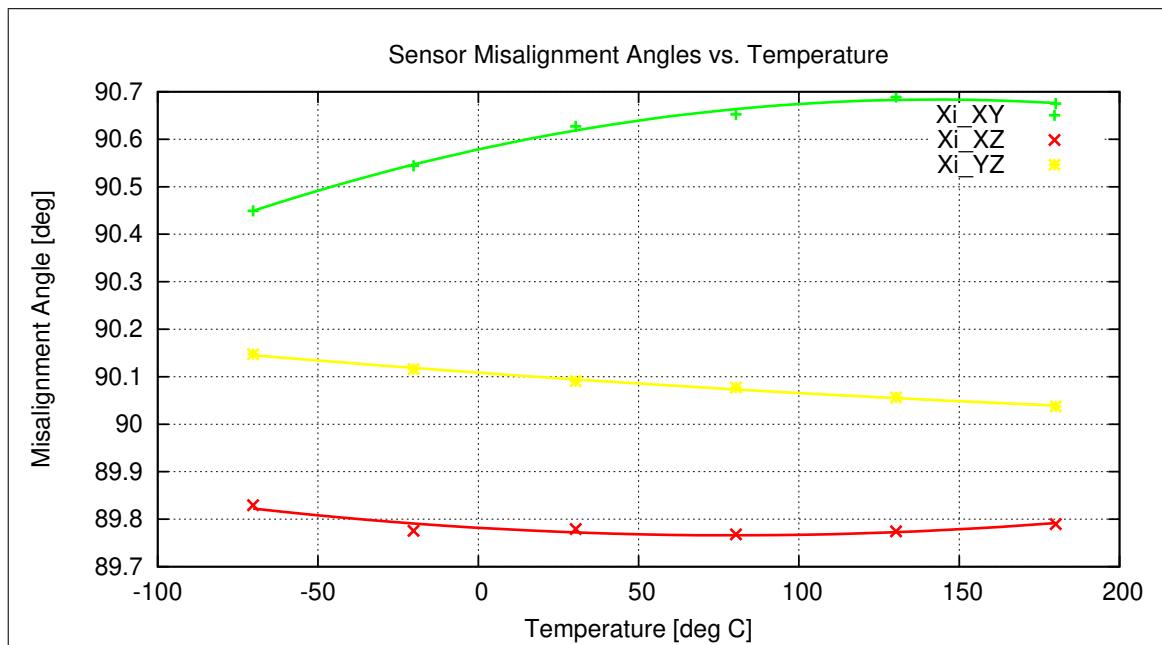


Figure 68: Temperature dependence of Misalignment Angles

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Offset & Residual MCF Field  $\underline{B}^{or} = \underline{B}^{off} + \underline{B}^{res}$  vs. Temperature:

$$\underline{B}^{or}(T) = \sum_{k=0}^n \underline{B}_k^{or} T^k \quad [\text{enT}, {}^\circ\text{C}]$$

	$\underline{B}_0^{or}$	$\underline{B}_1^{or}$	$\underline{B}_2^{or}$	$\underline{B}_3^{or}$	$\underline{B}_4^{or}$	$\underline{B}_5^{or}$
$B_x^{or}$	-1.154E+0	4.076E-3	5.321E-5	-5.044E-7		
$B_y^{or}$	9.191E-1	-4.584E-3	1.387E-4	-5.106E-7		
$B_z^{or}$	-9.347E+0	9.076E-3	-7.507E-5	3.609E-7		

Model Quality:

Minimum and maximum errors of the calculated Model vs. Temperature:

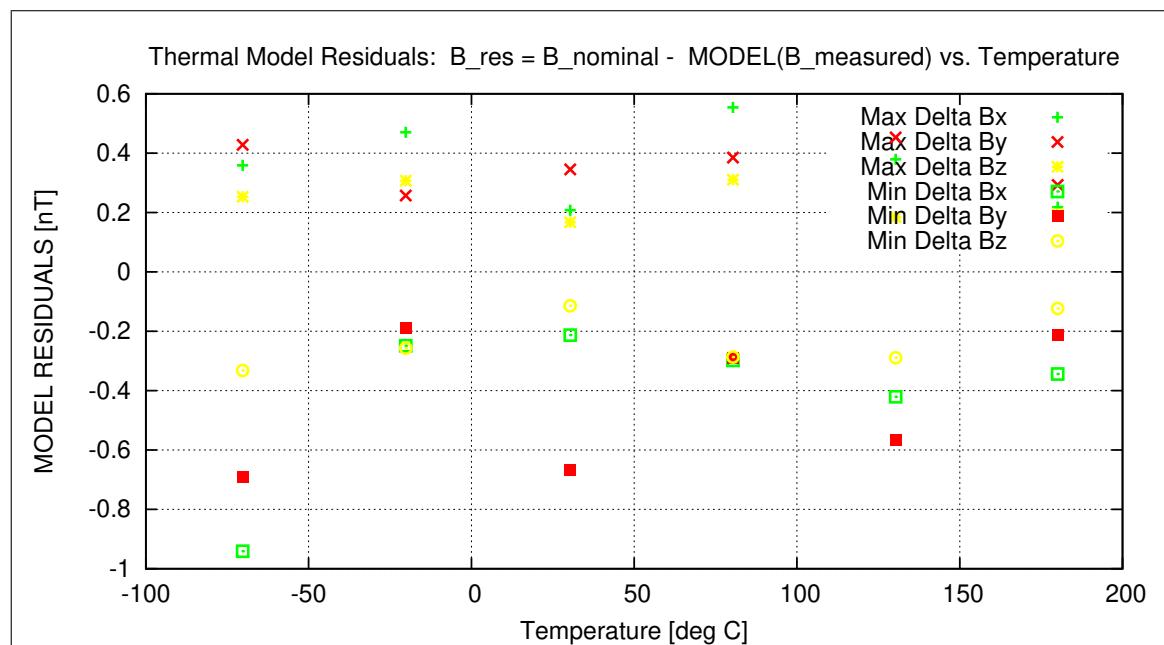


Figure 69: Residuals of Thermal Model

Sensor Rotation during Test:

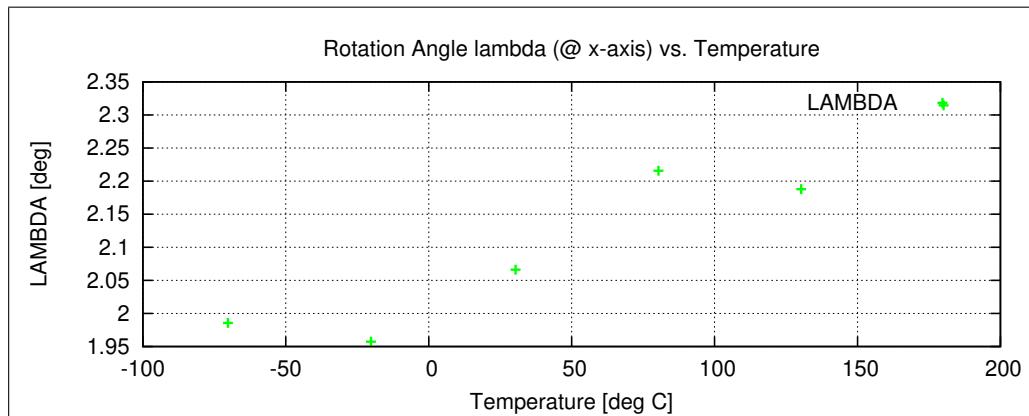


Figure 70: Rotation @ X-Axis

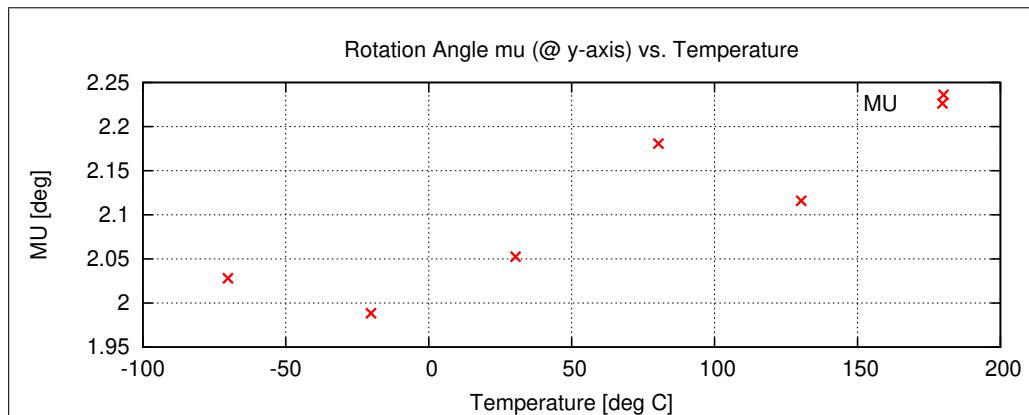


Figure 71: Rotation @ Y-Axis

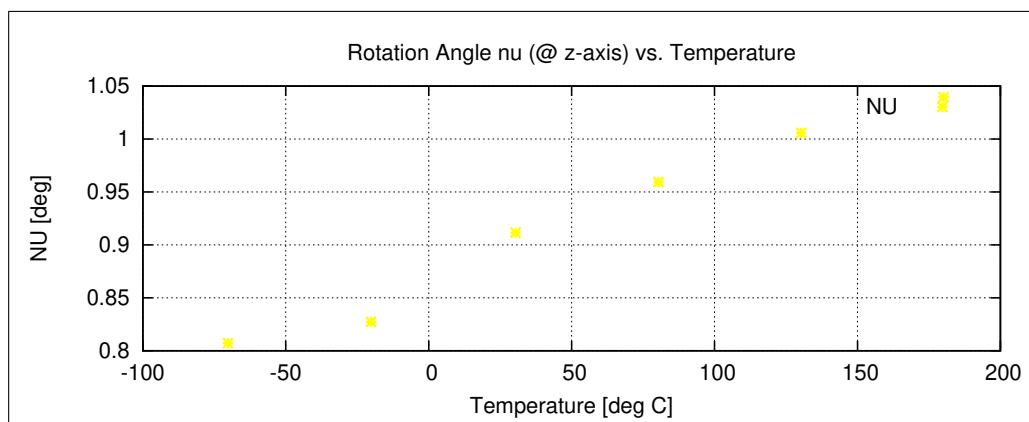


Figure 72: Rotation @ Z-Axis

**12.2.2 Temperature Calibration of the Sensor Offset****Used Temperature Measurements:**

Calibration Parameter File	Remark
OFF_PARAMETER__13-04-03-15-55-48.OPF	
OFF_PARAMETER__13-04-04-07-54-10.OPF	
OFF_PARAMETER__13-04-04-11-22-26.OPF	
OFF_PARAMETER__13-04-04-13-05-27.OPF	
OFF_PARAMETER__13-04-08-11-46-06.OPF	
OFF_PARAMETER__13-04-08-13-56-15.OPF	

Thermal Parameter File: THERMAL\_OFF\_PARAMETER\_\_13-04-03-15-55-48.TOF

**Facility Parameter:**Nominal Sensor Setup  $B_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{\underline{B}}_{\text{c}}$ 

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

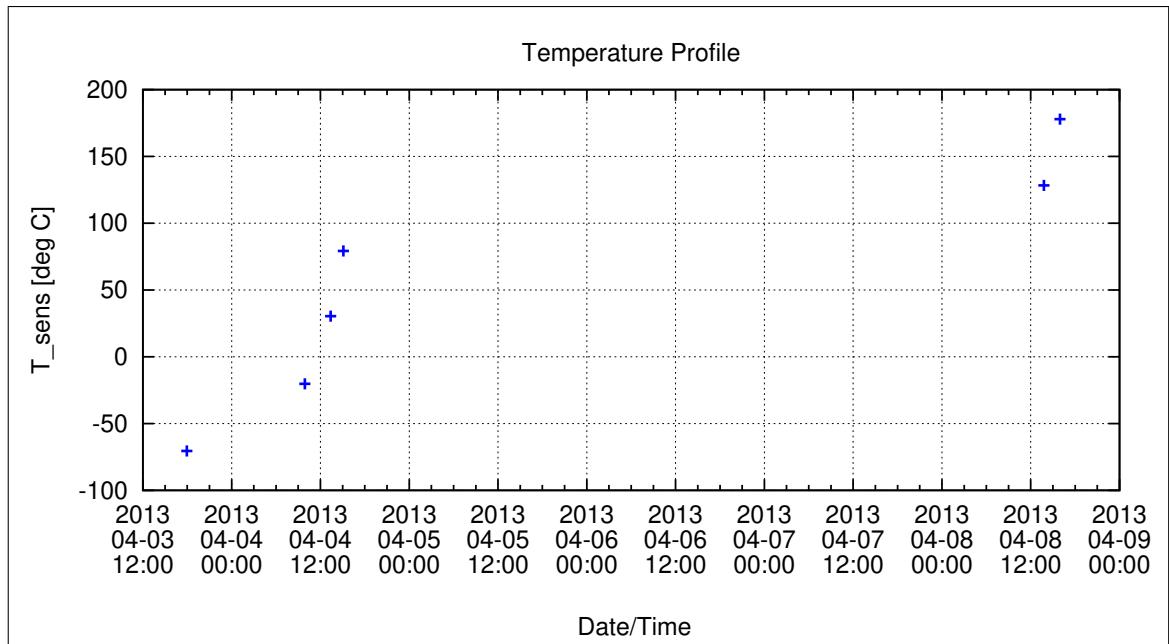
Sensor Temperature Channel: T<sub>59</sub>Coil System Temperature Channel: T<sub>29</sub>**Temperature Profile**

Figure 73: Temperature Profile

**Calibration Parameter:**Sensor Offset  $B_{\text{off}}$  vs. Temperature:

$$B_{\text{off},i}(T) = \sum_{k=0}^n B_{\text{off},k,i} T^k \quad [\text{enT}, \text{ } ^\circ\text{C}], i=\{\text{x,y,z}\}$$

	$B_{\text{off},0,i}$	$B_{\text{off},1,i}$	$B_{\text{off},2,i}$	$B_{\text{off},3,i}$	$B_{\text{off},4,i}$	$B_{\text{off},5,i}$
$B_{\text{off},x}$	-2.11499E-1	3.43452E-3	3.65776E-5	-3.04488E-7		
$B_{\text{off},y}$	9.20378E-1	-4.22661E-3	1.35052E-4	-4.54142E-7		
$B_{\text{off},z}$	1.60582E+0	1.55047E-3	-5.85991E-5	3.47774E-7		

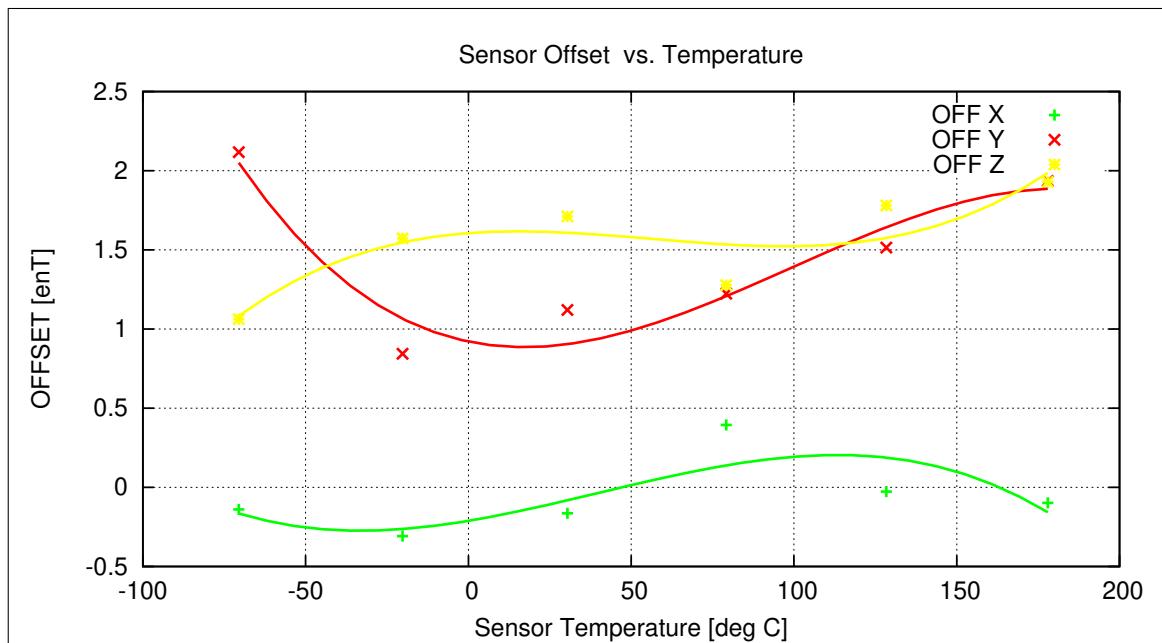


Figure 74: Temperature dependence of Sensor Offsets

## Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the offset measurements.

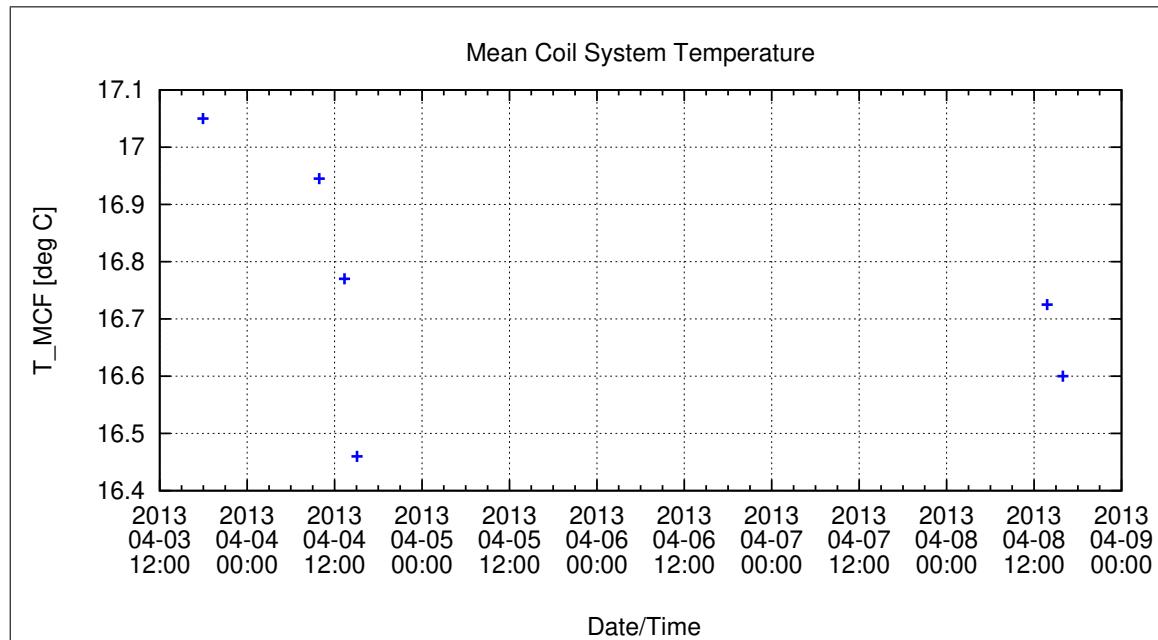


Figure 75: Coil System Temperature during Thermal Measurements

Coil System Residual Field:

The following graph shows the three components of the Coil System Residual field during the whole measurement. Axes designators are related to the actual DUT coordinate system and NOT to Coil System coordinates.

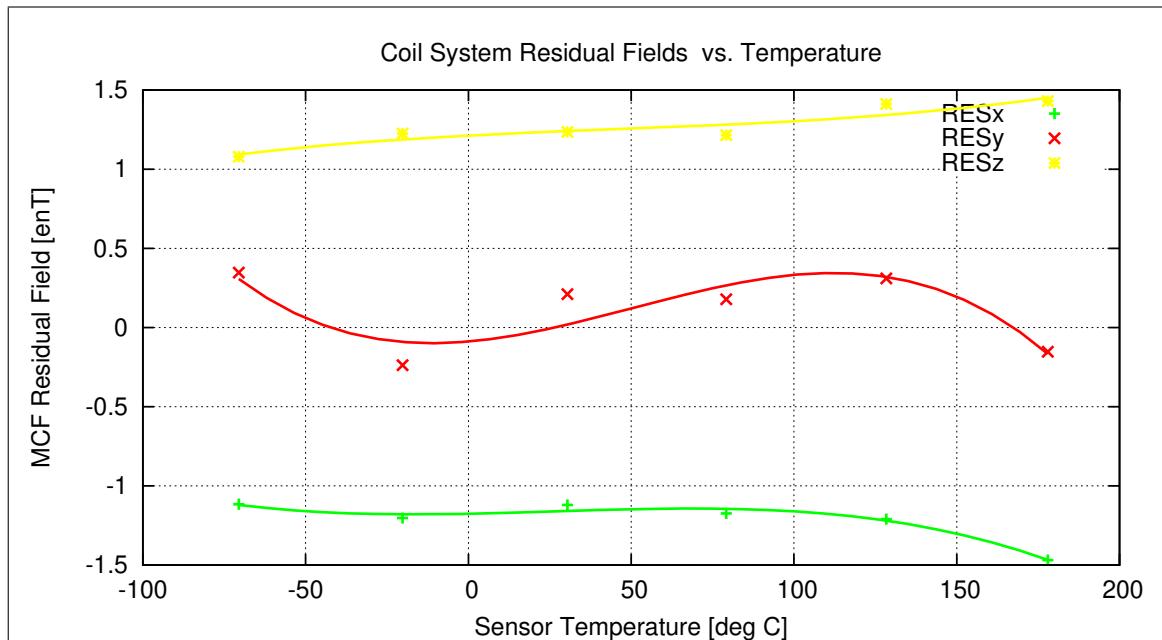


Figure 76: Coil System Residual Fields during Thermal Measurements

**Remark:**

The axes designation for this graph is given as follows (rf. to setup defined in chapter 1):

$$\begin{aligned} X_m &= X_c \\ Y_m &= Y_c \\ Z_m &= -X_c \end{aligned}$$

**12.2.3 Temperature Calibration of the AC Transfer Function****Used Temperature Measurements:**

Calibration Parameter File	Remark
FREQ_PARAMETER__13-04-03-14-41-31.FPF	
FREQ_PARAMETER__13-04-04-13-14-59.FPF	
FREQ_PARAMETER__13-04-08-10-31-48.FPF	
FREQ_PARAMETER__13-04-08-14-06-16.FPF	

Thermal Parameter File: THERMAL\_AC\_PARAMETER\_\_13-04-03-14-41-31.TAF

### Facility Parameter:

Nominal Sensor Setup: Diagonal in Space inside Thermal Box.

Sensor Temperature Channel:  $T_{59}$

Coil System Temperature Channel:  $T_{29}$

### Temperature Profile

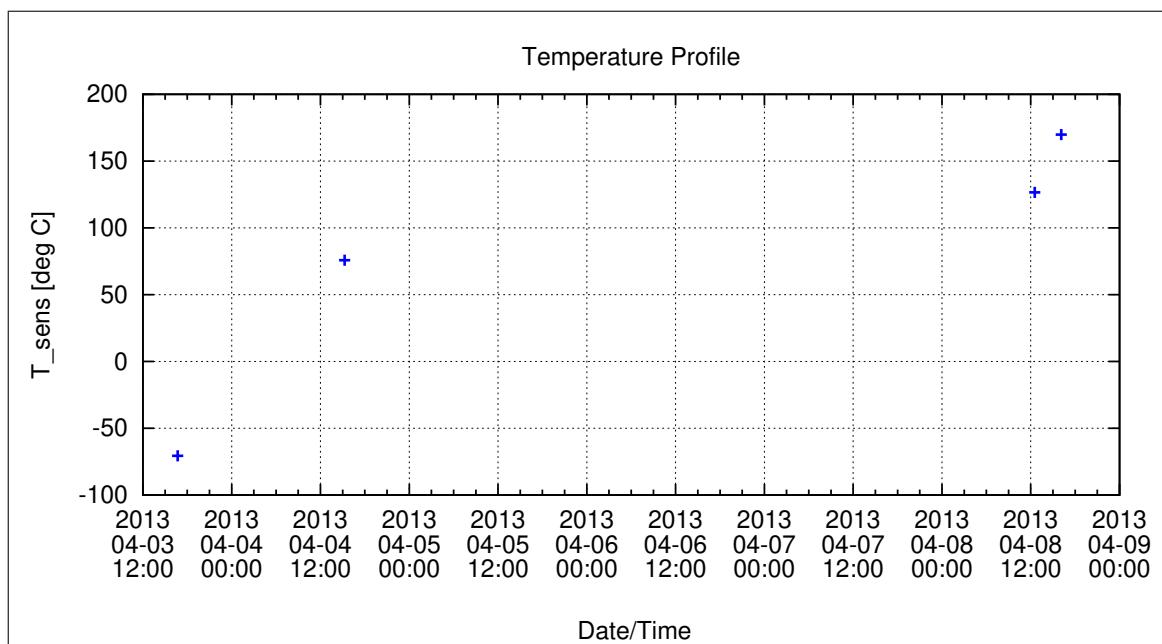


Figure 77: Temperature Profile

## Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the AC measurements.

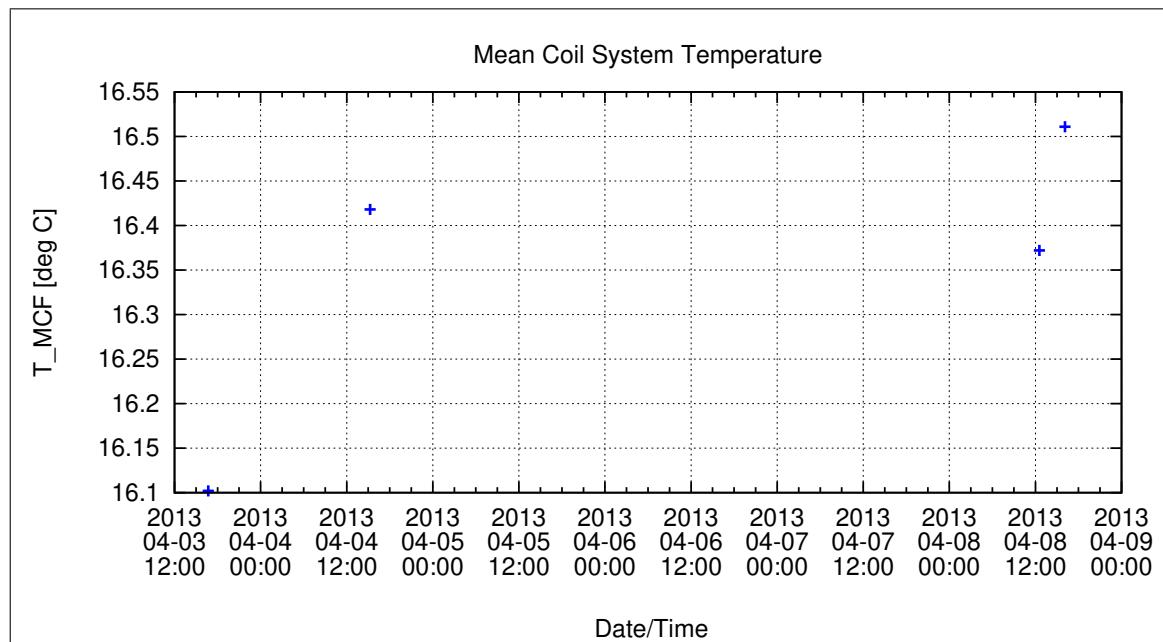


Figure 78: Coil System Temperature during Thermal AC Measurements

**Calibration Parameter:**-3dB Corner Frequency  $f_{3dB}$  vs. Temperature:

$$f_{3dB,i}(T) = \sum_{k=0}^n f_{3dB,k,i} T^k \quad [\text{Hz}, \text{ } ^\circ\text{C}], \ i=\{\text{x,y,z}\}$$

	$f_{3dB,0,i}$	$f_{3dB,1,i}$	$f_{3dB,2,i}$	$f_{3dB,3,i}$	$f_{3dB,4,i}$	$f_{3dB,5,i}$
$f_{3dB,x}$	5.91894E+1	9.13759E-3				
$f_{3dB,y}$	5.91557E+1	1.06586E-2				
$f_{3dB,z}$	5.61646E+1	2.16322E-2				

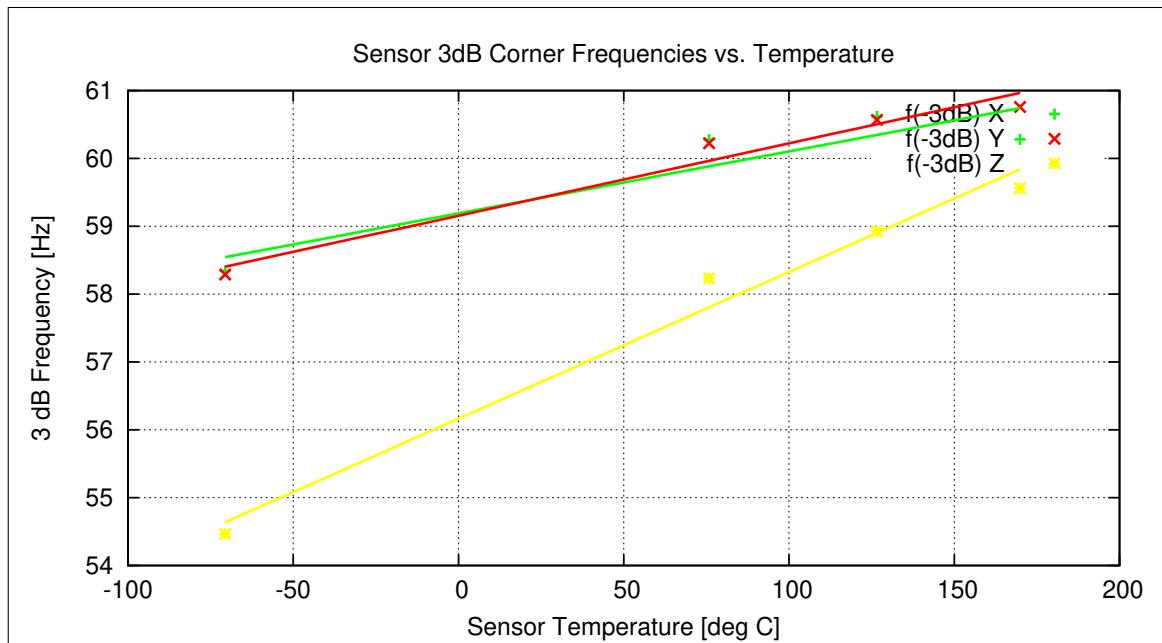


Figure 79: Temperature dependence of 3dB Corner Frequency

Instrument Sampling Frequency:

The following graph shows the calculated sampling frequencies vs. the actual sensor temperature.

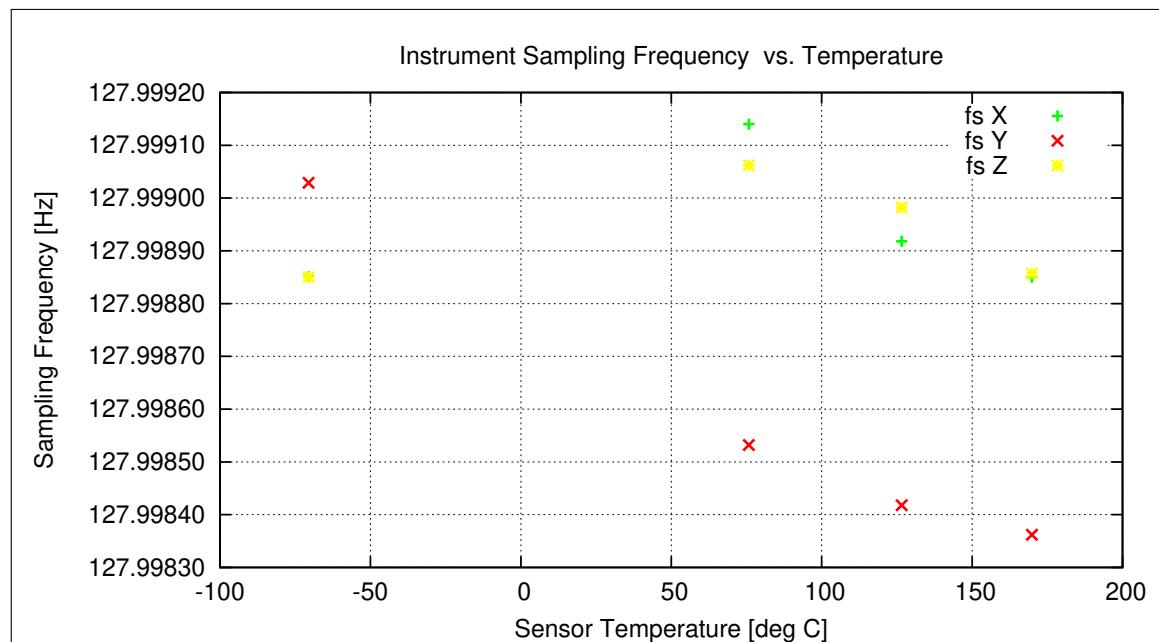


Figure 80: Instrument Sampling Frequency versus Sensor Temperature

Mean Samplerate: 127.998821 Hz.

Mean Standard Deviation of Samplerate: 0.000109 Hz.

## 13 Combined Measurements from April 09 – 11, 2013

### 13.1 Thermal-Analysis - IB Sensor, cal mode 0

#### 13.1.1 Temperature Calibration on Linear Axes

##### Used Temperature Measurements:

Calibration Parameter File	Remark
PARAMETER_TEMPLIN__13-04-09_09-52-27.CPF	
PARAMETER_TEMPLIN__13-04-09_11-54-15.CPF	
PARAMETER_TEMPLIN__13-04-10_08-18-43.CPF	
PARAMETER_TEMPLIN__13-04-10_11-47-03.CPF	
PARAMETER_TEMPLIN__13-04-11_08-06-33.CPF	
PARAMETER_TEMPLIN__13-04-11_14-47-36.CPF	

Thermal Parameter File: THERMAL\_PARAMETER\_\_13-04-09-52-27.TPF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Initial Sensor Rotation:

$$\underline{\underline{R}} = \begin{pmatrix} +0.999974 & +0.003127 & +0.006434 \\ -0.003132 & +0.999995 & +0.000706 \\ -0.006432 & -0.000726 & +0.999979 \end{pmatrix}$$

Initial Rotation Angles:

$$\text{Rotation @ X: } \lambda_x = +0^\circ 24'36''$$

$$\text{Rotation @ Y: } \mu_y = +0^\circ 11'2''$$

$$\text{Rotation @ Z: } \nu_z = +0^\circ 22'15''$$

Determinant of Rotation Matrix: 1.0000

Nominal Field Source: SOLARTRON

Automatic Coil correction: used

Used Sensor-Temperature-Channel:  $T_{59}$

## Temperature Profile

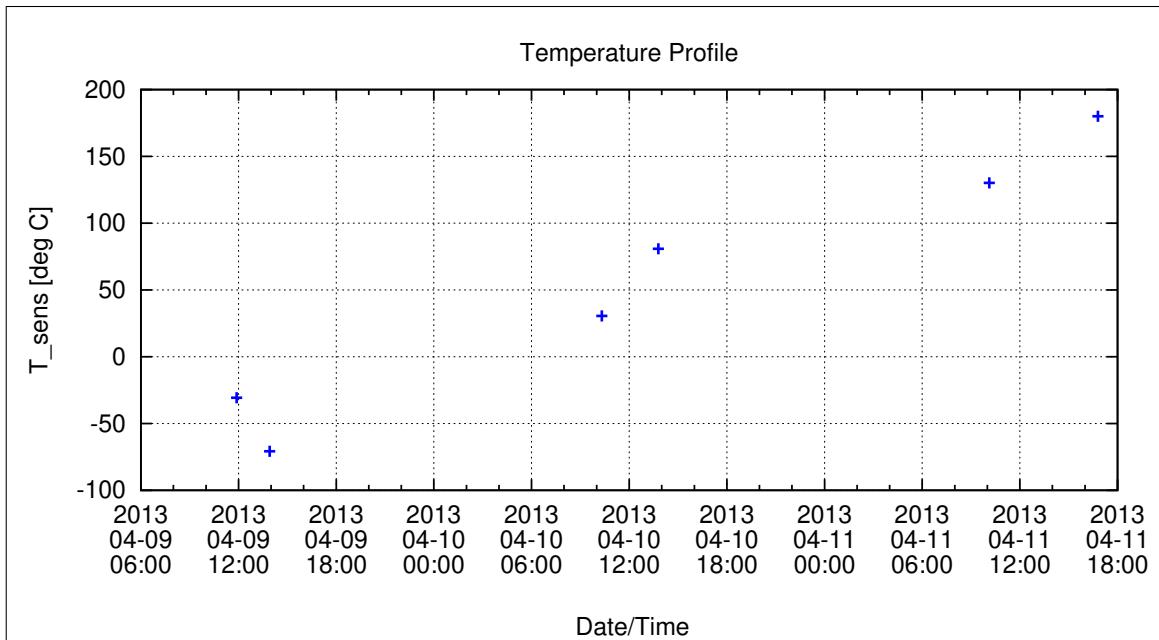


Figure 81: Temperature Profile

**Calibration Parameter:**Sensitivity  $\sigma_i$  vs. Temperature:

$$\sigma_i(T) = \sum_{k=0}^n \sigma_{k,i} T^k \quad [1, {}^\circ\text{C}], \quad i=\{\text{x}, \text{y}, \text{z}\}$$

	$\sigma_{0,i}$	$\sigma_{1,i}$	$\sigma_{2,i}$	$\sigma_{3,i}$	$\sigma_{4,i}$	$\sigma_{5,i}$
$\sigma_x$	9.75788E-1	-1.59695E-5				
$\sigma_y$	9.88057E-1	-1.44024E-5				
$\sigma_z$	9.85916E-1	-1.77112E-5				

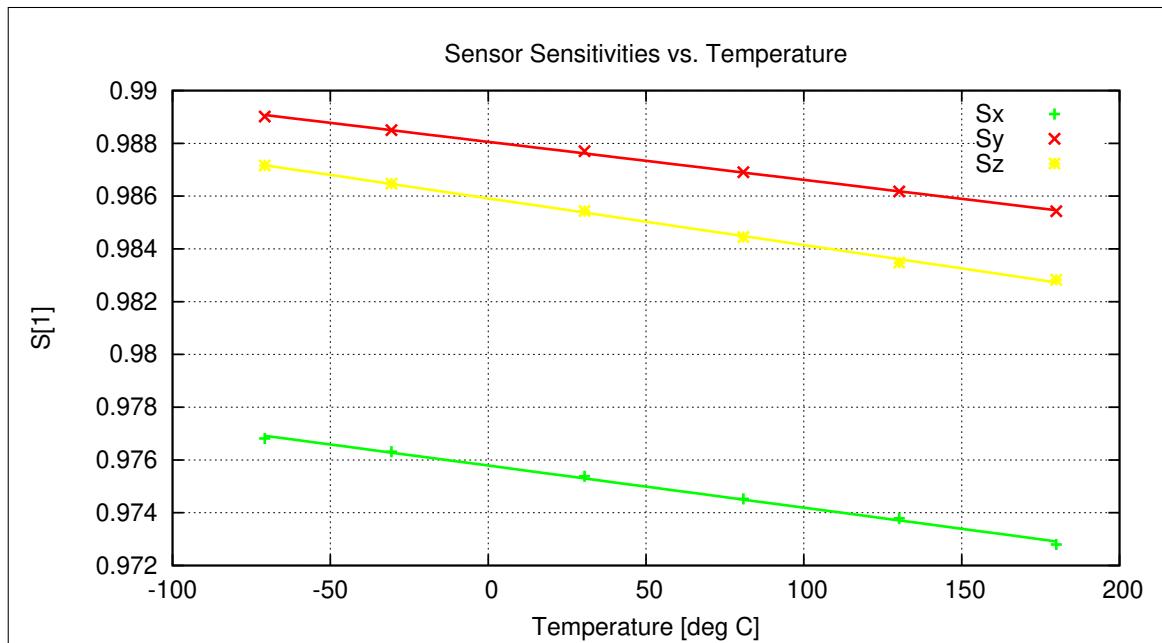


Figure 82: Temperature dependence of Sensitivities

Misalignment Angles  $\xi_{ij}$  vs. Temperature:

$$\xi_{ij}(T) = \sum_{k=0}^n \xi_{k,ij} T^k \quad [\text{deg, } ^\circ\text{C}], \text{ ij} = \{\text{xy}, \text{xz}, \text{yz}\}$$

	$\xi_{0,ij}$	$\xi_{1,ij}$	$\xi_{2,ij}$	$\xi_{3,ij}$	$\xi_{4,ij}$	$\xi_{5,ij}$
$\xi_{xy}$	8.9575E+1	5.8946E-5				
$\xi_{xz}$	8.9942E+1	4.1061E-5				
$\xi_{yz}$	9.0345E+1	-1.6514E-5				

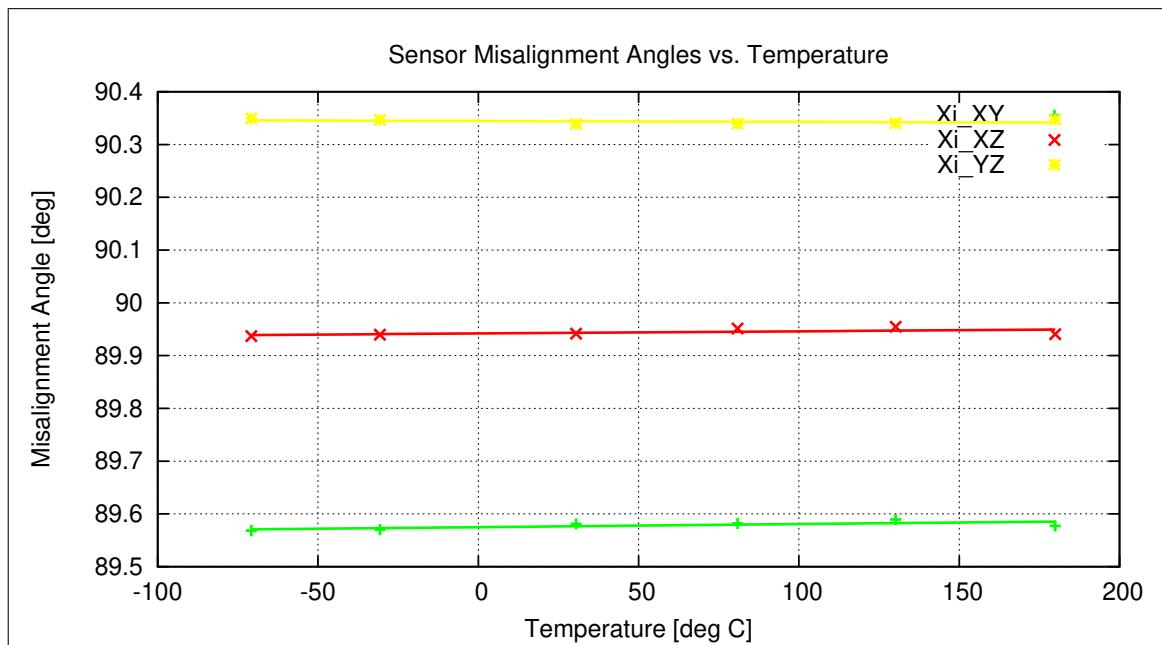


Figure 83: Temperature dependence of Misalignment Angles

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Offset & Residual MCF Field  $\underline{B}^{or} = \underline{B}^{off} + \underline{B}^{res}$  vs. Temperature:

$$\underline{B}^{or}(T) = \sum_{k=0}^n \underline{B}_k^{or} T^k \quad [\text{enT}, {}^\circ\text{C}]$$

	$\underline{B}_0^{or}$	$\underline{B}_1^{or}$	$\underline{B}_2^{or}$	$\underline{B}_3^{or}$	$\underline{B}_4^{or}$	$\underline{B}_5^{or}$
$B_x^{or}$	-3.543E+0	1.981E-3	1.637E-4	-7.621E-7		
$B_y^{or}$	-1.315E+0	-5.537E-3	-1.109E-4	6.784E-7		
$B_z^{or}$	-1.075E+1	6.562E-3	9.510E-6	-6.083E-8		

Model Quality:

Minimum and maximum errors of the calculated Model vs. Temperature:

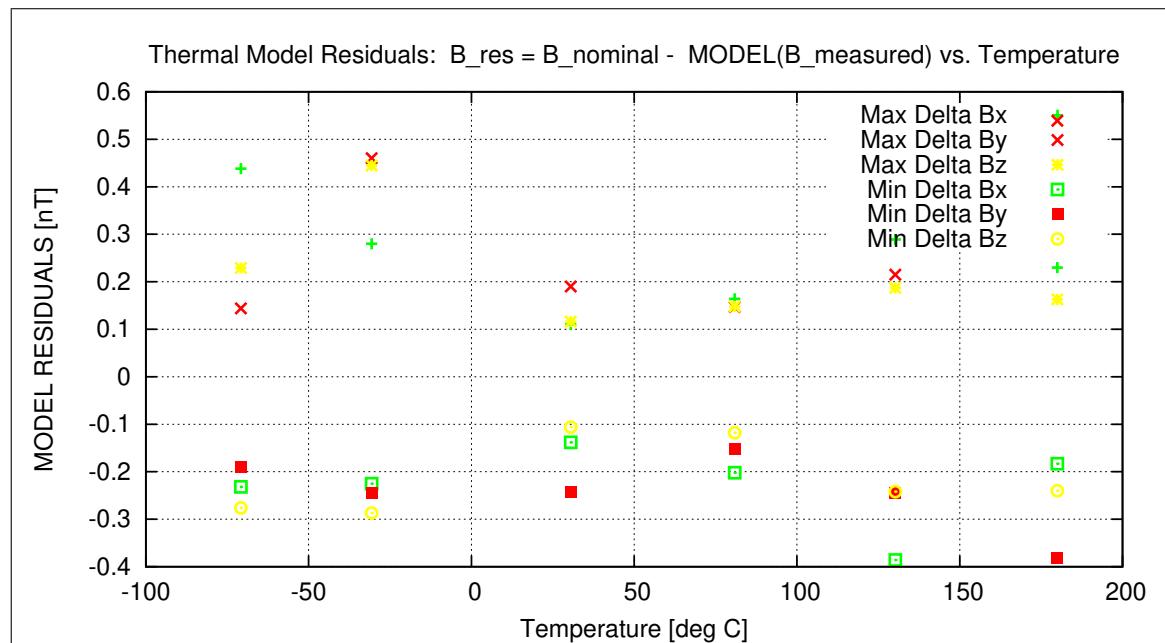


Figure 84: Residuals of Thermal Model

Sensor Rotation during Test:

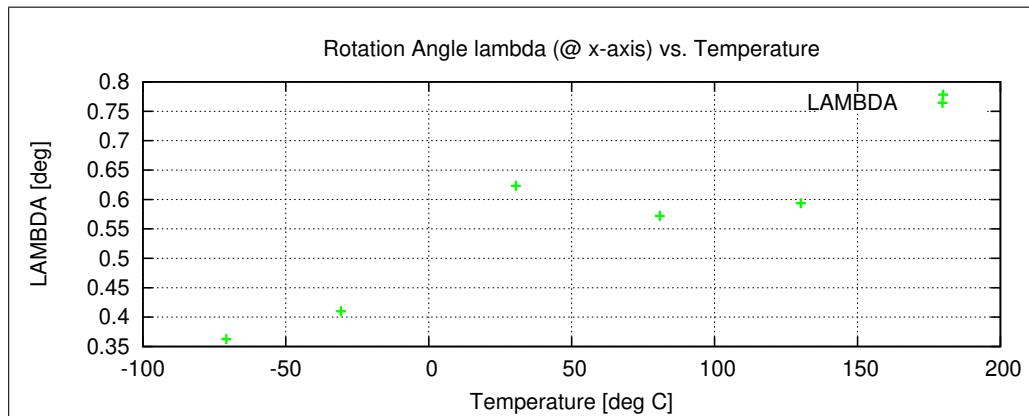


Figure 85: Rotation @ X-Axis

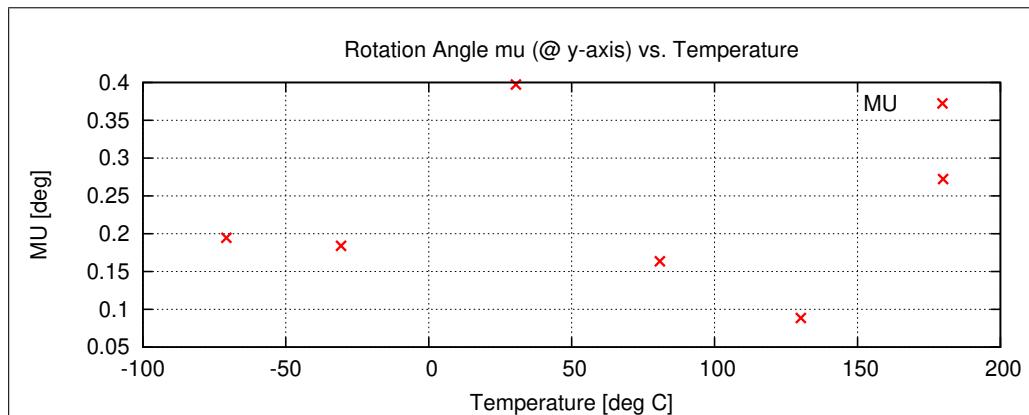


Figure 86: Rotation @ Y-Axis

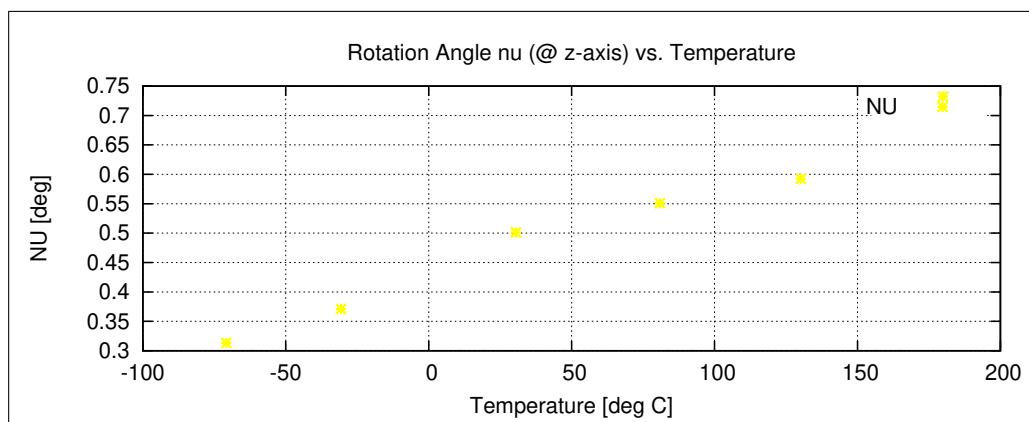


Figure 87: Rotation @ Z-Axis

**13.1.2 Temperature Calibration of the Sensor Offset****Used Temperature Measurements:**

Calibration Parameter File	Remark
OFF_PARAMETER__13-04-09-11-14-46.OPF	
OFF_PARAMETER__13-04-09-13-08-27.OPF	
OFF_PARAMETER__13-04-10-08-09-57.OPF	
OFF_PARAMETER__13-04-10-12-17-18.OPF	
OFF_PARAMETER__13-04-11-08-37-21.OPF	
OFF_PARAMETER__13-04-11-15-18-03.OPF	

Thermal Parameter File: THERMAL\_OFF\_PARAMETER\_\_13-04-09-11-14-46.TOF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{R}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{R}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Sensor Temperature Channel: T<sub>59</sub>

Coil System Temperature Channel: T<sub>29</sub>

## Temperature Profile

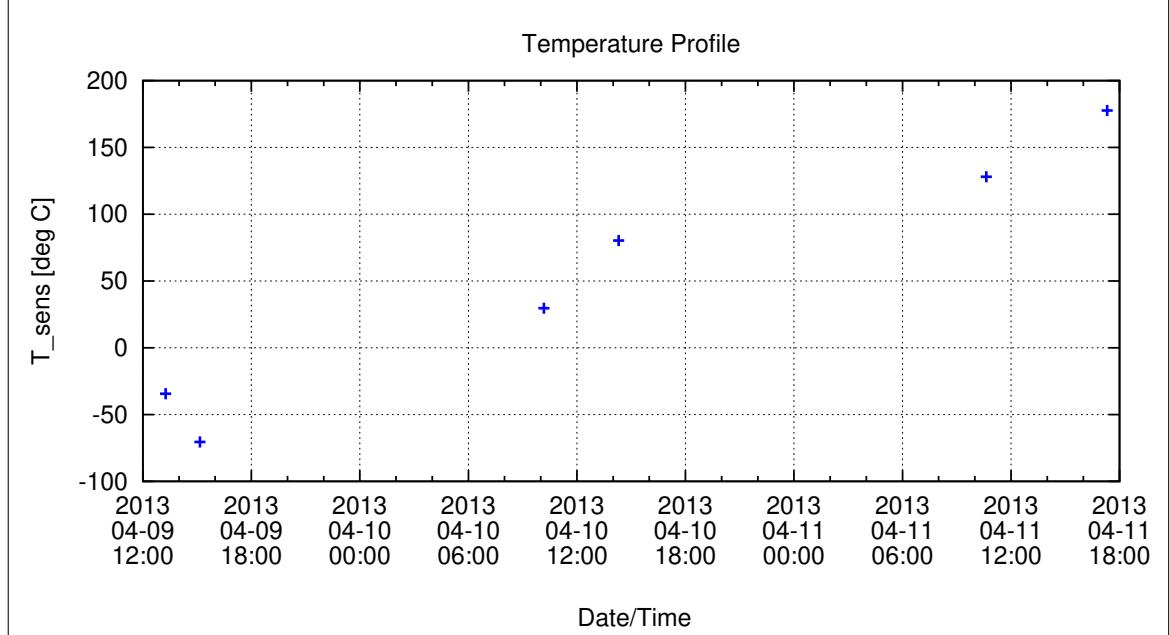


Figure 88: Temperature Profile

**Calibration Parameter:**Sensor Offset  $B_{\text{off}}$  vs. Temperature:

$$B_{\text{off},i}(T) = \sum_{k=0}^n B_{\text{off},k,i} T^k \quad [\text{enT}, \text{ } ^\circ\text{C}], \ i=\{\text{x,y,z}\}$$

	$B_{\text{off},0,i}$	$B_{\text{off},1,i}$	$B_{\text{off},2,i}$	$B_{\text{off},3,i}$	$B_{\text{off},4,i}$	$B_{\text{off},5,i}$
$B_{\text{off},x}$	-2.92971E-1	-3.69506E-3	4.77003E-5			
$B_{\text{off},y}$	-1.05443E+0	-1.72164E-3	1.51567E-5			
$B_{\text{off},z}$	1.46463E-1	3.34259E-3	-2.31102E-5			

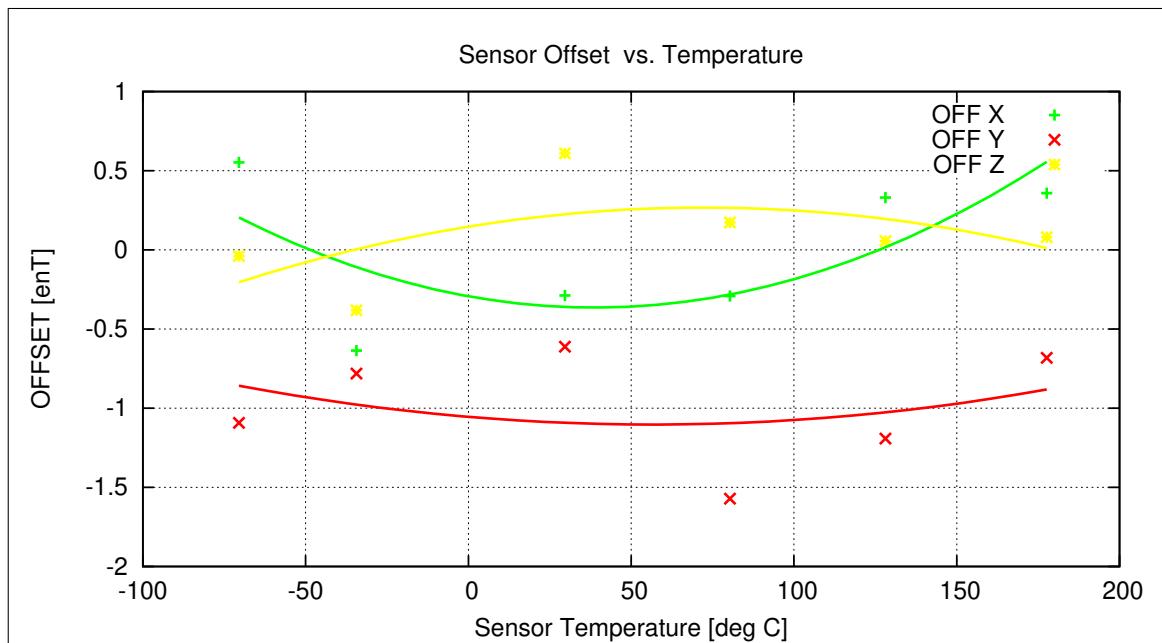


Figure 89: Temperature dependence of Sensor Offsets

Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the offset measurements.

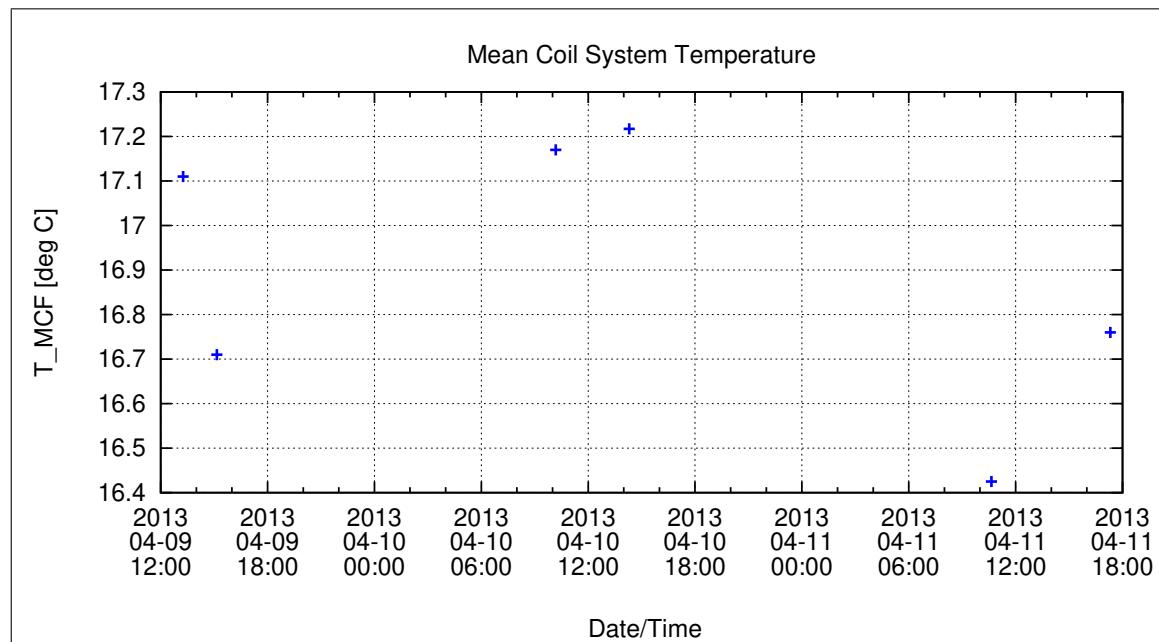


Figure 90: Coil System Temperature during Thermal Measurements

Coil System Residual Field:

The following graph shows the three components of the Coil System Residual field during the whole measurement. Axes designators are related to the actual DUT coordinate system and NOT to Coil System coordinates.

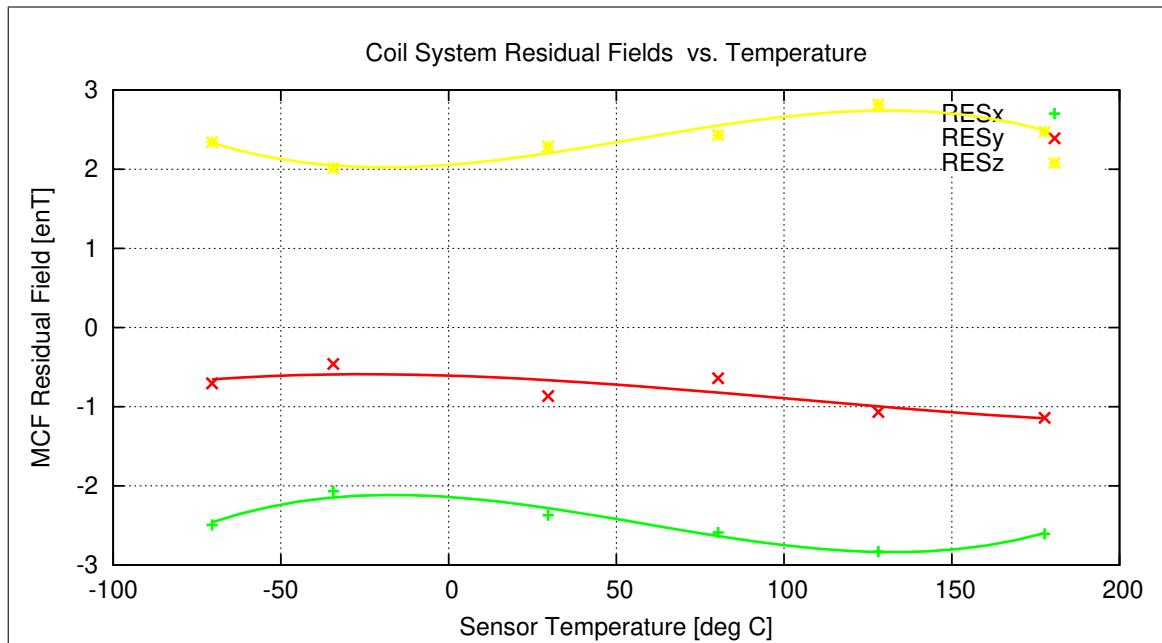


Figure 91: Coil System Residual Fields during Thermal Measurements

**Remark:**

The axes designation for this graph is given as follows (rf. to setup defined in chapter 1):

$$\begin{aligned} X_m &= X_c \\ Y_m &= Y_c \\ Z_m &= -X_c \end{aligned}$$

**13.1.3 Temperature Calibration of the AC Transfer Function****Used Temperature Measurements:**

Calibration Parameter File	Remark
FREQ_PARAMETER__13-04-09-12-26-36.FPF	
FREQ_PARAMETER__13-04-10-12-26-40.FPF	
FREQ_PARAMETER__13-04-11-08-46-10.FPF	
FREQ_PARAMETER__13-04-11-15-26-22.FPF	

Thermal Parameter File: THERMAL\_AC\_PARAMETER\_\_13-04-09-12-26-36.TAF

### Facility Parameter:

Nominal Sensor Setup: Diagonal in Space inside Thermal Box.

Sensor Temperature Channel: T<sub>59</sub>

Coil System Temperature Channel: T<sub>29</sub>

### Temperature Profile

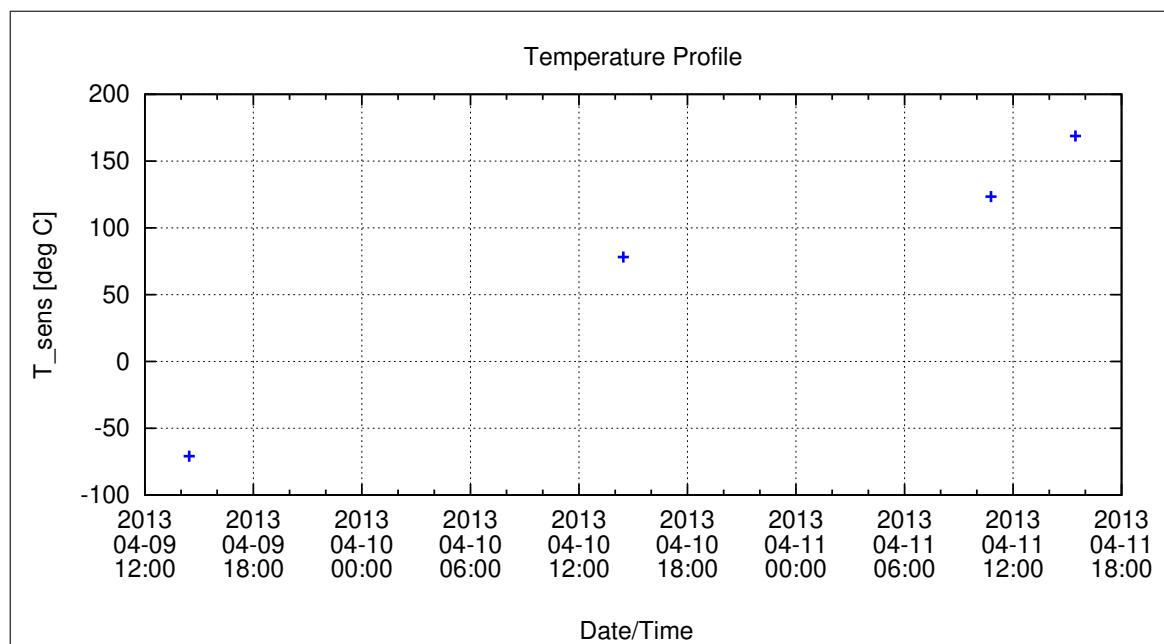


Figure 92: Temperature Profile

Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the AC measurements.

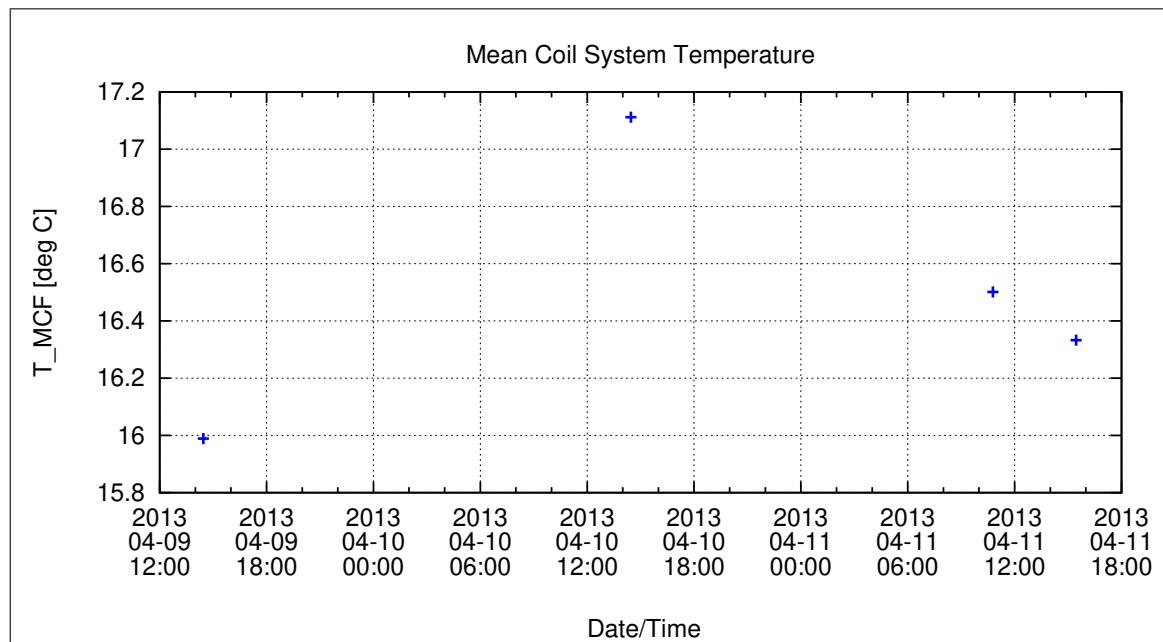


Figure 93: Coil System Temperature during Thermal AC Measurements

**Calibration Parameter:**-3dB Corner Frequency  $f_{3dB}$  vs. Temperature:

$$f_{3dB,i}(T) = \sum_{k=0}^n f_{3dB,k,i} T^k \quad [\text{Hz}, \text{ } ^\circ\text{C}], \ i=\{\text{x,y,z}\}$$

	$f_{3dB,0,i}$	$f_{3dB,1,i}$	$f_{3dB,2,i}$	$f_{3dB,3,i}$	$f_{3dB,4,i}$	$f_{3dB,5,i}$
$f_{3dB,x}$	5.23089E+1	-1.76236E-1	4.32362E-4			
$f_{3dB,y}$	4.80020E+1	-2.09909E-1	5.51143E-4			
$f_{3dB,z}$	5.28160E+1	-3.41876E-2	8.18077E-5			

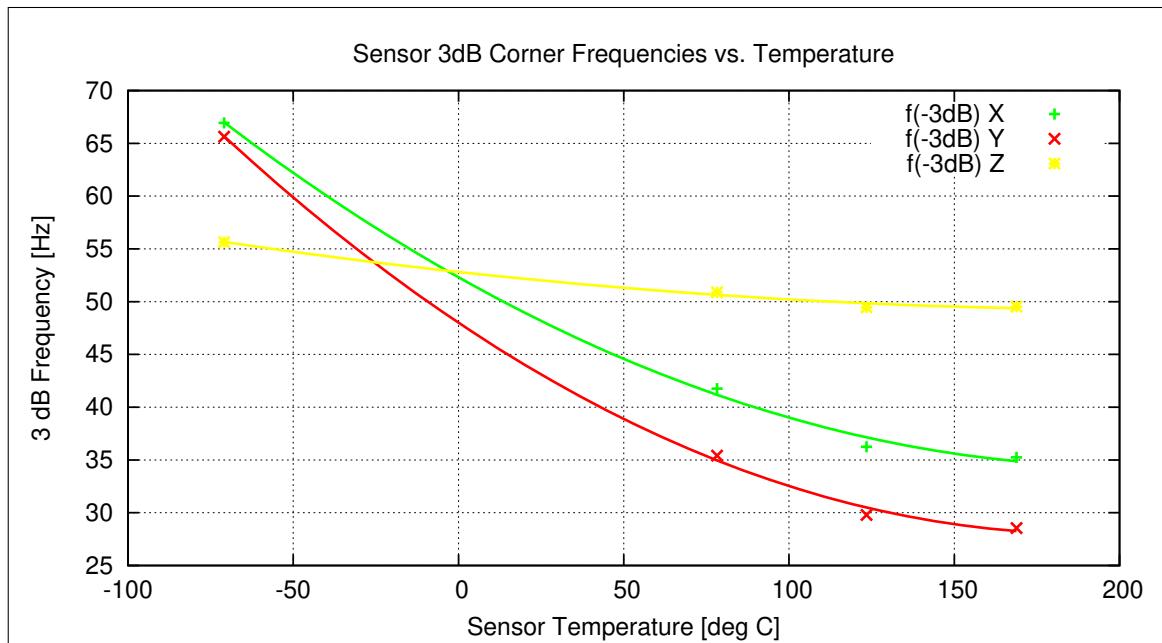


Figure 94: Temperature dependence of 3dB Corner Frequency

Instrument Sampling Frequency:

The following graph shows the calculated sampling frequencies vs. the actual sensor temperature.

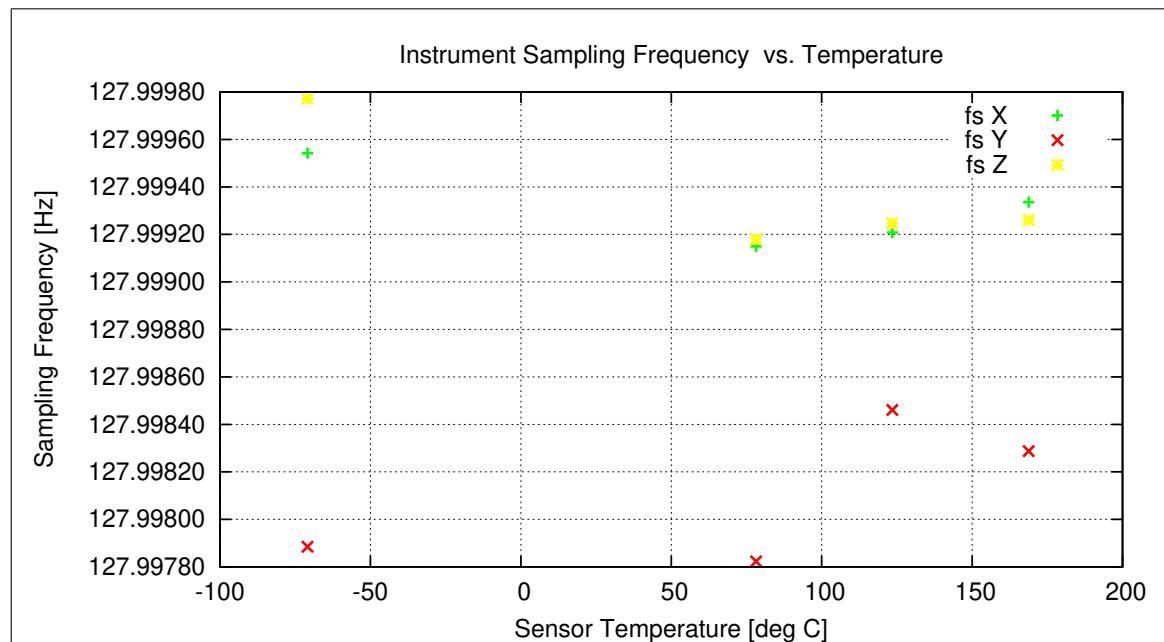


Figure 95: Instrument Sampling Frequency versus Sensor Temperature

Mean Samplerate: 127.998929 Hz.

Mean Standard Deviation of Samplerate: 0.000149 Hz.

## 13.2 Thermal-Analysis - IB Sensor, cal mode 4

### 13.2.1 Temperature Calibration on Linear Axes

#### Used Temperature Measurements:

Calibration Parameter File	Remark
PARAMETER_TEMPLIN__13-04-09_10-34-40.CPF	
PARAMETER_TEMPLIN__13-04-09_14-12-36.CPF	
PARAMETER_TEMPLIN__13-04-10_07-28-44.CPF	
PARAMETER_TEMPLIN__13-04-10_13-11-42.CPF	
PARAMETER_TEMPLIN__13-04-11_09-31-53.CPF	
PARAMETER_TEMPLIN__13-04-11_12-35-43.CPF	
PARAMETER_TEMPLIN__13-04-11_13-06-41.CPF	

Thermal Parameter File: THERMAL\_PARAMETER\_\_13-04-09-10-34-40.TPF

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## Facility Parameter:

Nominal Sensor Setup  $\underline{B}_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Calculated Initial Sensor Rotation:

$$\underline{\underline{R}} = \begin{pmatrix} +0.999707 & +0.023539 & +0.005617 \\ -0.023561 & +0.999715 & +0.003876 \\ -0.005524 & -0.004007 & +0.999977 \end{pmatrix}$$

Initial Rotation Angles:

$$\text{Rotation @ X: } \lambda_x = +1^\circ 23'12''$$

$$\text{Rotation @ Y: } \mu_y = +1^\circ 22'6''$$

$$\text{Rotation @ Z: } \nu_z = +0^\circ 23'28''$$

Determinant of Rotation Matrix: 1.0000

Nominal Field Source: FLDS

Automatic Coil correction: used

Used Sensor-Temperature-Channel:  $T_{59}$

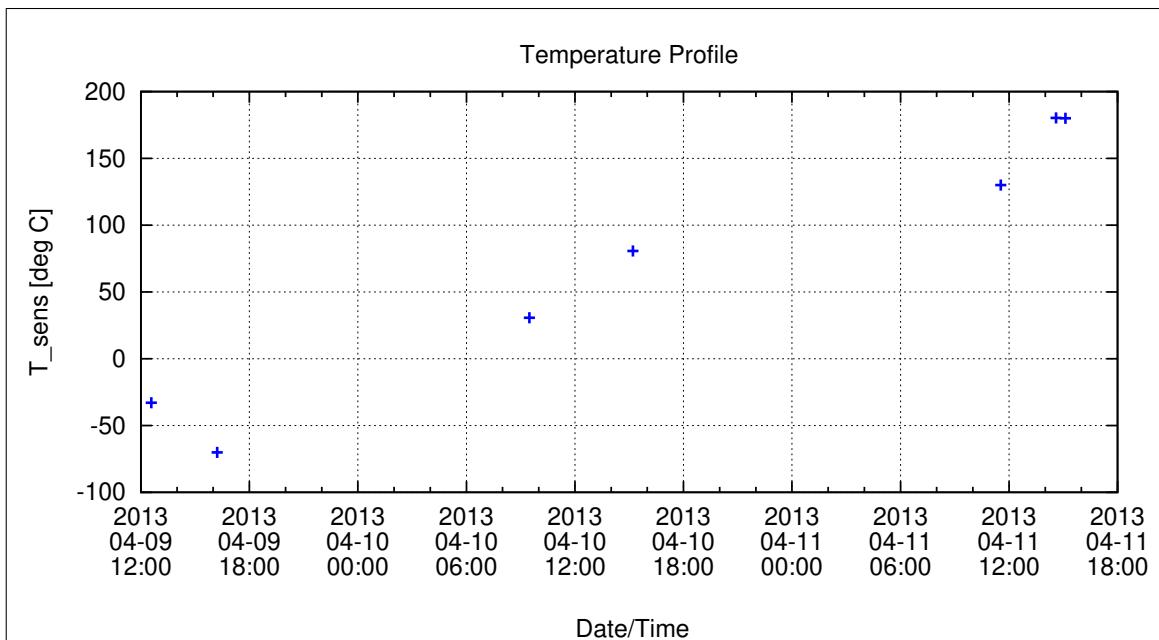
Temperature Profile

Figure 96: Temperature Profile

**Calibration Parameter:**Sensitivity  $\sigma_i$  vs. Temperature:

$$\sigma_i(T) = \sum_{k=0}^n \sigma_{k,i} T^k \quad [1, {}^\circ\text{C}], i=\{\text{x,y,z}\}$$

	$\sigma_{0,i}$	$\sigma_{1,i}$	$\sigma_{2,i}$	$\sigma_{3,i}$	$\sigma_{4,i}$	$\sigma_{5,i}$
$\sigma_x$	1.01127E+0	1.13608E-3				
$\sigma_y$	1.02445E+0	1.39015E-3				
$\sigma_z$	9.74889E-1	4.76147E-4				

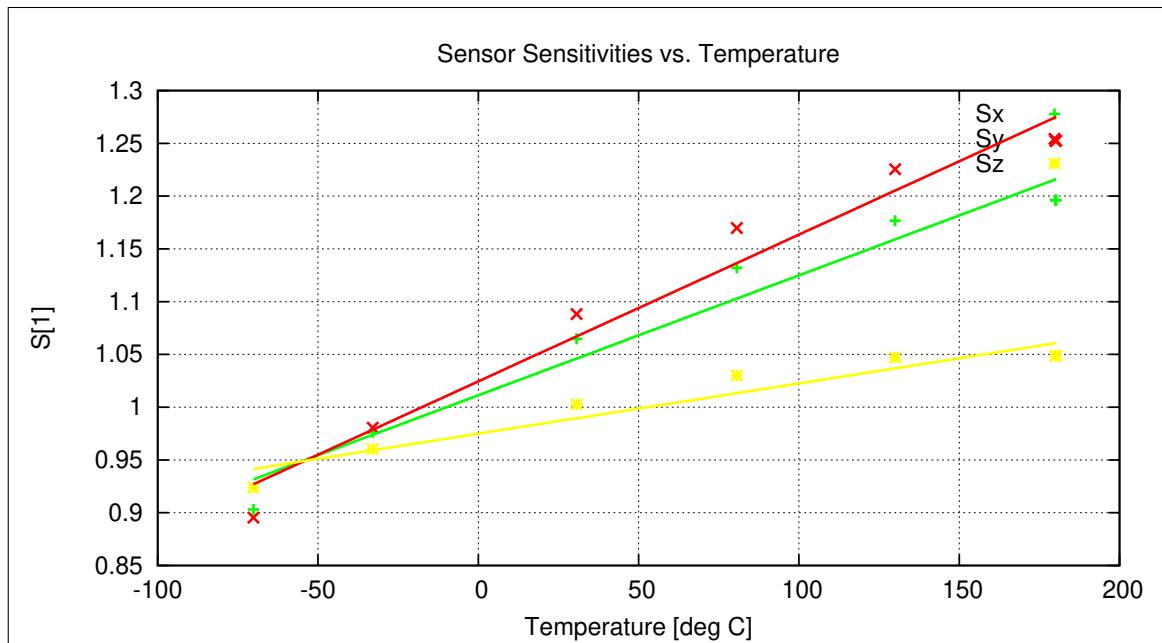


Figure 97: Temperature dependence of Sensitivities

Misalignment Angles  $\xi_{ij}$  vs. Temperature:

$$\xi_{ij}(T) = \sum_{k=0}^n \xi_{k,ij} T^k \quad [\text{deg, } ^\circ\text{C}], \text{ ij} = \{\text{xy}, \text{xz}, \text{yz}\}$$

	$\xi_{0,ij}$	$\xi_{1,ij}$	$\xi_{2,ij}$	$\xi_{3,ij}$	$\xi_{4,ij}$	$\xi_{5,ij}$
$\xi_{xy}$	9.0177E+1	1.0107E-3				
$\xi_{xz}$	8.9516E+1	-4.8192E-4				
$\xi_{yz}$	9.0554E+1	-1.7089E-3				

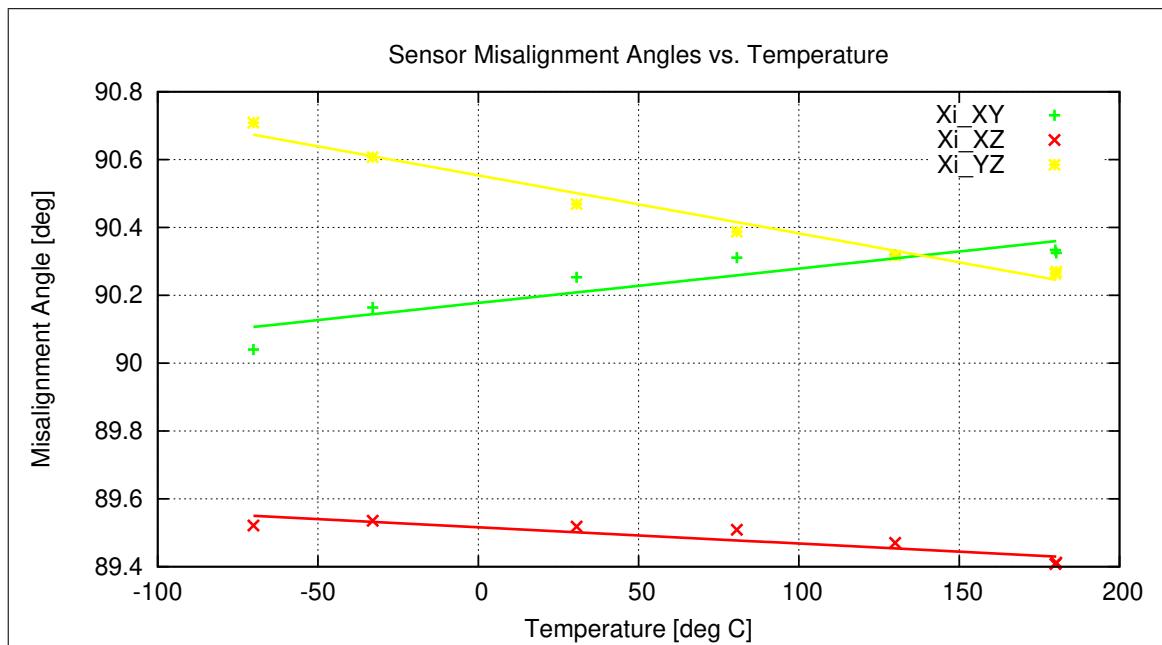


Figure 98: Temperature dependence of Misalignment Angles

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Offset & Residual MCF Field  $\underline{B}^{or} = \underline{B}^{off} + \underline{B}^{res}$  vs. Temperature:

$$\underline{B}^{or}(T) = \sum_{k=0}^n \underline{B}_k^{or} T^k \quad [\text{enT}, {}^\circ\text{C}]$$

	$\underline{B}_0^{or}$	$\underline{B}_1^{or}$	$\underline{B}_2^{or}$	$\underline{B}_3^{or}$	$\underline{B}_4^{or}$	$\underline{B}_5^{or}$
$B_x^{or}$	-2.626E+0	1.250E-2	-7.866E-5	2.016E-7		
$B_y^{or}$	-1.160E+0	-5.595E-3	-7.993E-5	5.415E-7		
$B_z^{or}$	-1.065E+1	7.654E-3	8.301E-5	-4.486E-7		

Model Quality:

Minimum and maximum errors of the calculated Model vs. Temperature:

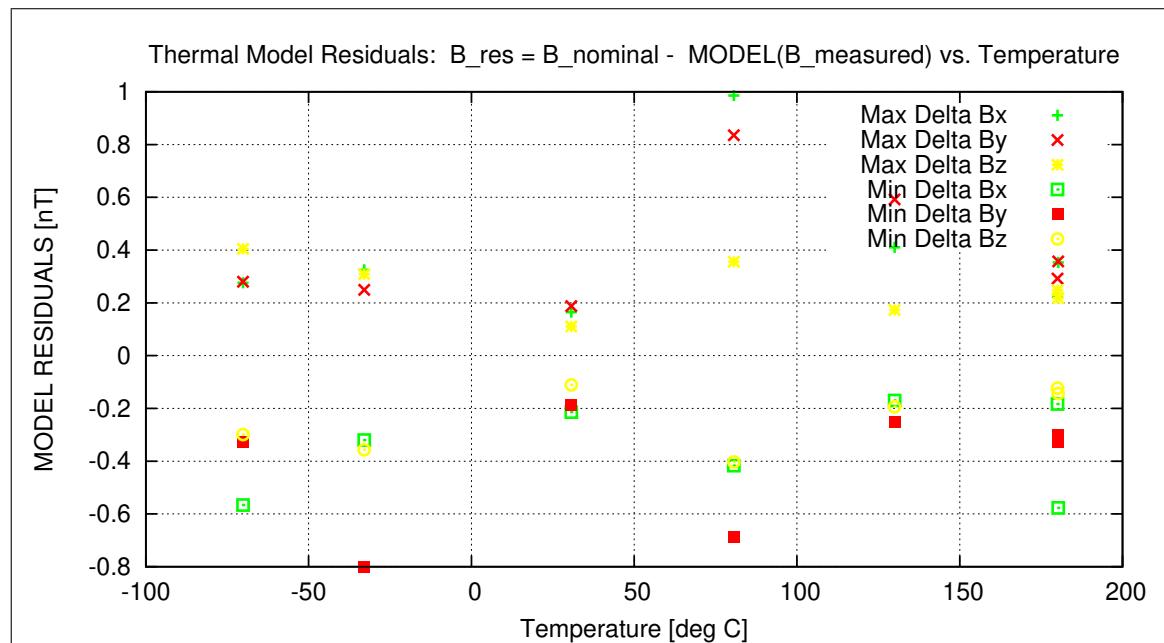


Figure 99: Residuals of Thermal Model

Sensor Rotation during Test:

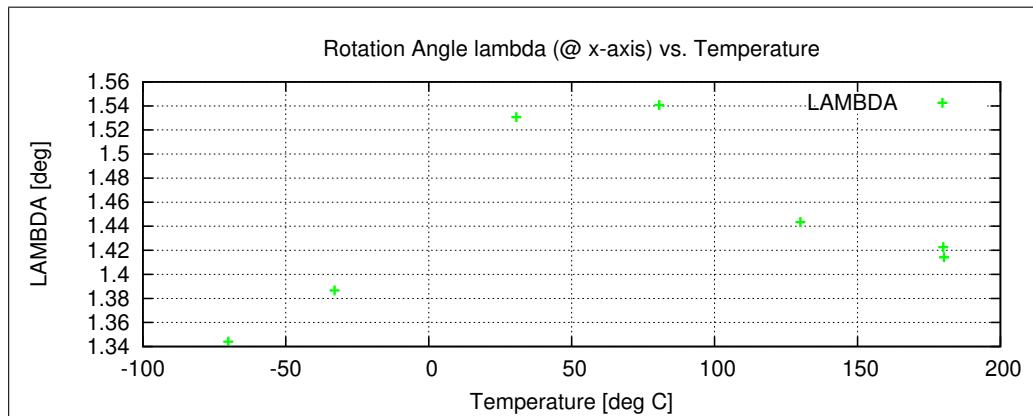


Figure 100: Rotation @ X-Axis

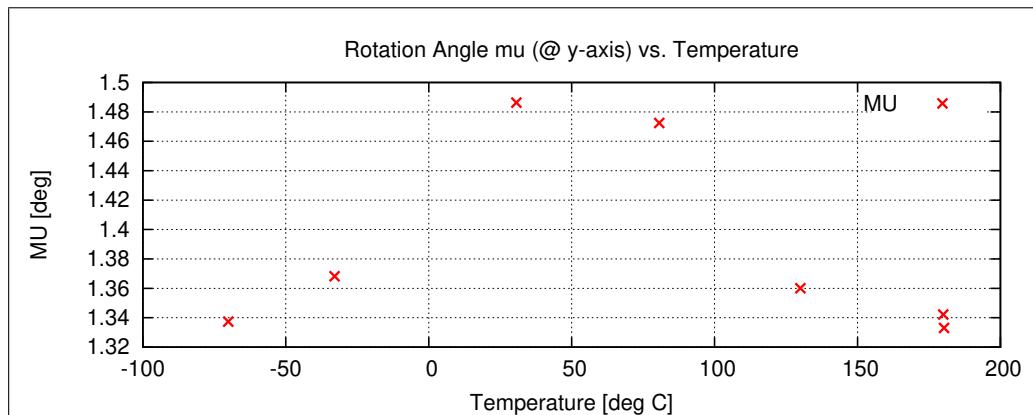


Figure 101: Rotation @ Y-Axis

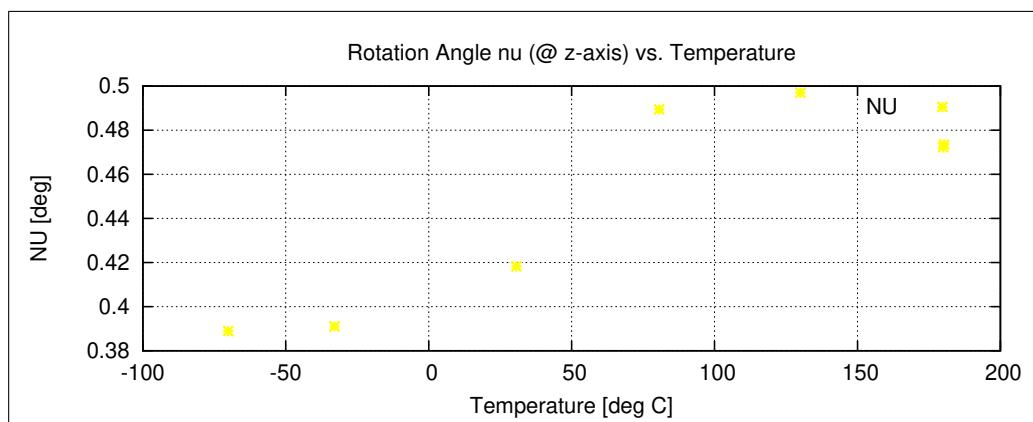


Figure 102: Rotation @ Z-Axis

**13.2.2 Temperature Calibration of the Sensor Offset****Used Temperature Measurements:**

Calibration Parameter File	Remark
OFF_PARAMETER__13-04-09-11-05-13.OPF	
OFF_PARAMETER__13-04-09-13-18-15.OPF	
OFF_PARAMETER__13-04-10-07-59-38.OPF	
OFF_PARAMETER__13-04-10-13-47-06.OPF	
OFF_PARAMETER__13-04-11-10-11-50.OPF	
OFF_PARAMETER__13-04-11-13-37-03.OPF	

Thermal Parameter File: THERMAL\_OFF\_PARAMETER\_\_13-04-09-11-05-13.TOF

**Facility Parameter:**

Nominal Sensor Setup  $B_{\text{DUT}} = \underline{\underline{R}}_{\text{nom}} \underline{B}_{\text{c}}$

$$\underline{\underline{R}}_{\text{nom}} = \begin{pmatrix} +1.000000 & +0.000000 & +0.000000 \\ +0.000000 & +1.000000 & +0.000000 \\ +0.000000 & +0.000000 & +1.000000 \end{pmatrix}$$

Sensor Temperature Channel: T<sub>59</sub>

Coil System Temperature Channel: T<sub>29</sub>

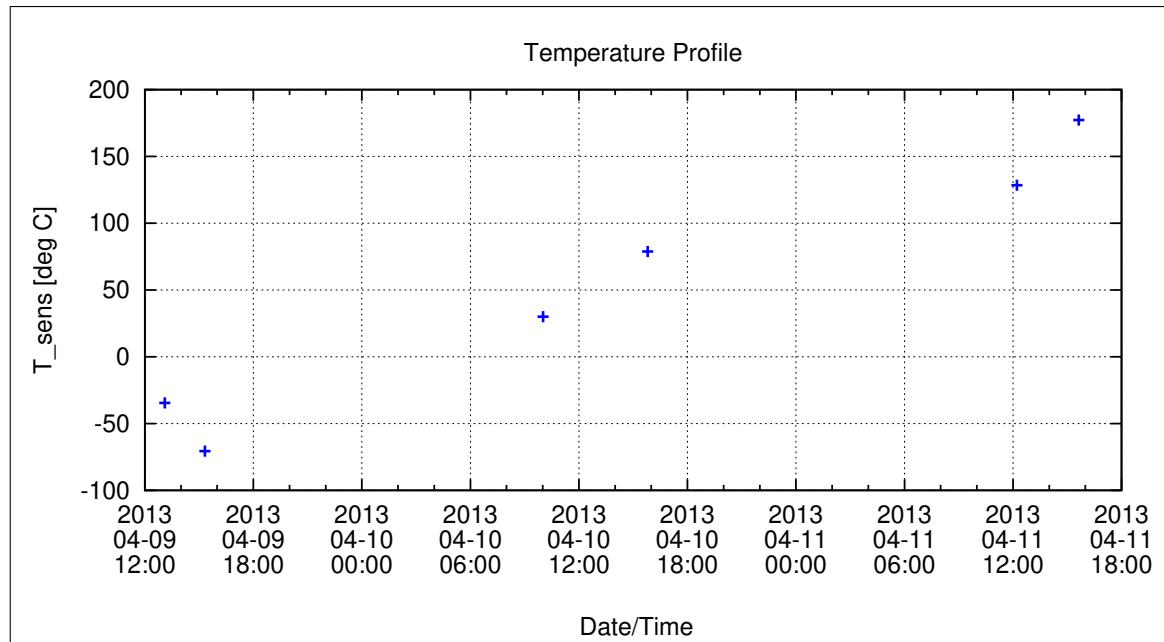
**Temperature Profile**

Figure 103: Temperature Profile

**Calibration Parameter:**Sensor Offset  $B_{\text{off}}$  vs. Temperature:

$$B_{\text{off},i}(T) = \sum_{k=0}^n B_{\text{off},k,i} T^k \quad [\text{enT}, \text{ } ^\circ\text{C}], i=\{\text{x,y,z}\}$$

	$B_{\text{off},0,i}$	$B_{\text{off},1,i}$	$B_{\text{off},2,i}$	$B_{\text{off},3,i}$	$B_{\text{off},4,i}$	$B_{\text{off},5,i}$
$B_{\text{off},x}$	-5.68307E-1	4.08661E-3	6.45150E-5	-3.46324E-7		
$B_{\text{off},y}$	-5.22529E-1	-2.03202E-3	-6.13830E-5	3.69060E-7		
$B_{\text{off},z}$	-6.12748E-2	-3.29684E-6	8.06491E-5	-4.46246E-7		

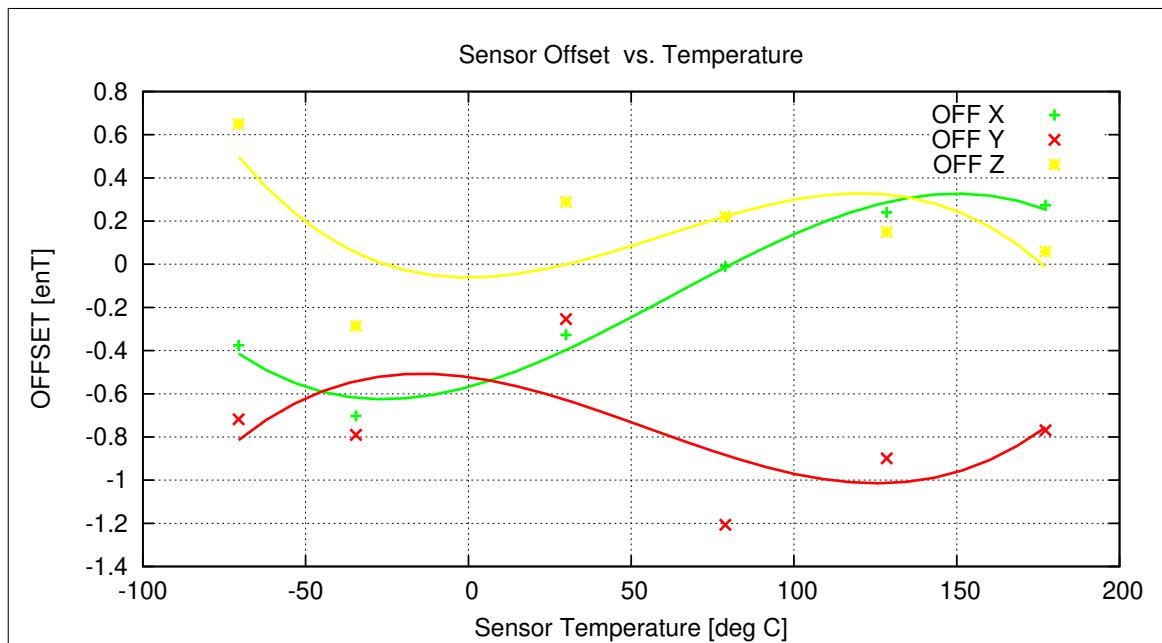


Figure 104: Temperature dependence of Sensor Offsets

## Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the offset measurements.

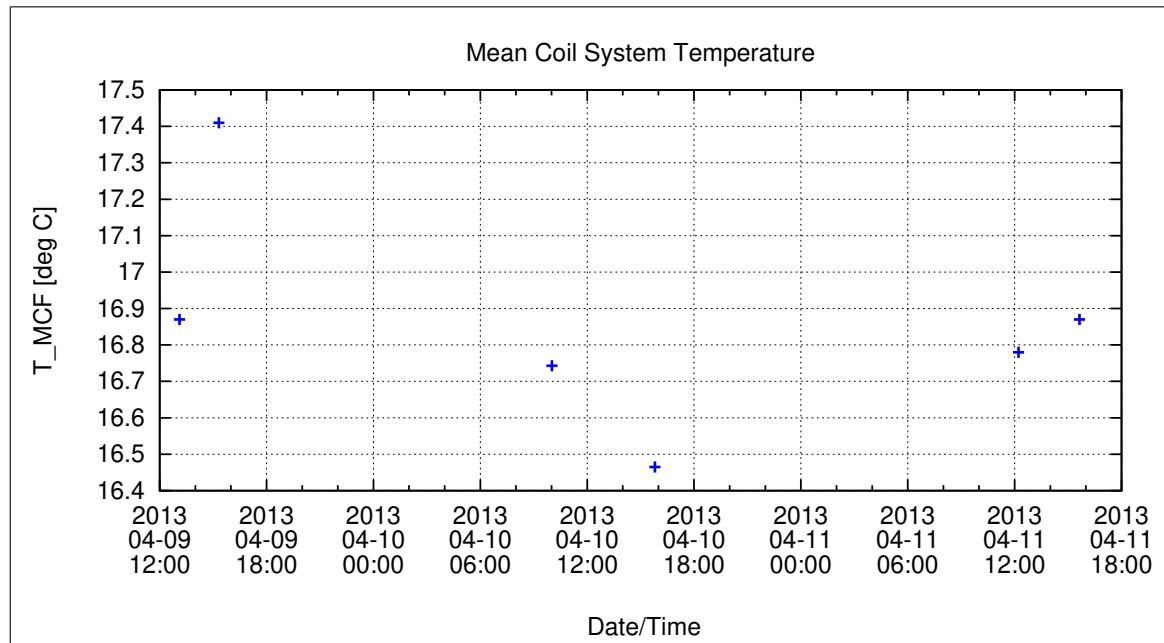


Figure 105: Coil System Temperature during Thermal Measurements

Coil System Residual Field:

The following graph shows the three components of the Coil System Residual field during the whole measurement. Axes designators are related to the actual DUT coordinate system and NOT to Coil System coordinates.

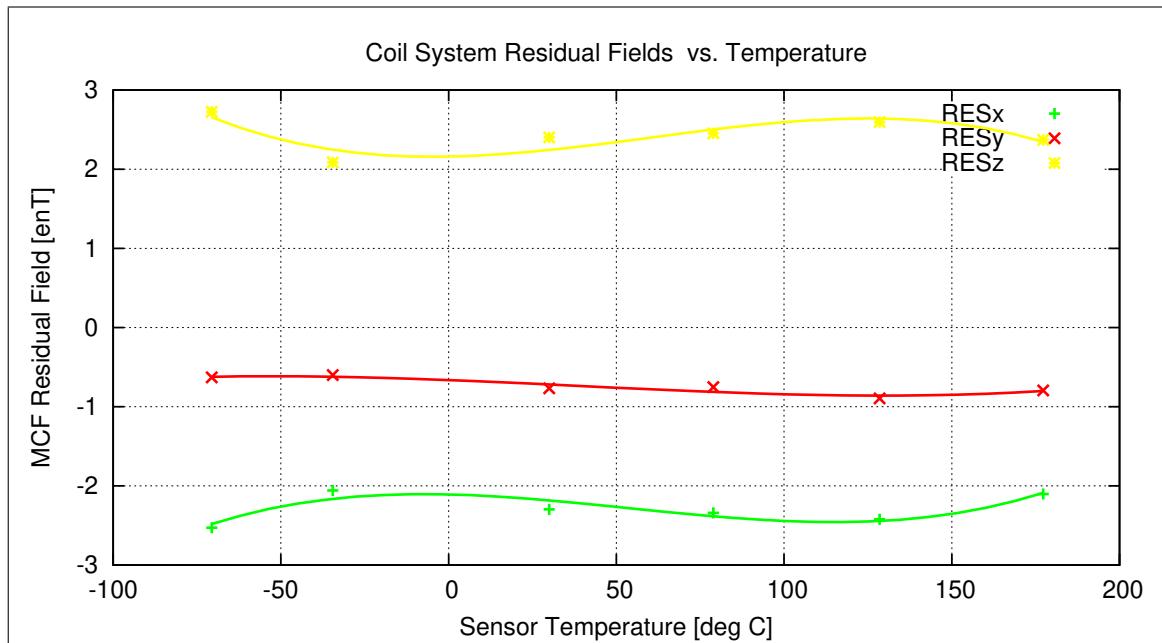


Figure 106: Coil System Residual Fields during Thermal Measurements

**Remark:**

The axes designation for this graph is given as follows (rf. to setup defined in chapter 1):

$$\begin{aligned} X_m &= X_c \\ Y_m &= Y_c \\ Z_m &= -X_c \end{aligned}$$

**13.2.3 Temperature Calibration of the AC Transfer Function****Used Temperature Measurements:**

Calibration Parameter File	Remark
FREQ_PARAMETER__13-04-09-13-27-51.FPF	
FREQ_PARAMETER__13-04-10-13-56-47.FPF	
FREQ_PARAMETER__13-04-11-10-20-53.FPF	
FREQ_PARAMETER__13-04-11-13-45-45.FPF	

Thermal Parameter File: THERMAL\_AC\_PARAMETER\_\_13-04-09-13-27-51.TAF

### Facility Parameter:

Nominal Sensor Setup: Diagonal in Space inside Thermal Box.

Sensor Temperature Channel:  $T_{59}$

Coil System Temperature Channel:  $T_{29}$

### Temperature Profile

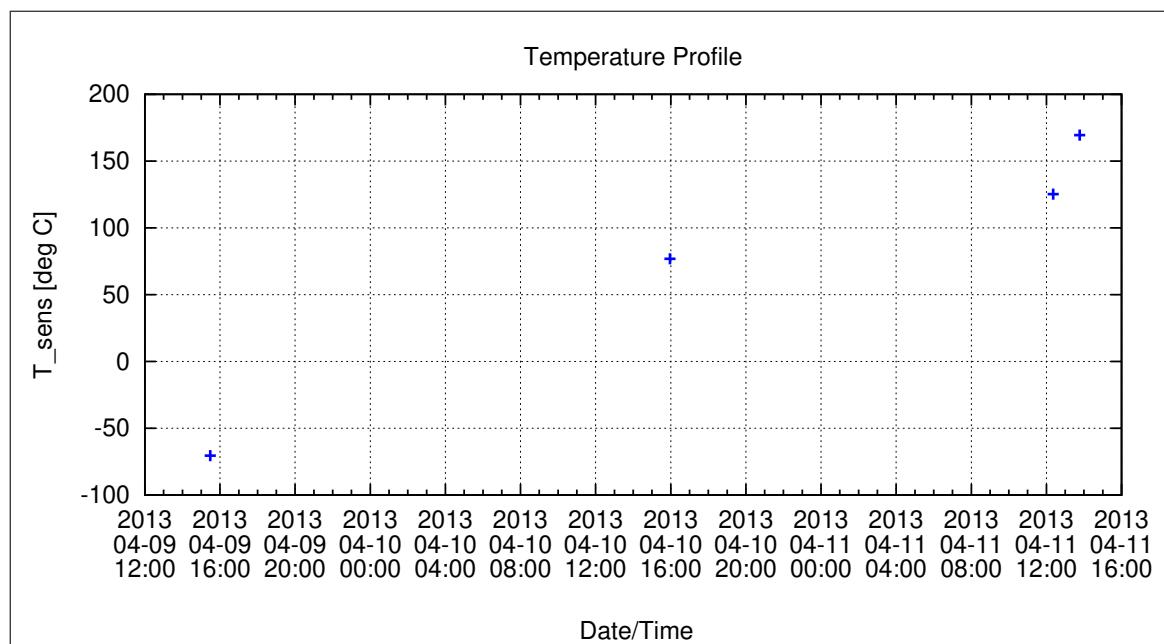


Figure 107: Temperature Profile

Coil System Temperature

The following graph shows the mean Coil System temperature during the complete thermal cycle for the AC measurements.

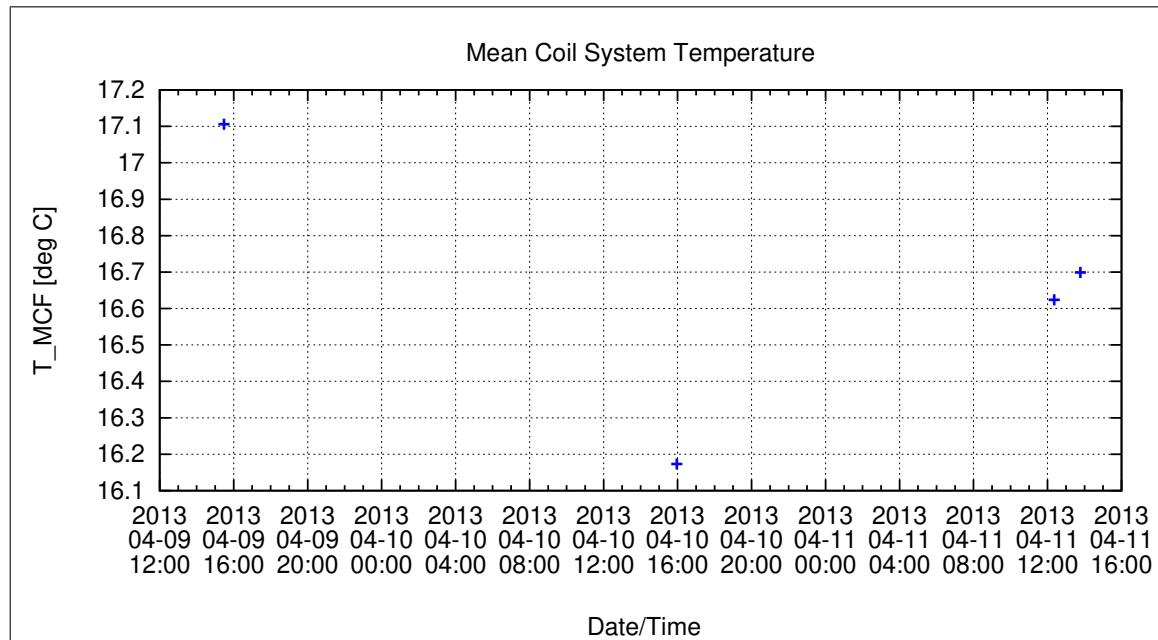


Figure 108: Coil System Temperature during Thermal AC Measurements

**Calibration Parameter:**-3dB Corner Frequency  $f_{3dB}$  vs. Temperature:

$$f_{3dB,i}(T) = \sum_{k=0}^n f_{3dB,k,i} T^k \quad [\text{Hz}, \text{ } ^\circ\text{C}], \ i=\{\text{x,y,z}\}$$

	$f_{3dB,0,i}$	$f_{3dB,1,i}$	$f_{3dB,2,i}$	$f_{3dB,3,i}$	$f_{3dB,4,i}$	$f_{3dB,5,i}$
$f_{3dB,x}$	5.87823E+1	7.50885E-3				
$f_{3dB,y}$	5.88830E+1	7.81382E-3				
$f_{3dB,z}$	5.59134E+1	2.01382E-2				

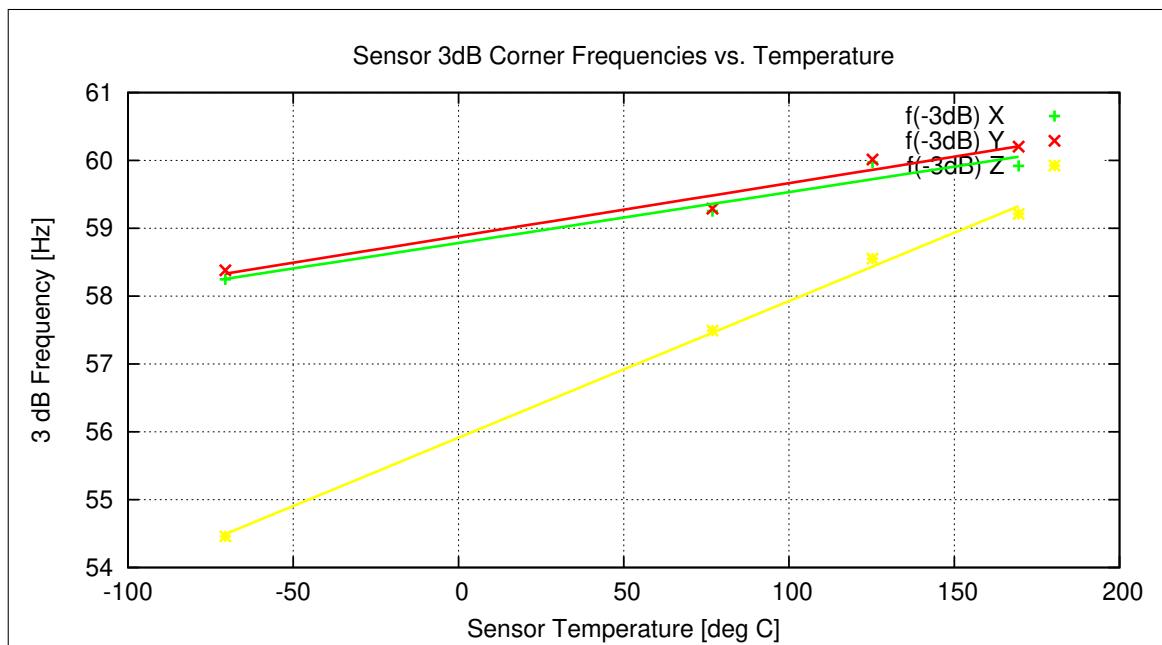


Figure 109: Temperature dependence of 3dB Corner Frequency

Instrument Sampling Frequency:

The following graph shows the calculated sampling frequencies vs. the actual sensor temperature.

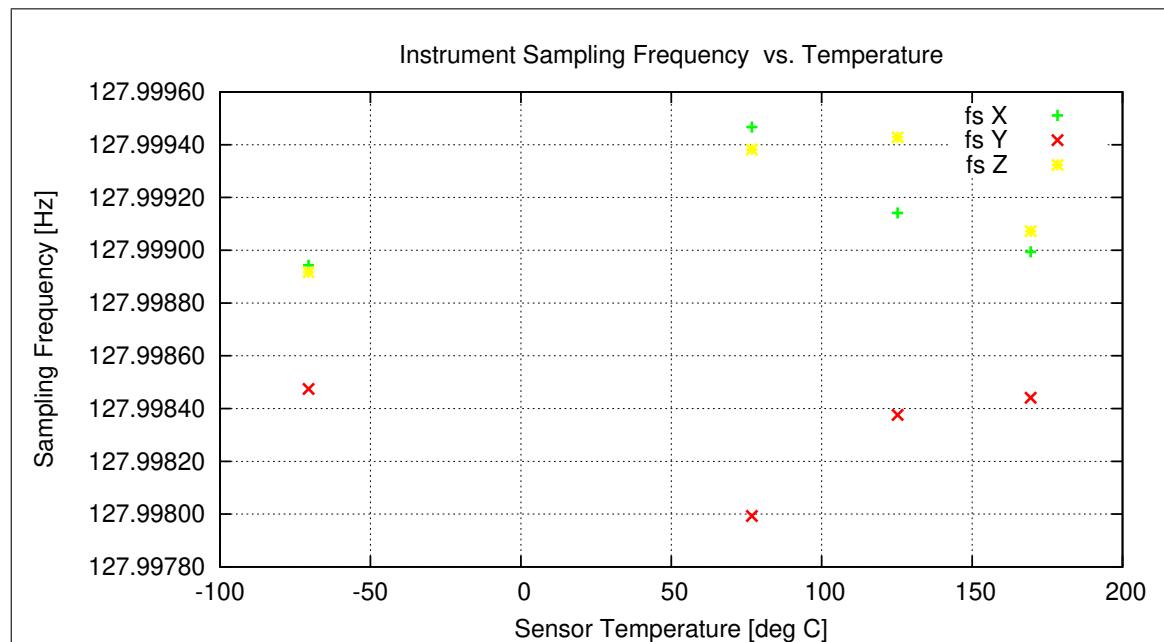


Figure 110: Instrument Sampling Frequency versus Sensor Temperature

Mean Samplerate: 127.998886 Hz.

Mean Standard Deviation of Samplerate: 0.000095 Hz.

## 14 Complete Temperature Profile

The following plot shows the complete thermal cycle of the sensor with all cooling and heating phases. The curves show the desired nominal temperatures in green and the actual measured temperatures in red.

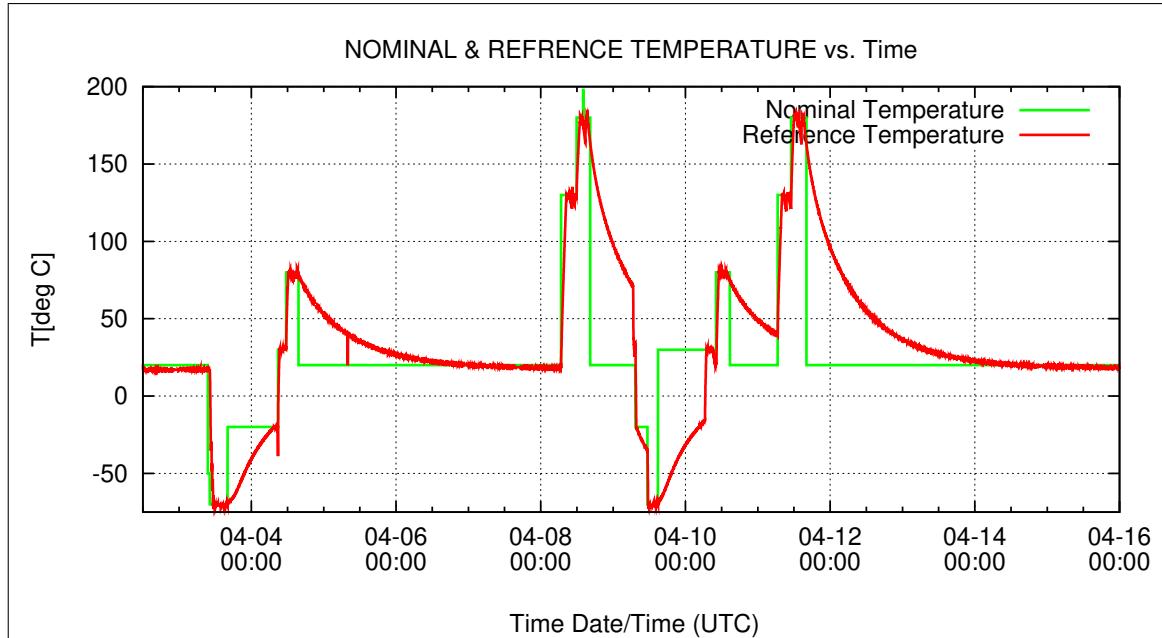


Figure 111: Complete thermal cycle

## 15 Mathematical Description of the Calibration

### 15.1 Basic Principle

The Magnetsrode Coil Facility (MCF) generates an artificial magnetic field  $\underline{B}^{\text{FLD}}$  that can be considered as a calibrated, orthogonal magnetic reference field<sup>1</sup> defined in coilsystem coordinates. For the calibration analysis this ideal coilsystem field is rotated to ideal orthogonal sensor coordinates using a nominal Rotation matrix  $\underline{\underline{R}}_{\text{nom}}$  at the first step. Nominal means that only rotations of  $\pm 90^\circ$  or  $\pm 180^\circ$  at any axis are considered here to get a coarse alignment of the applied field with the sensor-axes.

$$\underline{B}^c = \underline{\underline{R}}_{\text{nom}} \underline{B}^{\text{FLD}}$$

For a standard calibration the matrix  $\underline{\underline{R}}_{\text{nom}}$  is just a  $\underline{\underline{I}}$  - matrix - sensor coordinates and coilsystem coordinates have roughly the same direction. If the sensor coordinates are left-handed or the sensor is turned by about  $\pm 90^\circ$  or  $\pm 180^\circ$  at any axis  $\underline{\underline{R}}_{\text{nom}}$  will contain  $\pm 1$ -elements or 0-elements at any place. The rotated coil system field  $\underline{B}^c$  is the used reference field for the following analysis.

The magnetometer under test at the center of the coil system (CoC) generates magnetic raw data  $\underline{B}^r$ . These data include an eventually existing residual field of the coil system  $\underline{B}^{\text{res}}$  and the magnetometer offset  $\underline{B}^{\text{off}}$ . Both entities are combined in the offset & residual field  $\underline{B}^{\text{or}}$ :

$$\underline{B}^{\text{or}} = \underline{B}^{\text{off}} + \underline{B}^{\text{res}}$$

Therefore, the second step of the calibration is the generation of offset and residual field corrected measured field data  $\underline{B}^m$ :

$$\underline{B}^m = \underline{B}^r - \underline{B}^{\text{or}}$$

The actual offset and residual field is automatically taken into account during the calibration analysis. Either a constant field or - if needed - a linear trend of  $\underline{B}^{\text{or}}$  is subtracted from the raw data.

The relation between the calibration field and the magnetometer data is then defined by

$$\underline{B}^c = \underline{\underline{\Phi}} \underline{B}^m$$

where  $\underline{\underline{\Phi}}$  is the complete calibration transfer matrix, defined by

$$\underline{\underline{\phi}} = \underline{\underline{R}}_{\text{nom}} \underline{\underline{\rho}} \underline{\underline{\omega}} \underline{\underline{\sigma}},$$

---

<sup>1</sup>During the calibration the temperature dependent sensitivity of the coil system is calculated every 3 minutes and taken into account as well as the static misalignment of the coil system to produce orthogonal, known fields.

$\underline{\underline{\sigma}}(T)$  represents the temperature dependent sensitivity.

$\underline{\underline{\omega}}(T)$  describes the temperature dependent internal sensor misalignment (orthogonalisation matrix).

$\underline{\underline{\rho}}(T)$  describes the real rotation of the sensor against the coil axes.<sup>2</sup>

Thus the calibration algorithms have to solve the following problem:

$$\begin{aligned}\underline{\underline{B}}^c &= \underline{\underline{\Phi}} \underline{\underline{B}}^m \\ &= \underline{\underline{R}}_{\text{nom}} \underline{\underline{\rho}} \underline{\underline{\omega}} \underline{\underline{\sigma}} \underline{\underline{B}}^m\end{aligned}\quad (1)$$

The separation into these submatrices and evaluation of their elements is done in subsequent steps:

- Calculation of the Sensitivity matrix  $\underline{\underline{\sigma}}$

The sensitivity matrix shall contain the on-axis sensitivity coefficients of the sensors. Therefore,  $\underline{\underline{\sigma}}$  has to be a diagonal matrix of the following kind:

$$\underline{\underline{\sigma}} = \begin{pmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{pmatrix}$$

The separation of matrix  $\underline{\underline{\sigma}}$  from the transfer function  $\underline{\underline{\phi}}$  yields

$$\underline{\underline{\phi}} = \begin{pmatrix} \frac{\phi_{11}}{\sigma_1} & \frac{\phi_{12}}{\sigma_2} & \frac{\phi_{13}}{\sigma_3} \\ \frac{\phi_{21}}{\sigma_1} & \frac{\phi_{22}}{\sigma_2} & \frac{\phi_{23}}{\sigma_3} \\ \frac{\phi_{31}}{\sigma_1} & \frac{\phi_{32}}{\sigma_2} & \frac{\phi_{33}}{\sigma_3} \end{pmatrix} \begin{pmatrix} \sigma_1 & 0 & 0 \\ 0 & \sigma_2 & 0 \\ 0 & 0 & \sigma_3 \end{pmatrix} := \underline{\underline{\phi}} \underline{\underline{\sigma}}$$

For the computation of the sensitivity coefficients  $\sigma_i$  the transformation of the base-vectors has to be considered. Equation (1) transform the components of the fields, whereas

$$\underline{\underline{e}}^c = (\underline{\underline{\phi}}^T)^{-1} \underline{\underline{e}}^m := \underline{\underline{\Psi}} \underline{\underline{e}}^m$$

has to be used for the contragredient base-vector transformation of the skew sensorsystem  $\Sigma^m$  into the orthonormal coilsystem  $\Sigma^c$ . The length of the column vectors of  $\underline{\underline{\psi}}$  define the sensitivity coefficients  $\sigma_i$ :

$$\sigma_1 = \frac{1}{\sqrt{\psi_{11}^2 + \psi_{21}^2 + \psi_{31}^2}}$$

---

<sup>2</sup>Also the rotation matrix is regarded as temperature dependent being able to consider any thermal setup inadequacies causing fractional rotations.

$$\begin{aligned}\sigma_2 &= \frac{1}{\sqrt{\psi_{12}^2 + \psi_{22}^2 + \psi_{32}^2}} \\ \sigma_3 &= \frac{1}{\sqrt{\psi_{13}^2 + \psi_{23}^2 + \psi_{33}^2}}\end{aligned}$$

- Calculation of the Misalignment matrix  $\underline{\underline{\omega}}$

After the separation of  $\underline{\underline{\sigma}}$  the reduced transfer function  $\hat{\underline{\underline{\phi}}}$  contains only the misalignment and the real sensor rotation. The misalignment angles  $\xi_{xy}, \xi_{xz}, \xi_{yz}$ , hence the angles between the base vectors of the affine sensorsystem  $\Sigma^m$ , can be evaluated from the scalar products of all these base vectors. The base unit vectors are defined by the inverse transposed matrix of the reduced transfer function:

$$\begin{aligned}\underline{e}_x^m &:= \left( \begin{smallmatrix} \hat{\underline{\underline{\phi}}}^T \\ \underline{\underline{\phi}} \end{smallmatrix} \right)^{-1} \begin{pmatrix} 1 \\ 0 \\ 0 \end{pmatrix} \\ \underline{e}_y^m &:= \left( \begin{smallmatrix} \hat{\underline{\underline{\phi}}}^T \\ \underline{\underline{\phi}} \end{smallmatrix} \right)^{-1} \begin{pmatrix} 0 \\ 1 \\ 0 \end{pmatrix} \\ \underline{e}_z^m &:= \left( \begin{smallmatrix} \hat{\underline{\underline{\phi}}}^T \\ \underline{\underline{\phi}} \end{smallmatrix} \right)^{-1} \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}\end{aligned}$$

The misalignment angles can be derived from the scalar products:

$$\begin{aligned}\xi_{xy} &= \arccos(\underline{e}_x^m \cdot \underline{e}_y^m) \\ \xi_{xz} &= \arccos(\underline{e}_x^m \cdot \underline{e}_z^m) \\ \xi_{yz} &= \arccos(\underline{e}_y^m \cdot \underline{e}_z^m)\end{aligned}$$

Let's assume that the x-axis of the reference system  $\underline{e}_x^c$  is identical to the  $\underline{e}_x^m$ -axis of the sensor system. The angle between  $\underline{e}_y^c$  and  $\underline{e}_y^m$  is  $\beta$  (rotation angle around the  $\underline{e}_z^c$  axis). And the sensor  $\underline{e}_z^m$  axis can be constructed by a rotation of  $\eta$  in the  $\underline{e}_x^c, \underline{e}_y^c$ -plane and a second rotation of  $\gamma$  out of this plane. Then this misalignment of the base vectors is given by

$$\underline{\underline{Q}} = \begin{pmatrix} 1 & \sin \beta & \sin \gamma \\ 0 & \cos \beta & \cos \gamma \sin \eta \\ 0 & 0 & \cos \gamma \cos \eta \end{pmatrix} \quad (2)$$

By comparison of the angles  $\beta, \eta, \gamma$  with misalignment angles  $\xi_{xy}, \xi_{xz}, \xi_{yz}$ , the misalignment matrix (2) can be written in the following shape:

$$\underline{\underline{Q}} = \begin{pmatrix} 1 & \cos \xi_{xy} & \frac{\cos \xi_{xz}}{\sin \xi_{xy} - \cos \xi_{xy} \cos \xi_{xz}} \\ 0 & \sin \xi_{xy} & \frac{\sin \xi_{xy}}{\sin^2 \xi_{xz} - \frac{(\cos \xi_{yz} - \cos \xi_{xy} \cos \xi_{xz})^2}{\sin^2 \xi_{xy}}} \\ 0 & 0 & \sqrt{\sin^2 \xi_{xz} - \frac{(\cos \xi_{yz} - \cos \xi_{xy} \cos \xi_{xz})^2}{\sin^2 \xi_{xy}}} \end{pmatrix}$$

$\underline{\underline{Q}}$  transforms the base vectors. To achieve the transformation between the field components the transposed, inverse matrix of  $\underline{\underline{Q}}$  has to be calculated as the final misalignment matrix:

$$\underline{\underline{\omega}} = (\underline{\underline{Q}}^T)^{-1}$$

- Calculation of the Rotation matrix  $\underline{\underline{\rho}}$

With the knowledge of  $\underline{\underline{\omega}}$  and the nominal Setup matrix  $\underline{\underline{R}}_{\text{nom}}$  the rotation matrix  $\underline{\underline{\rho}}$  can be evaluated:

$$\underline{\underline{\rho}} = (\underline{\underline{R}}_{\text{nom}})^{-1} \stackrel{\wedge}{\underline{\underline{\phi}}} (\underline{\underline{\omega}})^{-1}$$

From this rotation matrix the actual rotation angles of the sensor wrt. the coil system can be calculated using again the scalar product:

$$\begin{aligned} \lambda &:= \arccos \left( \left[ \begin{array}{c} \underline{\underline{\rho}} \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \end{array} \right] \cdot \begin{bmatrix} 1 \\ 0 \\ 0 \end{bmatrix} \right) \\ \mu &:= \arccos \left( \left[ \begin{array}{c} \underline{\underline{\rho}} \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \end{array} \right] \cdot \begin{bmatrix} 0 \\ 1 \\ 0 \end{bmatrix} \right) \\ \nu &:= \arccos \left( \left[ \begin{array}{c} \underline{\underline{\rho}} \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \end{array} \right] \cdot \begin{bmatrix} 0 \\ 0 \\ 1 \end{bmatrix} \right) \end{aligned}$$

The rotation matrix  $\underline{\underline{\rho}}$  and the rotation angles  $\lambda, \mu, \nu$  are of interest just for the calibration to determine the right magnetometer parameters.

The transfer function for the normal use of the magnetometer is just given by

$$\stackrel{\sim}{\underline{\underline{\phi}}} = \underline{\underline{\omega}} \underline{\underline{\sigma}}$$

## 16 Nomenclature

### Abbreviations in theoretical sections:

Item	Meaning
$\underline{B}^c$	Magnetic calibration field generated by coil system
$\underline{B}^{off}$	Offset of the magnetometer [nT]
$\underline{B}_k^{off}$	Polynomial Fit coefficients for the sensor offset vs. temperature
$\underline{B}^m$	Measured magnetic field raw data, offset & residual field corrected [nT]
$\underline{B}^{or}$	$= \underline{B}^{off} + \underline{B}^{res}$ , Offset + Residual field at CoC [enT]
$\underline{B}^r$	Magnetic field raw data
$B_{0^\circ}^r$	Magnetic raw data, measured in normal position ( $0^\circ$ )[enT]
$B_{180^\circ}^r$	Magnetic raw data, measured in turned position ( $180^\circ$ )[enT]
$\underline{B}^{res}$	Residual field of the coil system
$e^\circ C$	Engineering degrees centigrade units
enT	Engineering NanoTesla units
$c_0, c_1, c_2, c_3$	Fit coefficients of the sensor thermistor
i	component x   y   z
CoC	Center of Coil system
DUT	Device under Test
$\underline{\underline{\phi}}$	$= \underline{R}_{\text{nom}} \underline{\rho} \underline{\underline{\omega}} \underline{\underline{\sigma}}$ , Calibration Transfer Matrix
$\underline{\underline{\phi}}^{\wedge}$	$= \underline{\underline{\omega}} \underline{\underline{\sigma}}$ , Transfer Matrix
$\underline{\underline{\phi}}^{\wedge}$	$= \underline{\underline{\phi}} \underline{\underline{\sigma}}^{-1}$ , Reduced Transfer Matrix
$\underline{\underline{\psi}}$	$= (\underline{\underline{\phi}}^T)^{-1}$ , Auxilliary transfer matrix
$\underline{\underline{O}}$	Base vector Orthogonalisation matrix
$\underline{\underline{\omega}}$	$= (\underline{\underline{Q}}^T)^{-1}$ , Field components orthogonalisation matrix
$\underline{\underline{R}}_{\text{nom}}$	Nominal Rotation matrix of sensor vs. coil system
$\underline{\underline{\rho}}$	$=$ Actual rotation matrix
$\underline{\underline{\sigma}}$	Sensitivity matrix
$\sigma_{k,i}$	Polynomial Fit coefficient for sensitivity vs. temperature.
TeMeSys	Coefficient of order $k$ for the sensor component $i$
$T_s^c$	MRode Temperature Measurement System
$T_s^r$	Temperature of sensor s, calibrated data [ $^\circ C$ ]
s	Temperature of sensor s, raw data [ $e^\circ C$ ]
$U_T, IB$	Sensor IB   OB
$U_{T,OB}$	IB-Temperature data [V], measured
$\xi_{ij}$	OB-Temperature data [V], measured
$\xi_{k,ij}^0$	Temperature dependent alignment angle (ij component)
	Polynomial Fit coefficient for misalignment angle vs. temperature.
$\lambda, \mu, \nu$	Coefficient of order $k$ for the angle $ij$
	Rotation angles wrt. coil system reference coordinates.