

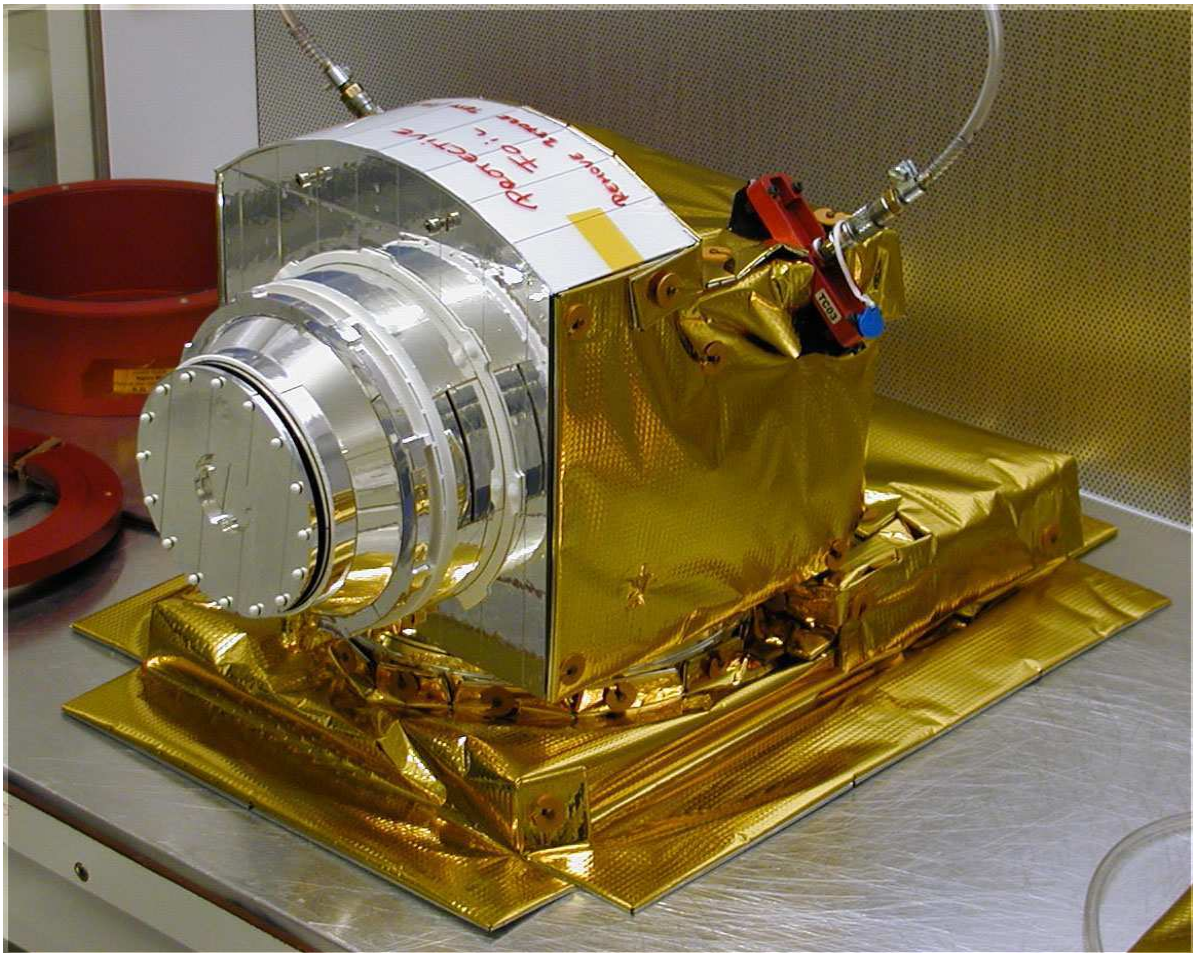
**Venus Express**

**ASPERA-4**

**ELS Data Analysis Summary**

**v2.0**

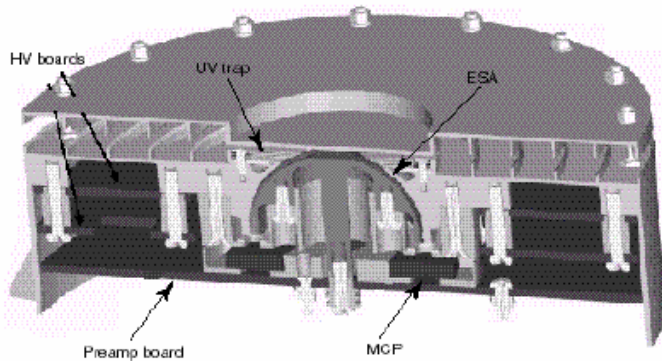
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# 1. ASPERA-4 Electron Spectrometer



**Figure 1: Cutaway diagram of ELS**

The ELS instrument was manufactured by South-west Research Institute (SwRI) in San Antonio, Texas as the Flight Spare for Mars Express. It represents a new generation of ultra-light, low-power, electron sensor (Barabash et al, 2004). It is formed by a spherical top-hat electrostatic analyzer and a collimator system (Figure 1). Particles enter the aperture at any angle in the plane of incidence. Electrons are then deflected into the spectrometer by applying a positive voltage to

the inner spherical electron deflection plate. The electrons hit a micro channel plate (MCP) after being filtered in energy by the analyzer plates. The plates are stepped in voltage to achieve an energy spectrum. Electrons with energies up to 20 keV/q will be measured, with a maximum time resolution of one energy sweep per four seconds. There are 16 anodes behind the MCP, each anode defining a 22.5° sector and each connected to a preamplifier. The ELS sensor will be mounted on the ASPERA-4 scan platform, on top of the NPI sensor, in such a way that the full 4- $\pi$  angular distribution of electrons will be measured during each platform scan.

## 2. MSSL calibration facility

The design of MSSL's calibration facility for electron instruments is based on Marshall et al, 1986. The calibration system is housed in a cylindrical stainless steel vacuum chamber. A grounded  $\mu$ -metal shroud inside the chamber, enclosed at both ends, ensures that the residual magnetic field inside the chamber is less than one tenth of the Earth's magnetic field; this results in an electron beam divergence of less than 1° at 1keV.

Light from a mercury UV lamp outside the vacuum chamber is transmitted through a quartz window on to a gold-coated quartz disc inside the chamber. Over 90% of the output wavelength of the lamp is at the 253.7nm mercury line. The energy of the incident UV light is just sufficient to knock photoelectrons out of the gold layer on the quartz disc and as a result, the kinetic energy of the ejected photoelectrons is small (~0.3eV). These electrons are then accelerated by an electric field and emerge through the grid with an energy defined by the applied voltage (between 5eV and 10keV). The intensity of the beam can be varied by placing one of a series of neutral density filters in front of the UV lamp. The cross-section of the resulting electron beam is approximately 120mm in diameter.

The instrument to be calibrated is mounted on a 2-axis rotary table, which allows movement of the instrument over the complete azimuthal and elevation



**Figure 3: The Venus Express ASPERA-4 ELS sensor mounted in the MSSL calibration facility**

angle response range. The mounting is such that the centre of the instrument aperture is at the centre of rotation of both the axes. This ensures that the centre of the aperture is always illuminated by the same area of the beam. A channeltron is mounted as close as possible to the instrument aperture in order to provide a constant reference to the beam intensity. A schematic diagram of the calibration facility is shown in Figure 2. A photograph of the Venus Express ASPERA-4 instrument inside the MSSL calibration facility is presented in Figure 3.

### 3. Energy-angle scans

All of the analyser parameters are extracted from the Energy (sweep voltage) – Angle scans carried out at the centre of each anode for beam energies of 10eV, 30 eV, 50eV, 70eV, 100eV, 200eV, 1 keV, 3 keV, 6 keV, 10 keV, 12 keV. An example plot at 200 eV is shown in Figure 4.

### 4. K-factors

Figure 5 is a plot of the lab-measured k-factor for the 10 energies, shown as different colour lines. Table 1 shows the energy-averaged k-factors for each anode.

Table 1: Energy sensitivity for each anode (eV/V)

0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
10.490	10.627	10.824	10.956	11.077	11.192	11.310	11.397	11.315	11.193	11.007	10.808	10.558	10.419	10.355	10.363

A 4D polynomial fit to the values above gives the following relationship between k-factor (k) and anode (a):

$$(1) \quad k = 10.518 + 0.0424a + 0.0573a^2 - 0.00889 a^3 + 0.000323 a^4$$

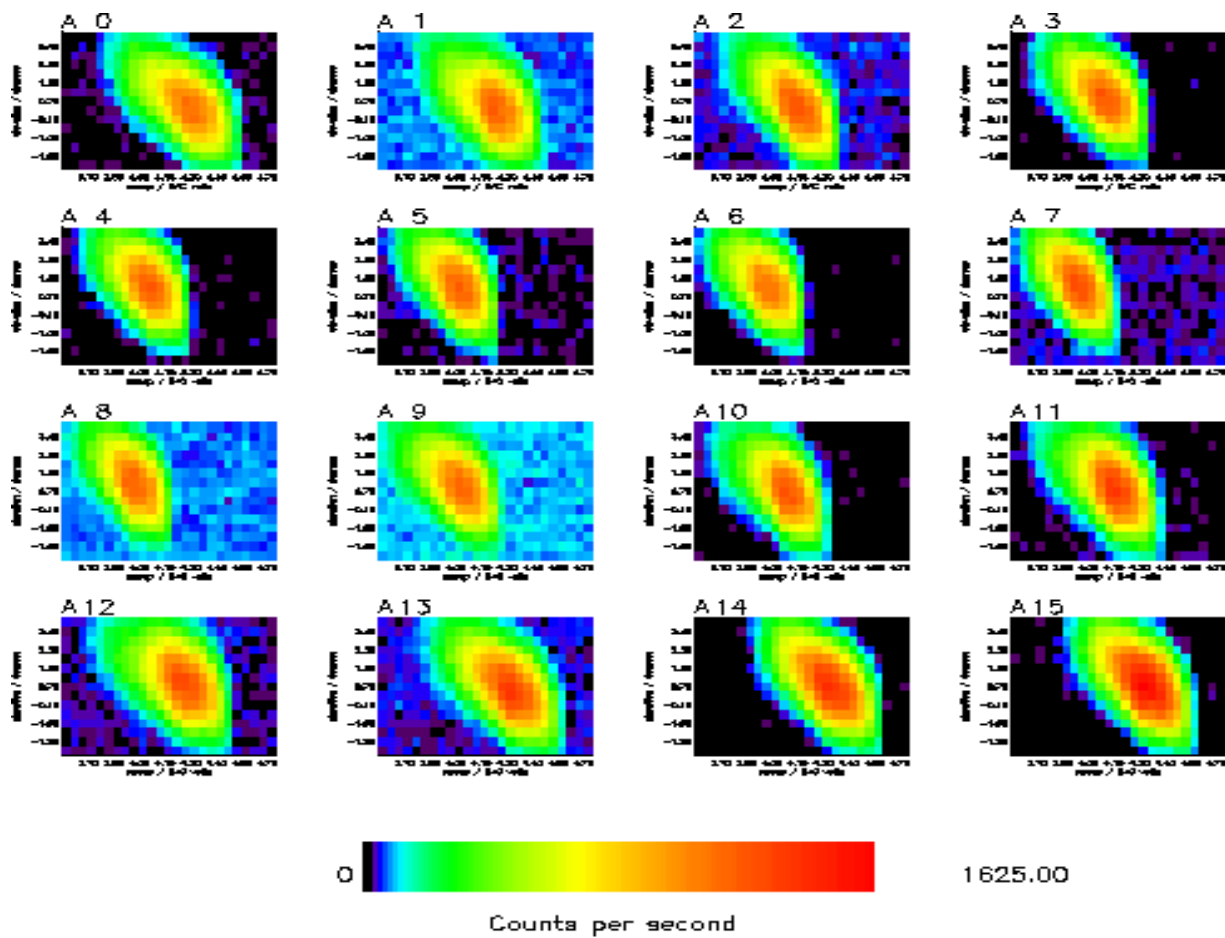


Figure 4: Energy-angle response of ELS at 200eV electron beam energy

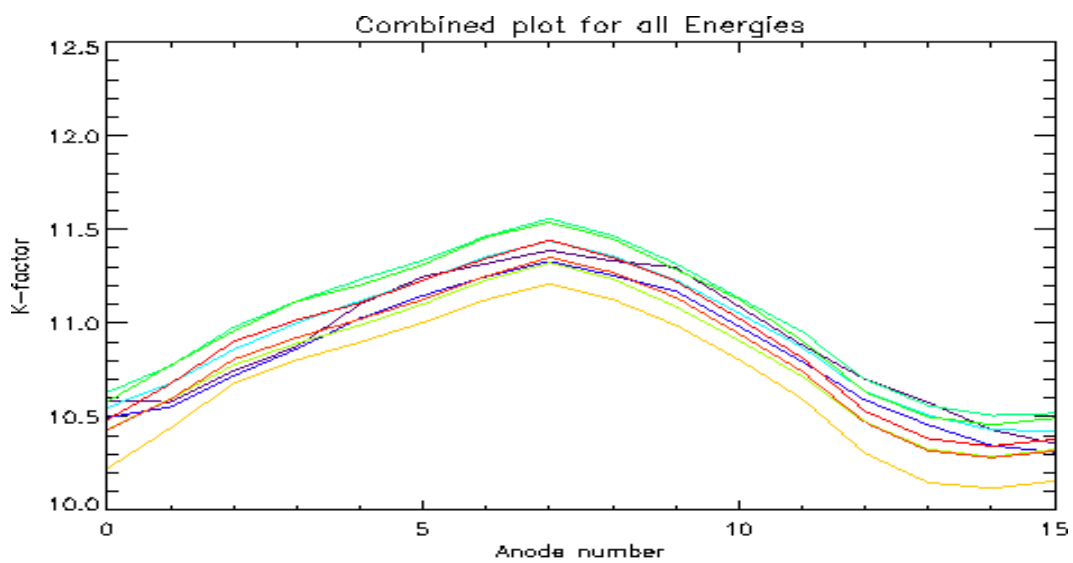
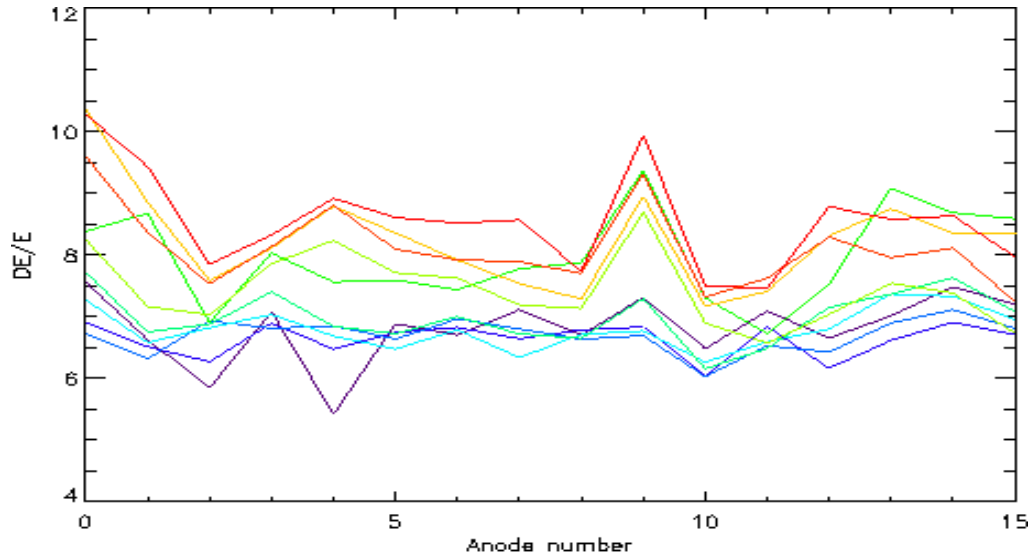


Figure 5: Plot of analyser k-factor across the 16 anodes for 10 beam energies

## 5. Energy Resolution

Figure 6 is a plot of the energy resolution across the 16 anodes. The measured values are given in Table 2.



**Figure 6: Plot of energy resolution across the 16 anodes for 10 beam energies**

Table 2: Laboratory measured energy resolutions

Energy(eV) Anode	29.9200	50.3000	70.2000	100.400	199.990	970.000	3021.00	5994.00	9990.00	11997.0
0	7.56060	6.90909	6.72312	7.27587	7.72092	8.50001	8.24999	10.3585	9.60001	10.2789
1	6.63077	6.51376	6.31894	6.58139	6.75295	8.47059	7.16505	8.85577	8.36232	9.43137
2	5.84375	6.27102	6.93560	6.82143	6.87952	6.90908	7.03000	7.58824	7.53731	7.84849
3	7.07937	6.89624	6.81164	7.03614	7.40244	8.31249	7.85859	8.11000	8.13636	8.32654
4	5.41935	6.47620	6.85121	6.68675	6.84146	7.53125	8.23470	8.78788	8.80303	8.91752
5	6.88524	6.74758	6.63986	6.47561	6.72839	7.43750	7.71134	8.35714	8.09231	8.60825
6	6.70492	6.82524	6.96503	6.78750	7.00000	7.71875	7.62500	7.91752	7.92188	8.51579
7	7.11667	6.64357	6.80357	6.33751	6.72151	7.29032	7.18750	7.53609	7.89063	8.56842
8	6.70492	6.78431	6.63604	6.71606	6.65000	7.43750	7.13541	7.28866	7.70313	7.73958
9	7.31147	6.83496	6.69231	6.76830	7.29630	7.84376	8.69388	8.94950	9.30769	9.93815
10	6.48387	6.02885	6.03114	6.26507	6.15854	7.43750	6.89898	7.17000	7.31819	7.50000
11	7.09523	6.83962	6.52881	6.59524	6.48810	6.36364	6.57426	7.41176	7.62686	7.46000
12	6.65626	6.16667	6.42857	6.80233	7.15116	8.02941	7.03847	8.31429	8.28986	8.78640
13	7.01538	6.61817	6.89903	7.36781	7.36781	8.64707	7.54286	8.74528	7.95715	8.57693
14	7.48485	6.90991	7.11290	7.32955	7.63219	8.88235	7.38095	8.35515	8.11428	8.63460
15	7.19697	6.71171	6.81108	6.95454	7.08045	7.79412	6.73333	8.33962	7.24286	7.97116

Using the data in Table 2, we find that the energy resolution,  $\Delta E/E$ , for each anode can be fit to the log of the energy ( $E$ ) by the equation:

$$(2) \quad \Delta E/E = m_0 + m_1 \log_{10}(E)$$

The coefficients  $m_0$  and  $m_1$  are given for each anode in Table 3:

Table 3: Coefficients for energy resolution straight line fit

Anode	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
$m_0$	4.969	4.749	5.507	6.063	4.293	5.366	5.780	5.735	5.991	4.928	5.302	6.190	5.141	5.943	6.469	6.347
$m_1$	1.211	0.998	0.528	0.555	1.143	0.724	0.585	0.533	0.394	1.098	0.516	0.256	0.805	0.626	0.475	0.339

## 6. Fine polar scans

The energy-angle scans also provide the peak response of the instrument for each energy. In order to obtain the relative response of the instrument, a fine scan is carried out at polar steps of 0.25 degrees across the polar range of  $\pm 168.75^\circ$  at the peak elevation and voltage. Figure 7 is an example of the response at 100 eV.

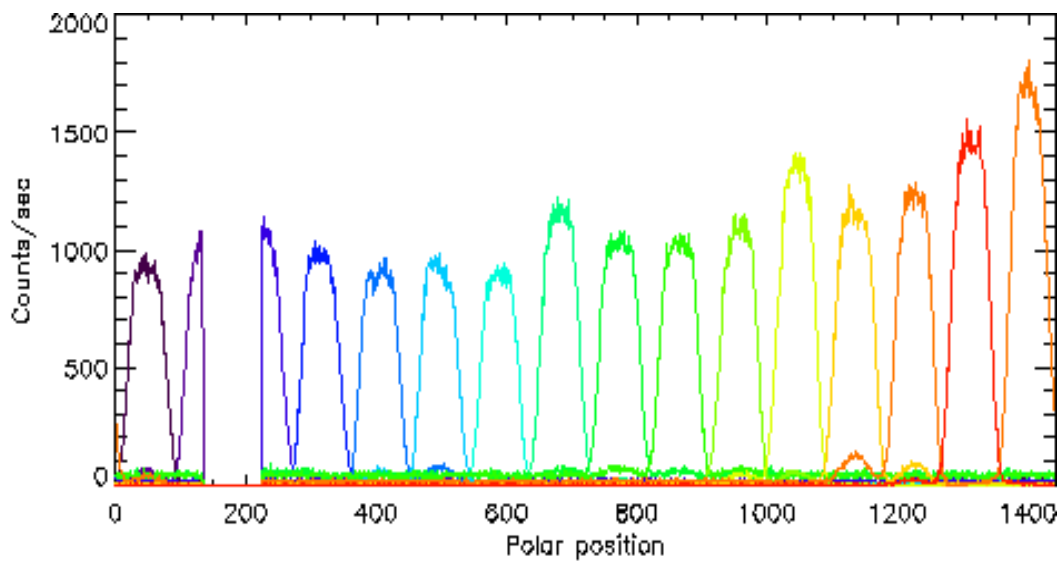


Figure 7: Plot of the analyser response at peak elevation and sweep voltage at fine polar steps in a 100eV beam

## 7. Energy Table

The Venus Express engineering telemetry (TM) packets include indices representing the deflection reference voltage applied to the ELS. The anode-dependent centre energies are calculated using this TM index. There are two deflection power supplies – the low range supply, which produces a voltage from 0V to 21.8V, and the high range supply which covers 0V to 2777V. For each setting, the TM packet gives the range and the index for the power supply. The index can be between 0 at 4095. If the deflection range is Low, the deflection plate voltage requested is determined by the equation:

$$(3) \quad \text{Low Range Reference Deflection Voltage [volts]} = \text{TM} * (21.8 / 4095)$$

If the deflection range is High, the voltage requested on the deflection plates is determined by the equation:

(4) High Range Reference Deflection Voltage [volts] = TM \* (2777.0 / 4095)

To convert these voltages to anode-dependent energies, they are simply multiplied by the k-factors as calculated using the anode-dependent relationship, Equation (1), given in Section 4.

Table 4 shows the centre energy values, for each anode, for the 127 energy steps most commonly used in the standard 4s resolution measurements. It also gives the TM index, and which power supply is being used. Table 5 shows the centre energy values for the 31 energy steps used in the 1s resolution measurements.

Table 4: The anode-dependent 4s energy table using the k-factors from Table 1. Energies in eV.

Power Supply	TM Index	Anode/Energy	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
Low	16	1	0.89 5892	0.90 3655	0.91 7020	0.93 2436	0.94 7009	0.95 8508	0.96 5360	0.96 6653	0.96 2137	0.95 2219	0.93 7969	0.92 1118	0.90 4053	0.88 9825	0.88 2145	0.88 5383
Low	18	2	1.00 788	1.01 661	1.03 165	1.04 899	1.06 539	1.07 832	1.08 603	1.08 748	1.08 240	1.07 125	1.05 522	1.03 626	1.01 706	1.00 105	0.99 2413	0.99 6056
Low	19	3	1.06 387	1.07 309	1.08 896	1.10 727	1.12 457	1.13 823	1.14 636	1.14 790	1.14 254	1.13 076	1.11 384	1.09 383	1.07 356	1.05 667	1.04 755	1.05 139
Low	21	4	1.17 586	1.18 605	1.20 359	1.22 382	1.24 295	1.25 804	1.26 703	1.26 873	1.26 280	1.24 979	1.23 108	1.20 897	1.18 657	1.16 790	1.15 782	1.16 207
Low	23	5	1.28 784	1.29 900	1.31 822	1.34 038	1.36 133	1.37 786	1.38 770	1.38 956	1.38 307	1.36 881	1.34 833	1.32 411	1.29 958	1.27 912	1.26 808	1.27 274
Low	25	6	1.39 983	1.41 196	1.43 284	1.45 693	1.47 970	1.49 767	1.50 837	1.51 040	1.50 334	1.48 784	1.46 558	1.43 925	1.41 258	1.39 035	1.37 835	1.38 341
Low	27	7	1.51 182	1.52 492	1.54 747	1.57 349	1.59 808	1.61 748	1.62 904	1.63 123	1.62 361	1.60 687	1.58 282	1.55 439	1.52 559	1.50 158	1.48 862	1.49 408
Low	29	8	1.62 380	1.63 787	1.66 210	1.69 004	1.71 645	1.73 730	1.74 971	1.75 206	1.74 387	1.72 590	1.70 007	1.66 953	1.63 860	1.61 281	1.59 889	1.60 476
Low	32	9	1.79 178	1.80 731	1.83 404	1.86 487	1.89 402	1.91 702	1.93 072	1.93 331	1.92 427	1.90 444	1.87 594	1.84 224	1.80 811	1.77 965	1.76 429	1.77 077
Low	35	10	1.95 976	1.97 674	2.00 598	2.03 970	2.07 158	2.09 674	2.11 172	2.11 455	2.10 467	2.08 298	2.05 181	2.01 494	1.97 762	1.94 649	1.92 969	1.93 678
Low	38	11	2.12 774	2.14 618	2.17 792	2.21 454	2.24 915	2.27 646	2.29 273	2.29 580	2.28 507	2.26 152	2.22 768	2.18 765	2.14 713	2.11 333	2.09 509	2.10 279
Low	41	12	2.29 572	2.31 561	2.34 986	2.38 937	2.42 671	2.45 618	2.47 373	2.47 705	2.46 548	2.44 006	2.40 355	2.36 036	2.31 664	2.28 018	2.26 050	2.26 879
Low	45	13	2.51 970	2.54 153	2.57 912	2.62 248	2.66 346	2.69 580	2.71 507	2.71 871	2.70 601	2.67 812	2.63 804	2.59 064	2.54 265	2.50 263	2.48 103	2.49 014
Low	49	14	2.74 367	2.76 744	2.80 837	2.85 559	2.90 022	2.93 543	2.95 641	2.96 038	2.94 654	2.91 617	2.87 253	2.82 092	2.76 866	2.72 509	2.70 157	2.71 149
Low	53	15	2.96 764	2.99 336	3.03 763	3.08 869	3.13 697	3.17 506	3.19 775	3.20 204	3.18 708	3.15 423	3.10 702	3.05 120	2.99 467	2.94 755	2.92 211	2.93 283
Low	57	16	3.19 162	3.21 927	3.26 688	3.32 180	3.37 372	3.41 468	3.43 909	3.44 370	3.42 761	3.39 228	3.34 152	3.28 148	3.22 069	3.17 000	3.14 264	3.15 418
Low	62	17	3.47 158	3.50 166	3.55 345	3.61 319	3.66 966	3.71 422	3.74 077	3.74 578	3.72 828	3.68 985	3.63 463	3.56 933	3.50 320	3.44 807	3.41 831	3.43 086
Low	68	18	3.80 754	3.84 053	3.89 734	3.96 285	4.02 479	4.07 366	4.10 278	4.10 828	4.08 908	4.04 693	3.98 637	3.91 475	3.84 222	3.78 176	3.74 912	3.76 288
Low	74	19	4.14 350	4.17 940	4.24 122	4.31 252	4.37 992	4.43 310	4.46 479	4.47 077	4.44 988	4.40 401	4.33 811	4.26 017	4.18 124	4.11 544	4.07 992	4.09 490
Low	80	20	4.47 946	4.51 827	4.58 510	4.66 218	4.73 505	4.79 254	4.82 680	4.83 327	4.81 068	4.76 110	4.68 985	4.60 559	4.52 026	4.44 913	4.41 073	4.42 692
Low	87	21	4.87 141	4.91 362	4.98 630	5.07 012	5.14 936	5.21 189	5.24 914	5.25 618	5.23 162	5.17 769	5.10 021	5.00 858	4.91 579	4.83 842	4.79 666	4.81 427
Low	95	22	5.31 936	5.36 545	5.44 481	5.53 634	5.62 287	5.69 114	5.73 182	5.73 950	5.71 269	5.65 380	5.56 919	5.46 914	5.36 781	5.28 334	5.23 774	5.25 696
Low	103	23	5.76 731	5.81 728	5.90 332	6.00 256	6.09 637	6.17 039	6.21 450	6.22 283	6.19 375	6.12 991	6.03 818	5.92 969	5.81 984	5.72 825	5.67 881	5.69 965
Low	112	24	6.27 124	6.32 558	6.41 914	6.52 705	6.62 906	6.70 955	6.75 752	6.76 657	6.73 496	6.66 553	6.56 579	6.44 782	6.32 837	6.22 878	6.17 501	6.19 768
Low	121	25	6.77 518	6.83 389	6.93 496	7.05 155	7.16 176	7.24 872	7.30 053	7.31 031	7.27 616	7.20 116	7.09 309	6.96 595	6.83 690	6.72 930	6.67 122	6.69 571
Low	132	26	7.39	7.45	7.56	7.69	7.81	7.90	7.96	7.97	7.93	7.85	7.73	7.59	7.45	7.34	7.27	7.30

			111	515	542	260	283	769	422	489	763	581	825	922	844	106	770	441
Low	143	27	8.00 704	8.07 641	8.19 587	8.33 365	8.46 389	8.56 666	8.62 790	8.63 946	8.59 910	8.51 046	8.38 310	8.23 249	8.07 997	7.95 281	7.88 417	7.91 311
Low	155	28	8.67 896	8.75 415	8.88 363	9.03 297	9.17 415	9.28 554	9.35 192	9.36 445	9.32 070	9.22 462	9.08 658	8.92 333	8.75 801	8.62 018	8.54 578	8.57 715
Low	169	29	9.46 286	9.54 485	9.68 602	9.84 885	10.0 028	10.1 242	10.1 966	10.2 103	10.1 626	10.0 578	9.90 730	9.72 931	9.54 906	9.39 878	9.31 766	9.35 186
Low	183	30	10.2 468	10.3 355	10.4 884	10.6 647	10.8 314	10.9 629	11.0 413	11.0 561	11.0 044	10.8 910	10.7 280	10.5 353	10.3 401	10.1 774	10.0 895	10.1 266
Low	199	31	11.1 427	11.2 392	11.4 054	11.5 972	11.7 784	11.9 214	12.0 067	12.0 227	11.9 666	11.8 432	11.6 660	11.4 564	11.2 442	11.0 672	10.9 717	11.0 120
Low	216	32	12.0 945	12.1 993	12.3 798	12.5 879	12.7 846	12.9 399	13.0 324	13.0 498	12.9 888	12.8 550	12.6 626	12.4 351	12.2 047	12.0 126	11.9 090	11.9 527
Low	235	33	13.1 584	13.2 724	13.4 687	13.6 952	13.9 092	14.0 781	14.1 787	14.1 977	14.1 314	13.9 857	13.7 764	13.5 289	13.2 783	13.0 693	12.9 565	13.0 041
Low	255	34	14.2 783	14.4 020	14.6 150	14.8 607	15.0 930	15.2 762	15.3 854	15.4 060	15.3 341	15.1 760	14.9 489	14.6 803	14.4 083	14.1 816	14.0 592	14.1 108
Low	277	35	15.5 101	15.6 445	15.8 759	16.1 428	16.3 951	16.5 942	16.7 128	16.7 352	16.6 570	16.4 853	16.2 386	15.9 468	15.6 514	15.4 051	15.2 721	15.3 282
Low	301	36	16.8 540	17.0 000	17.2 514	17.5 415	17.8 156	18.0 319	18.1 608	18.1 852	18.1 002	17.9 136	17.6 455	17.3 285	17.0 075	16.7 398	16.5 954	16.6 563
Low	327	37	18.3 098	18.4 684	18.7 416	19.0 567	19.3 545	19.5 895	19.7 295	19.7 560	19.6 637	19.4 610	19.1 698	18.8 253	18.4 766	18.1 858	18.0 288	18.0 950
Low	355	38	19.8 776	20.0 498	20.3 464	20.6 884	21.0 118	21.2 669	21.4 189	21.4 476	21.3 474	21.1 274	20.8 112	20.4 373	20.0 587	19.7 430	19.5 726	19.6 444
Low	385	39	21.5 574	21.7 442	22.0 658	22.4 367	22.7 874	23.0 641	23.2 290	23.2 601	23.1 514	22.9 128	22.5 699	22.1 644	21.7 538	21.4 114	21.2 266	21.3 045
Low	419	40	23.4 612	23.6 645	24.0 145	24.4 182	24.7 998	25.1 009	25.2 804	25.3 142	25.1 960	24.9 362	24.5 631	24.1 218	23.6 749	23.3 023	23.1 012	23.1 860
Low	455	41	25.4 769	25.6 977	26.0 778	26.5 161	26.9 306	27.2 576	27.4 524	27.4 892	27.3 608	27.0 787	26.6 735	26.1 943	25.7 090	25.3 044	25.0 860	25.1 781
Low	494	42	27.6 607	27.9 003	28.3 130	28.7 890	29.2 389	29.5 939	29.8 055	29.8 454	29.7 060	29.3 998	28.9 598	28.4 395	27.9 126	27.4 734	27.2 362	27.3 362
Low	536	43	30.0 124	30.2 724	30.7 202	31.2 366	31.7 248	32.1 100	32.3 396	32.3 829	32.2 316	31.8 993	31.4 220	30.8 574	30.2 858	29.8 091	29.5 519	29.6 603
Low	582	44	32.5 881	32.8 704	33.3 566	33.9 174	34.4 475	34.8 657	35.1 150	35.1 620	34.9 977	34.6 370	34.1 186	33.5 057	32.8 849	32.3 674	32.0 880	32.2 058
Low	632	45	35.3 877	35.6 944	36.2 223	36.8 312	37.4 069	37.8 611	38.1 317	38.1 828	38.0 044	37.6 127	37.0 498	36.3 841	35.7 101	35.1 481	34.8 447	34.9 726
Low	687	46	38.4 674	38.8 007	39.3 745	40.0 365	40.6 622	41.1 559	41.4 501	41.5 057	41.3 117	40.8 859	40.2 741	39.5 505	38.8 178	38.2 069	37.8 771	38.0 161
Low	746	47	41.7 710	42.1 329	42.7 561	43.4 748	44.1 543	44.6 904	45.0 099	45.0 702	44.8 596	44.3 972	43.7 328	42.9 471	42.1 515	41.4 881	41.1 300	41.2 810
Low	810	48	45.3 545	45.7 475	46.4 241	47.2 046	47.9 423	48.5 245	48.8 713	48.9 368	48.7 082	48.2 061	47.4 847	46.6 316	45.7 677	45.0 474	44.6 586	44.8 225
Low	880	49	49.2 741	49.7 010	50.4 361	51.2 840	52.0 855	52.7 179	53.0 948	53.1 659	52.9 175	52.3 720	51.5 883	50.6 615	49.7 229	48.9 404	48.5 180	48.6 961
Low	955	50	53.4 736	53.9 369	54.7 346	55.6 548	56.5 246	57.2 109	57.6 199	57.6 971	57.4 275	56.8 356	55.9 851	54.9 792	53.9 606	53.1 114	52.6 530	52.8 463
Low	1037	51	58.0 650	58.5 681	59.4 344	60.4 335	61.3 780	62.1 233	62.5 674	62.6 512	62.3 585	61.7 157	60.7 921	59.6 999	58.5 939	57.6 718	57.1 740	57.3 839
Low	1127	52	63.1 044	63.6 512	64.5 926	65.6 785	66.7 050	67.5 149	67.9 975	68.0 886	67.7 705	67.0 719	66.0 682	64.8 812	63.6 792	62.6 771	62.1 361	62.3 642
Low	1223	53	68.4 798	69.0 731	70.0 947	71.2 731	72.3 870	73.2 659	73.7 897	73.8 885	73.5 433	72.7 853	71.6 960	70.4 079	69.1 035	68.0 160	67.4 290	67.6 765
Low	1329	54	74.4 150	75.0 598	76.1 700	77.4 505	78.6 609	79.6 161	80.1 852	80.2 926	79.9 175	79.0 937	77.9 101	76.5 103	75.0 929	73.9 111	73.2 732	73.5 421
Low	1443	55	80.7 983	81.4 984	82.7 038	84.0 941	85.4 084	86.4 454	87.0 634	87.1 800	86.7 727	85.8 783	84.5 931	83.0 733	81.5 343	80.2 511	79.5 585	79.8 505
Low	1567	56	87.7 414	88.5 017	89.8 107	91.3 204	92.7 477	93.8 739	94.5 449	94.6 716	94.2 293	93.2 579	91.8 624	90.2 119	88.5 407	87.1 472	86.3 951	86.7 122
Low	1702	57	95.3 005	96.1 263	97.5 480	99.1 879	100. 738	101. 961	102. 690	102. 828	102. 347	101. 292	99.7 765	97.9 839	96.1 686	94.6 552	93.8 382	94.1 826
Low	1848	58	103. 476	104. 372	105. 916	107. 696	109. 380	110. 708	111. 499	111. 648	111. 127	109. 981	108. 335	106. 389	104. 418	102. 775	101. 888	102. 262
Low	2007	59	112. 378	113. 352	115. 029	116. 962	118. 790	120. 233	121. 092	121. 255	120. 688	119. 444	117. 657	115. 543	113. 402	111. 617	110. 654	111. 060
Low	2179	60	122.	123.	124.	126.	128.	130.	131.	131.	131.	129.	127.	125.	123.	121.	120.	120.



			009	066	887	986	971	537	470	646	031	680	740	445	121	183	137	578
Low	2366	<b>61</b>	132. 480	133. 628	135. 604	137. 884	140. 039	141. 739	142. 753	142. 944	142. 276	140. 809	138. 702	136. 210	133. 687	131. 583	130. 447	130. 926
Low	2570	<b>62</b>	143. 903	145. 150	147. 296	149. 773	152. 113	153. 960	155. 061	155. 269	154. 543	152. 950	150. 661	147. 954	145. 213	142. 928	141. 695	142. 215
Low	2791	<b>63</b>	156. 277	157. 631	159. 963	162. 652	165. 194	167. 200	168. 395	168. 621	167. 833	166. 103	163. 617	160. 677	157. 701	155. 219	153. 879	154. 444
Low	3031	<b>64</b>	169. 716	171. 186	173. 718	176. 638	179. 399	181. 577	182. 875	183. 120	182. 265	180. 386	177. 687	174. 494	171. 261	168. 566	167. 111	167. 725
Low	3291	<b>65</b>	184. 274	185. 870	188. 620	191. 790	194. 788	197. 153	198. 562	198. 828	197. 899	195. 860	192. 929	189. 462	185. 952	183. 026	181. 446	182. 112
Low	3574	<b>66</b>	200. 120	201. 854	204. 839	208. 283	211. 538	214. 107	215. 637	215. 926	214. 917	212. 702	209. 519	205. 755	201. 943	198. 765	197. 049	197. 772
Low	3881	<b>67</b>	217. 310	219. 193	222. 435	226. 174	229. 709	232. 498	234. 160	234. 474	233. 378	230. 973	227. 516	223. 429	219. 289	215. 838	213. 975	214. 761
High	31	<b>68</b>	221. 114	223. 030	226. 329	230. 134	233. 730	236. 568	238. 260	238. 579	237. 464	235. 016	231. 499	227. 340	223. 128	219. 617	217. 721	218. 521
High	34	<b>69</b>	242. 512	244. 614	248. 232	252. 405	256. 350	259. 462	261. 317	261. 667	260. 444	257. 760	253. 903	249. 341	244. 721	240. 870	238. 791	239. 668
High	37	<b>70</b>	263. 911	266. 197	270. 134	274. 676	278. 969	282. 356	284. 374	284. 755	283. 425	280. 503	276. 306	271. 341	266. 315	262. 123	259. 861	260. 815
High	40	<b>71</b>	285. 309	287. 781	292. 037	296. 947	301. 588	305. 250	307. 432	307. 844	306. 405	303. 247	298. 709	293. 342	287. 908	283. 377	280. 931	281. 962
High	43	<b>72</b>	306. 707	309. 364	313. 940	319. 218	324. 207	328. 143	330. 489	330. 932	329. 386	325. 990	321. 112	315. 343	309. 501	304. 630	302. 001	303. 109
High	47	<b>73</b>	335. 238	338. 142	343. 144	348. 912	354. 366	358. 668	361. 232	361. 716	360. 026	356. 315	350. 983	344. 677	338. 291	332. 968	330. 094	331. 305
High	51	<b>74</b>	363. 769	366. 921	372. 348	378. 607	384. 524	389. 193	391. 975	392. 501	390. 667	386. 640	380. 854	374. 011	367. 082	361. 305	358. 187	359. 502
High	56	<b>75</b>	399. 432	402. 893	408. 852	415. 725	422. 223	427. 349	430. 404	430. 981	428. 967	424. 546	418. 192	410. 679	403. 071	396. 727	393. 303	394. 747
High	61	<b>76</b>	435. 096	438. 866	445. 357	452. 844	459. 921	465. 506	468. 833	469. 461	467. 268	462. 451	455. 531	447. 347	439. 059	432. 149	428. 419	429. 992
High	66	<b>77</b>	470. 759	474. 838	481. 861	489. 962	497. 620	503. 662	507. 262	507. 942	505. 569	500. 357	492. 870	484. 015	475. 048	467. 571	463. 536	465. 237
High	72	<b>78</b>	513. 556	518. 005	525. 667	534. 504	542. 858	549. 449	553. 377	554. 118	551. 529	545. 844	537. 676	528. 016	518. 234	510. 078	505. 675	507. 532
High	78	<b>79</b>	556. 352	561. 173	569. 473	579. 046	588. 096	595. 237	599. 492	600. 295	597. 490	591. 331	582. 482	572. 017	561. 420	552. 584	547. 815	549. 826
High	84	<b>80</b>	599. 148	604. 340	613. 613	623. 588	633. 334	641. 024	645. 606	646. 471	643. 451	636. 818	627. 289	616. 018	604. 606	595. 091	589. 955	592. 120
High	92	<b>81</b>	656. 210	661. 896	671. 686	682. 977	693. 652	702. 074	707. 093	708. 040	704. 732	697. 468	687. 030	674. 687	662. 188	651. 766	646. 141	648. 513
High	100	<b>82</b>	713. 272	719. 452	730. 093	742. 367	753. 969	763. 124	768. 579	769. 609	766. 013	758. 117	746. 772	733. 355	719. 769	708. 442	702. 327	704. 905
High	108	<b>83</b>	770. 334	777. 008	788. 501	801. 756	814. 287	824. 174	830. 065	831. 178	827. 294	818. 766	806. 514	792. 024	777. 351	765. 117	758. 513	761. 298
High	118	<b>84</b>	841. 661	848. 953	861. 510	875. 992	889. 684	900. 486	906. 923	908. 138	903. 895	894. 578	881. 191	865. 359	849. 328	835. 961	828. 746	831. 788
High	128	<b>85</b>	912. 988	920. 899	934. 519	950. 229	965. 081	976. 799	983. 781	985. 099	980. 497	970. 390	955. 868	938. 695	921. 304	906. 805	898. 979	902. 279
High	139	<b>86</b>	991. 448	1000 .04	1014 .83	1031 .89	1048 .02	1060 .74	1068 .32	1069 .76	1064 .76	1053 .78	1038 .01	1019 .36	1000 .48	984. 734	976. 235	979. 818
High	151	<b>87</b>	1077 .04	1086 .37	1102 .44	1120 .97	1138 .49	1152 .32	1160 .55	1162 .11	1156 .68	1144 .76	1127 .63	1107 .37	1086 .85	1069 .75	1060 .51	1064 .41
High	164	<b>88</b>	1169 .77	1179 .90	1197 .35	1217 .48	1236 .51	1251 .52	1260 .47	1262 .16	1256 .26	1243 .31	1224 .71	1202 .70	1180 .42	1161 .84	1151 .82	1156 .04
High	178	<b>89</b>	1269 .62	1280 .62	1299 .57	1321 .41	1342 .07	1358 .36	1368 .07	1369 .90	1363 .50	1349 .45	1329 .25	1305 .37	1281 .19	1261 .03	1250 .14	1254 .73
High	193	<b>90</b>	1376 .61	1388 .54	1409 .08	1432 .77	1455 .16	1472 .83	1483 .36	1485 .35	1478 .41	1463 .17	1441 .27	1415 .38	1389 .15	1367 .29	1355 .49	1360 .47
High	210	<b>91</b>	1497 .87	1510 .85	1533 .20	1558 .97	1583 .34	1602 .56	1614 .02	1616 .18	1608 .63	1592 .05	1568 .22	1540 .05	1511 .52	1487 .73	1474 .89	1480 .30
High	228	<b>92</b>	1626 .26	1640 .35	1664 .61	1692 .60	1719 .05	1739 .92	1752 .36	1754 .71	1746 .51	1728 .51	1702 .64	1672 .05	1641 .07	1615 .25	1601 .31	1607 .18
High	248	<b>93</b>	1768 .91	1784 .24	1810 .63	1841 .07	1869 .84	1892 .55	1906 .08	1908 .63	1899 .71	1880 .13	1851 .99	1818 .72	1785 .03	1756 .94	1741 .77	1748 .16
High	269	<b>94</b>	1918	1935	1963	1996	2028	2052	2067	2070	2060	2039	2008	1972	1936	1905	1889	1896

			.70	.33	.95	.97	.18	.80	.48	.25	.57	.33	.82	.73	.18	.71	.26	.19
High	292	<b>95</b>	2082 .75	2100 .80	2131 .87	2167 .71	2201 .59	2228 .32	2244 .25	2247 .26	2236 .76	2213 .70	2180 .57	2141 .40	2101 .73	2068 .65	2050 .80	2058 .32
High	317	<b>96</b>	2261 .07	2280 .66	2314 .40	2353 .30	2390 .08	2419 .10	2436 .40	2439 .66	2428 .26	2403 .23	2367 .27	2324 .74	2281 .67	2245 .76	2226 .38	2234 .55
High	345	<b>97</b>	2460 .79	2482 .11	2518 .82	2561 .16	2601 .19	2632 .78	2651 .60	2655 .15	2642 .74	2615 .50	2576 .36	2530 .08	2483 .20	2444 .12	2423 .03	2431 .92
High	374	<b>98</b>	2667 .64	2690 .75	2730 .55	2776 .45	2819 .84	2854 .08	2874 .49	2878 .34	2864 .89	2835 .36	2792 .93	2742 .75	2691 .94	2649 .57	2626 .70	2636 .35
High	407	<b>99</b>	2903 .02	2928 .17	2971 .48	3021 .43	3068 .65	3105 .91	3128 .12	3132 .31	3117 .67	3085 .54	3039 .36	2984 .76	2929 .46	2883 .36	2858 .47	2868 .96
High	442	<b>100</b>	3152 .66	3179 .98	3227 .01	3281 .26	3332 .54	3373 .01	3397 .12	3401 .67	3385 .78	3350 .88	3300 .73	3241 .43	3181 .38	3131 .31	3104 .29	3115 .68
High	480	<b>101</b>	3423 .71	3453 .37	3504 .45	3563 .36	3619 .05	3662 .99	3689 .18	3694 .12	3676 .86	3638 .96	3584 .51	3520 .11	3454 .89	3400 .52	3371 .17	3383 .54
High	521	<b>102</b>	3716 .15	3748 .35	3803 .79	3867 .73	3928 .18	3975 .88	4004 .30	4009 .66	3990 .93	3949 .79	3890 .68	3820 .78	3750 .00	3690 .98	3659 .12	3672 .56
High	566	<b>103</b>	4037 .12	4072 .10	4132 .33	4201 .79	4267 .47	4319 .28	4350 .16	4355 .99	4335 .63	4290 .94	4226 .73	4150 .79	4073 .89	4009 .78	3975 .17	3989 .76
High	614	<b>104</b>	4379 .49	4417 .44	4482 .77	4558 .13	4629 .37	4685 .58	4719 .08	4725 .40	4703 .32	4654 .84	4585 .18	4502 .80	4419 .38	4349 .83	4312 .29	4328 .12
High	667	<b>105</b>	4757 .52	4798 .75	4869 .72	4951 .58	5028 .98	5090 .04	5126 .42	5133 .29	5109 .31	5056 .64	4980 .97	4891 .48	4800 .86	4725 .31	4684 .52	4701 .72
High	724	<b>106</b>	5164 .09	5208 .83	5285 .87	5374 .73	5458 .74	5525 .02	5564 .51	5571 .97	5545 .93	5488 .77	5406 .63	5309 .49	5211 .13	5129 .12	5084 .85	5103 .51
High	787	<b>107</b>	5613 .45	5662 .09	5745 .83	5842 .42	5933 .74	6005 .79	6048 .72	6056 .82	6028 .52	5966 .38	5877 .10	5771 .51	5664 .58	5575 .44	5527 .31	5547 .60
High	854	<b>108</b>	6091 .34	6144 .12	6235 .00	6339 .81	6438 .90	6517 .08	6563 .67	6572 .46	6541 .75	6474 .32	6377 .43	6262 .85	6146 .83	6050 .09	5997 .87	6019 .89
High	928	<b>109</b>	6619 .16	6676 .52	6775 .26	6889 .16	6996 .83	7081 .79	7132 .41	7141 .97	7108 .60	7035 .33	6930 .04	6805 .54	6679 .46	6574 .34	6517 .60	6541 .52
High	1008	<b>110</b>	7189 .78	7252 .08	7359 .34	7483 .05	7600 .01	7692 .29	7747 .28	7757 .66	7721 .41	7641 .82	7527 .46	7392 .22	7255 .27	7141 .09	7079 .46	7105 .44
High	1094	<b>111</b>	7803 .19	7870 .81	7987 .22	8121 .49	8248 .42	8348 .58	8408 .25	8419 .52	8380 .18	8293 .80	8169 .69	8022 .91	7874 .27	7750 .35	7683 .46	7711 .66
High	1188	<b>112</b>	8473 .67	8547 .09	8673 .51	8819 .31	8957 .15	9065 .91	9130 .72	9142 .95	9100 .23	9006 .43	8871 .65	8712 .26	8550 .86	8416 .29	8343 .65	8374 .27
High	1291	<b>113</b>	9208 .34	9288 .13	9425 .50	9583 .95	9733 .74	9851 .93	9922 .36	9935 .65	9889 .23	9787 .29	9640 .83	9467 .62	9292 .22	9145 .98	9067 .04	9100 .33
High	1402	<b>114</b>	1000 0.1	1008 6.7	1023 5.9	1040 8.0	1057 0.6	1069 9.0	1077 5.5	1078 9.9	1073 9.5	1062 8.8	1046 9.7	1028 1.6	1009 1.2	9932 .35	9846 .63	9882 .77
High	1522	<b>115</b>	1085 6.0	1095 0.1	1111 2.0	1129 8.8	1147 5.4	1161 4.7	1169 7.8	1171 3.4	1165 8.7	1153 8.5	1136 5.9	1116 1.7	1095 4.9	1078 2.5	1068 9.4	1072 8.7
High	1653	<b>116</b>	1179 0.4	1189 2.5	1206 8.4	1227 1.3	1246 3.1	1261 4.4	1270 4.6	1272 1.6	1266 2.2	1253 1.7	1234 4.1	1212 2.4	1189 7.8	1171 0.5	1160 9.5	1165 2.1
High	1795	<b>117</b>	1280 3.2	1291 4.2	1310 5.2	1332 5.5	1353 3.7	1369 8.1	1379 6.0	1381 4.5	1374 9.9	1360 8.2	1340 4.6	1316 3.7	1291 9.9	1271 6.5	1260 6.8	1265 3.0
High	1949	<b>118</b>	1390 1.7	1402 2.1	1422 9.5	1446 8.7	1469 4.9	1487 3.3	1497 9.6	1499 9.7	1492 9.6	1477 5.7	1455 4.6	1429 3.1	1402 8.3	1380 7.5	1368 8.4	1373 8.6
High	2117	<b>119</b>	1510 0.0	1523 0.8	1545 6.1	1571 5.9	1596 1.5	1615 5.3	1627 0.8	1629 2.6	1621 6.5	1604 9.3	1580 9.2	1552 5.1	1523 7.5	1499 7.7	1486 8.3	1492 2.8
High	2299	<b>120</b>	1639 8.1	1654 0.2	1678 4.8	1706 7.0	1733 3.8	1754 4.2	1766 9.6	1769 3.3	1761 0.6	1742 9.1	1716 8.3	1685 9.8	1654 7.5	1628 7.1	1614 6.5	1620 5.8
High	2496	<b>121</b>	1780 3.3	1795 7.5	1822 3.1	1852 9.5	1881 9.1	1904 7.6	1918 3.7	1920 9.4	1911 9.7	1892 2.6	1863 9.4	1830 4.6	1796 5.4	1768 2.7	1753 0.1	1759 4.4
High	2711	<b>122</b>	1933 6.8	1950 4.3	1979 2.8	2012 5.6	2044 0.1	2068 8.3	2083 6.2	2086 4.1	2076 6.6	2055 2.6	2024 5.0	1988 1.3	1951 2.9	1920 5.9	1904 0.1	1911 0.0
High	2944	<b>123</b>	2099 8.7	2118 0.7	2149 3.9	2185 5.3	2219 6.9	2246 6.4	2262 7.0	2265 7.3	2255 1.4	2231 9.0	2198 5.0	2159 0.0	2119 0.0	2085 6.5	2067 6.5	2075 2.4
High	3197	<b>124</b>	2280 3.3	2300 0.9	2334 1.1	2373 3.5	2410 4.4	2439 7.1	2457 1.5	2460 4.4	2448 9.4	2423 7.0	2387 4.3	2344 5.4	2301 1.0	2264 8.9	2245 3.4	2253 5.8
High	3472	<b>125</b>	2476 4.8	2497 9.4	2534 8.8	2577 5.0	2617 7.8	2649 5.7	2668 5.1	2672 0.8	2659 6.0	2632 1.8	2592 7.9	2546 2.1	2499 0.4	2459 7.1	2438 4.8	2447 4.3
High	3770	<b>126</b>	2689 0.4	2712 3.3	2752 4.5	2798 7.2	2842 4.6	2876 9.8	2897 5.4	2901 4.3	2887 8.7	2858 1.0	2815 3.3	2764 7.5	2713 5.3	2670 8.2	2647 7.7	2657 4.9
High	4095	<b>127</b>	2920 8.5	2946 1.6	2989 7.3	3039 9.9	3087 5.0	3124 9.9	3147 3.3	3151 5.5	3136 8.2	3104 4.9	3058 0.3	3003 0.9	2947 4.5	2901 0.7	2876 0.3	2886 5.9

Table 5: The anode-dependent 1s energy table using the k-factors from Table 1. Energies in eV.

Power Supply	TM Index	Anode/Energy	0	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15
Low	151	1	8.45 498	8.52 824	8.65 438	8.79 986	8.93 740	9.04 592	9.11 058	9.12 279	9.08 016	8.98 657	8.85 209	8.69 305	8.53 200	8.39 773	8.32 524	8.35 580
Low	168	2	9.40 687	9.48 837	9.62 871	9.79 058	9.94 360	10.0 643	10.1 363	10.1 499	10.1 024	9.99 830	9.84 868	9.67 174	9.49 255	9.34 316	9.26 252	9.29 653
Low	188	3	10.5 267	10.6 179	10.7 750	10.9 561	11.1 274	11.2 625	11.3 430	11.3 582	11.3 051	11.1 886	11.0 211	10.8 231	10.6 226	10.4 554	10.3 652	10.4 033
Low	209	4	11.7 026	11.8 040	11.9 786	12.1 799	12.3 703	12.5 205	12.6 100	12.6 269	12.5 679	12.4 384	12.2 522	12.0 321	11.8 092	11.6 233	11.5 230	11.5 653
Low	234	5	13.1 024	13.2 159	13.4 114	13.6 369	13.8 500	14.0 182	14.1 184	14.1 373	14.0 712	13.9 262	13.7 178	13.4 713	13.2 218	13.0 137	12.9 014	12.9 487
Low	261	6	14.6 142	14.7 409	14.9 589	15.2 104	15.4 481	15.6 357	15.7 474	15.7 685	15.6 949	15.5 331	15.3 006	15.0 257	14.7 474	14.5 153	14.3 900	14.4 428
Low	291	7	16.2 940	16.4 352	16.6 783	16.9 587	17.2 237	17.4 329	17.5 575	17.5 810	17.4 989	17.3 185	17.0 593	16.7 528	16.4 425	16.1 837	16.0 440	16.1 029
Low	325	8	18.1 978	18.3 555	18.6 270	18.9 401	19.2 361	19.4 697	19.6 089	19.6 351	19.5 434	19.3 420	19.0 525	18.7 102	18.3 636	18.0 746	17.9 186	17.9 843
Low	363	9	20.3 256	20.5 017	20.8 049	21.1 546	21.4 853	21.7 461	21.9 016	21.9 309	21.8 285	21.6 035	21.2 802	20.8 979	20.5 107	20.1 879	20.0 137	20.0 871
Low	406	10	22.7 333	22.9 302	23.2 694	23.6 606	24.0 304	24.3 221	24.4 960	24.5 288	24.4 142	24.1 626	23.8 010	23.3 734	22.9 403	22.5 793	22.3 844	22.4 666
Low	453	11	25.3 649	25.5 847	25.9 631	26.3 996	26.8 122	27.1 378	27.3 317	27.3 684	27.2 405	26.9 597	26.5 563	26.0 791	25.5 960	25.1 932	24.9 757	25.0 674
Low	505	12	28.2 766	28.5 216	28.9 434	29.4 300	29.8 900	30.2 529	30.4 692	30.5 100	30.3 674	30.0 544	29.6 047	29.0 728	28.5 342	28.0 851	27.8 427	27.9 449
Low	564	13	31.5 802	31.8 538	32.3 250	32.8 684	33.3 821	33.7 874	34.0 289	34.0 745	33.9 153	33.5 657	33.0 634	32.4 694	31.8 679	31.3 663	31.0 956	31.2 098
Low	630	14	35.2 758	35.5 814	36.1 077	36.7 147	37.2 885	37.7 412	38.0 110	38.0 620	37.8 841	37.4 936	36.9 325	36.2 690	35.5 971	35.0 369	34.7 345	34.8 620
Low	703	15	39.3 633	39.7 043	40.2 916	40.9 689	41.6 092	42.1 144	42.4 155	42.4 723	42.2 739	41.8 381	41.2 120	40.4 716	39.7 218	39.0 967	38.7 593	38.9 015
Low	785	16	43.9 547	44.3 356	44.9 913	45.7 476	46.4 626	47.0 268	47.3 630	47.4 264	47.2 048	46.7 183	46.0 191	45.1 923	44.3 551	43.6 570	43.2 802	43.4 391
Low	877	17	49.1 061	49.5 316	50.2 642	51.1 091	51.9 080	52.5 382	52.9 138	52.9 847	52.7 371	52.1 935	51.4 125	50.4 888	49.5 534	48.7 735	48.3 526	48.5 301
Low	979	18	54.8 174	55.2 924	56.1 102	57.0 534	57.9 451	58.6 487	59.0 679	59.1 471	58.8 707	58.2 639	57.3 920	56.3 609	55.3 167	54.4 462	53.9 762	54.1 744
Low	1092	19	61.1 446	61.6 744	62.5 866	63.6 388	64.6 334	65.4 182	65.8 858	65.9 741	65.6 658	64.9 890	64.0 164	62.8 663	61.7 016	60.7 306	60.2 064	60.4 274
Low	1220	20	68.3 118	68.9 037	69.9 228	71.0 982	72.2 094	73.0 862	73.6 087	73.7 073	73.3 629	72.6 067	71.5 202	70.2 352	68.9 340	67.8 492	67.2 636	67.5 105
Low	1362	21	76.2 628	76.9 236	78.0 613	79.3 736	80.6 142	81.5 930	82.1 762	82.2 863	81.9 019	81.0 576	79.8 447	78.4 101	76.9 575	75.7 464	75.0 926	75.3 682
Low	1520	22	85.1 097	85.8 472	87.1 169	88.5 814	89.9 659	91.0 582	91.7 092	91.8 320	91.4 030	90.4 608	89.1 071	87.5 062	85.8 850	84.5 334	83.8 038	84.1 114
Low	1697	23	95.0 206	95.8 439	97.2 615	98.8 965	100. 442	101. 662	102. 388	102. 526	102. 047	100. 995	99.4 834	97.6 960	95.8 861	94.3 771	93.5 625	93.9 060
Low	1895	24	106. 107	107. 027	108. 610	110. 435	112. 161	113. 523	114. 335	114. 488	113. 953	112. 778	111. 091	109. 095	107. 074	105. 389	104. 479	104. 863
Low	2115	25	118. 426	119. 452	121. 219	123. 256	125. 183	126. 703	127. 608	127. 779	127. 182	125. 871	123. 988	121. 760	119. 504	117. 624	116. 609	117. 037
Low	2361	26	132. 200	133. 346	135. 318	137. 593	139. 743	141. 440	142. 451	142. 642	141. 975	140. 512	138. 409	135. 922	133. 404	131. 305	130. 172	130. 649
Low	2636	27	147. 598	148. 877	151. 079	153. 619	156. 020	157. 914	159. 043	159. 256	158. 512	156. 878	154. 530	151. 754	148. 943	146. 599	145. 333	145. 867
Low	2943	28	164. 788	166. 216	168. 674	171. 510	174. 191	176. 306	177. 566	177. 804	176. 973	175. 149	172. 528	169. 428	166. 289	163. 672	162. 260	162. 855
Low	3286	29	183. 994	185. 588	188. 333	191. 499	194. 492	196. 854	198. 261	198. 526	197. 599	195. 562	192. 635	189. 175	185. 670	182. 748	181. 171	181. 836
Low	3668	30	205. 383	207. 163	210. 227	213. 761	217. 102	219. 738	221. 309	221. 605	220. 570	218. 296	215. 030	211. 166	207. 254	203. 992	202. 232	202. 974
Low	4095	31	229. 292	231. 279	234. 700	238. 645	242. 375	245. 318	247. 072	247. 403	246. 247	243. 709	240. 062	235. 749	231. 381	227. 740	225. 774	226. 603

## 8. Geometric Factors

The geometric factor, [GF], in units of  $\text{cm}^2 \text{sr eV/eV}$ , is given by

$$(5) \quad [GF] = (e \Delta E \Delta \theta \Delta \phi) / (E * T_c) \sum_l \sum_m \sum_n N_{lmn} / I_{lmn}$$

where:  $\Delta E$  = Spacing between calibration points in energy,  
 $\Delta \theta$  = Elevation spacing,  
 $\Delta \phi$  = Azimuth spacing,  
 $E$  = Peak transmitted energy,  
 $T_c$  = Accumulation time,  
 $I$  = Beam current in ELS aperture per unit area,  
 $N$  = ELS counts.

The geometric factors measured in the laboratory by Dhiren Kataria are displayed in Table 6. Note that [GF] incorporates both the purely geometric response of the instrument as well as the detector response.

Table 6: Laboratory measured geometric factors ( $\text{cm}^2 \text{sr eV/eV}$ )

Energy(eV) Anode	29.9200	50.3000	70.2000	100.400	199.990	970.000	3021.00	5994.00	9990.00	11997.0
0	2.07540e-006	3.37581e-006	4.73706e-006	6.46449e-006	8.85756e-006	1.08817e-005	8.04262e-006	6.94579e-006	7.42996e-006	5.75665e-006
1	4.57159e-006	5.38168e-006	6.13679e-006	7.10438e-006	9.63588e-006	1.07470e-005	8.32344e-006	7.52185e-006	8.14427e-006	6.11427e-006
2	5.28905e-006	5.95252e-006	6.63087e-006	7.39277e-006	9.47093e-006	9.99465e-006	8.43561e-006	7.54510e-006	7.78974e-006	5.80410e-006
3	4.10182e-006	5.07612e-006	5.80111e-006	6.61061e-006	8.70769e-006	9.52572e-006	8.44829e-006	7.37566e-006	7.42463e-006	5.69616e-006
4	2.75657e-006	4.23158e-006	5.19947e-006	6.14290e-006	8.25067e-006	9.26740e-006	8.10313e-006	6.92202e-006	7.06366e-006	5.36508e-006
5	3.12045e-006	4.36811e-006	5.26247e-006	6.23110e-006	8.07105e-006	8.73019e-006	7.78427e-006	6.40499e-006	6.59983e-006	4.99699e-006
6	3.43856e-006	4.15704e-006	4.80389e-006	5.51189e-006	7.23690e-006	8.07841e-006	7.01710e-006	5.74396e-006	5.92093e-006	4.49043e-006
7	4.06785e-006	4.84366e-006	5.58990e-006	6.32900e-006	8.70944e-006	9.17226e-006	7.42745e-006	5.87616e-006	6.33978e-006	4.69977e-006
8	4.72466e-006	5.15194e-006	5.69955e-006	6.96500e-006	8.51592e-006	9.72213e-006	8.29093e-006	6.61914e-006	7.63213e-006	5.41397e-006
9	4.02959e-006	4.66755e-006	5.74074e-006	7.58045e-006	9.39149e-006	1.06782e-005	9.33263e-006	6.99206e-006	8.69915e-006	5.86279e-006
10	3.20888e-006	4.50439e-006	5.59275e-006	6.49422e-006	8.33294e-006	9.62592e-006	8.62126e-006	6.89954e-006	7.48176e-006	5.68084e-006
11	4.42217e-006	5.77331e-006	6.97938e-006	8.04752e-006	1.03845e-005	1.12857e-005	9.49013e-006	6.46349e-006	8.06194e-006	6.10723e-006
12	3.76111e-006	5.24365e-006	6.59177e-006	8.00591e-006	1.04415e-005	1.29351e-005	1.00476e-005	9.05845e-006	9.09767e-006	7.05230e-006
13	4.43609e-006	5.74996e-006	7.16811e-006	8.55046e-006	1.14662e-005	1.42535e-005	1.07045e-005	9.34059e-006	9.74682e-006	7.63039e-006
14	5.90117e-006	6.89419e-006	8.37360e-006	9.65106e-006	1.17197e-005	1.44310e-005	1.06524e-005	8.89006e-006	9.61936e-006	7.42696e-006
15	6.32660e-006	7.43104e-006	9.01837e-006	1.05006e-005	1.37654e-005	1.49384e-005	1.04071e-005	8.82440e-006	9.39500e-006	7.23438e-006

To find the geometric factor for each of the energies in Table 4, we need to extrapolate from the values in Table 6. The data measured between 199.99 and 5994.00eV in Table 4 are the

most reliable, therefore we only use those in the extrapolation. The best fit is found if we perform the interpolation in log-log space.

## 9. Calculating Raw Data from Telemetry

Due to the compression of the science values, the way in which the science data decodes is a bit complicated. First we need to figure out the science data structure and we need to decompress the data.

There are five quantities which are important when reconstructing the science data matrix. The first important quantity is the Rice Compression bit. When the Rice compression bit is set, the science data is Rice compressed. In order to be decoded, the science values within the ELS science data packet must be Rice decoded. This must happen before any decoding of the packet. Use the IRF Rice decode software to Rice decode the science data within the packet. If the Rice compression bit is not set, then the science data is not Rice compressed. Rice coding is a lossless data compression scheme to conserve the number of bits in the Venus Express mass memory.

The second important information is the sector mask. The sector mask tells you which ELS anodes are returning data within the packet. The data order is from anode 0 to anode 15 with each bit of the sensor mask representing the presence of anode data for that anode. The number of bits that are set in the sector mask tells you how many and which anodes have sweeps within the packet.

The third important information is the Log compression bit. This tells you whether the words within the packet are 8-bit or 16-bit. 16-bit words are not log compressed and the log compression bit is set to 0. 8-bit words are log compressed and the log compression bit is set. The 8-bit output value is split in a 4-bit exponent (e) and a 4-bit mantissa (m) according to the formula:

For  $e < 2$ , counts = m (for counts  $\leq 32$ , the output value is the same as the input value)

For  $e \geq 2$ , counts =  $(m + 16) * 2^{(e-1)}$

The compression of telemetry to 8-bits is a lossy process.

The fourth important information is the energy compression. This tells you how many energy steps are in the sweep. If the value of the energy compression is 0, there are 128 energy steps in the sweep. If the value of the energy compression is 1, there are 64 energy steps in the sweep and each science value represents the sum of two energy step values. If the value of the energy compression is 2, there are 32 energy steps in the sweep and each science value represents the sum of four energy step values. Energy compression occurs between successive energy steps obtained from the deflection values decoded from the ELS engineering data packet. Science values for each energy step are adjusted by dividing the science value by the number of energy steps included within a single science measurement.

The fifth important information is the time compression. This tells you how many sweeps are added together, forming each data value. This information is not relevant to decoding the science data, only in determining the actual value of the science data. The science values are adjusted by dividing the science value by the number of sweeps included in the sum representing a single science measurement. For example, if the time compression is a 3, representing 8 sweeps, divide all of the science values by 8. The Accumulation time for each

energy step is now 28125e-6 sec and there is a latency between accumulations of 3125e-6 sec.

The index indicating time compression was to be an indicator of the number of energy sweeps included within the sum. However, the Main Unit software does not include the science sweep within the sum if during that accumulation period of the sweeps, the Main Unit outputs an ELS engineering packet. However, it still reports the time compression as if it added the sweep. Thus, unless there is an ELS engineering packet output during the accumulation cycle, the time compression decodes as follows: TM value 0 = 1 spectra in sum, TM value 1 = 2 spectra in sum, TM value 2 = 4 spectra in sum, TM value 3 = 8 spectra in sum, TM value 4 = 16 spectra in sum. When the Main Unit outputs an engineering packet, it discards the science data for the same time period. Thus, the time compression decodes as follows: TM value 0 = 1 spectra in sum, TM value 1 = 1 spectra in sum, TM value 2 = 3 spectra in sum, TM value 3 = 7 spectra in sum, TM value 4 = 15 spectra in sum.

To convert the 16-bit science data value to absolute units, you divide each science value by the number of summed energy step values and divide by the number of sweeps included within the measurement. Expand out the science values to each of the energy steps represented in the ELS engineering data packet (for example, if a 64 step sweep, steps 0 and 1 get the same value, 2 and 3 are the same, etc.). This gives you the number of counts within an ELS accumulation for each of the 128 energy step values.

Now, throw out the last step and any steps which include the last step (for example, in a 64 step sweep, then steps 126 and 127 should be discarded). Since the last step is the flyback step, the science data is not valid and should not be included in the spectrum.

## 10. Data Calibration

The raw data from the telemetry is in units of counts/accumulation. The accumulation time for the Aspera-3 and 4 ELS is 3.6/128 s. So to convert to counts/second we divide the raw data by the accumulation time:

$$(6) \quad \text{Counts/sec} = \text{raw/accutime}$$

The differential energy flux (DEF), differential number flux (DNF) and the phase space density (PSD) are all dependent on the geometric factor (GF) and the energy level (en), and thus on the anode (an).

$$(7) \quad \text{DEF}(an,en) [\text{cm}^{-2} \text{sr}^{-1} \text{s}^{-1}] = \text{raw}/(\text{GF}(an,en) \times \text{accutime} \times A_A)$$

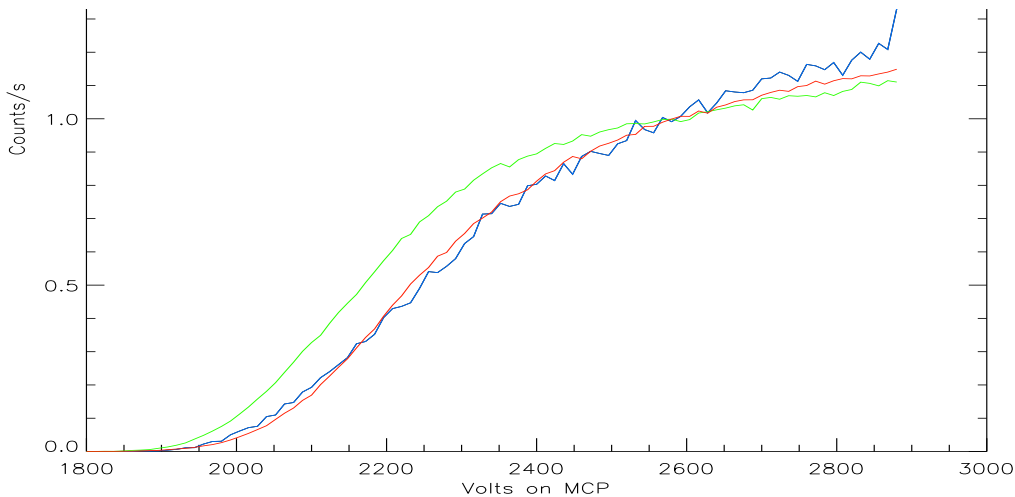
$$(8) \quad \text{DNF}(an,en) [\text{cm}^{-2} \text{sr}^{-1} \text{s}^{-1} \text{J}^{-1}] = \text{DEF}/(\text{earray}(an,en) \times E)$$

$$(9) \quad \text{PSD}(an,en) [\text{cm}^{-6} \text{s}^3] = (\text{raw} \times m_e^2)/(\text{GF}(an,en) \times \text{accutime} \times 2 \times (\text{earray}(an,en) \times E)^2 \times A_A)$$

In the above equations, earray is the array that contains all the data in Table 4 or 5, E is the conversion from eV to Joules =  $1.602 \times 10^{-19}$  J,  $m_e$  is the mass of an electron =  $9.11 \times 10^{-31}$  kg, and  $A_A$  is the active anode area ratio (the proportion of the anode area that actually measures counts) = 0.87.

## 11. MCP voltage response

This set of tests determined the operational regime of the microchannel plate detector. Tests were carried out with the beam incident on anode 10 and the MCP voltage was raised from 1800V to 2880V. The results for the different energies, normalised to the voltage at 2,580V are shown in Figure 8.



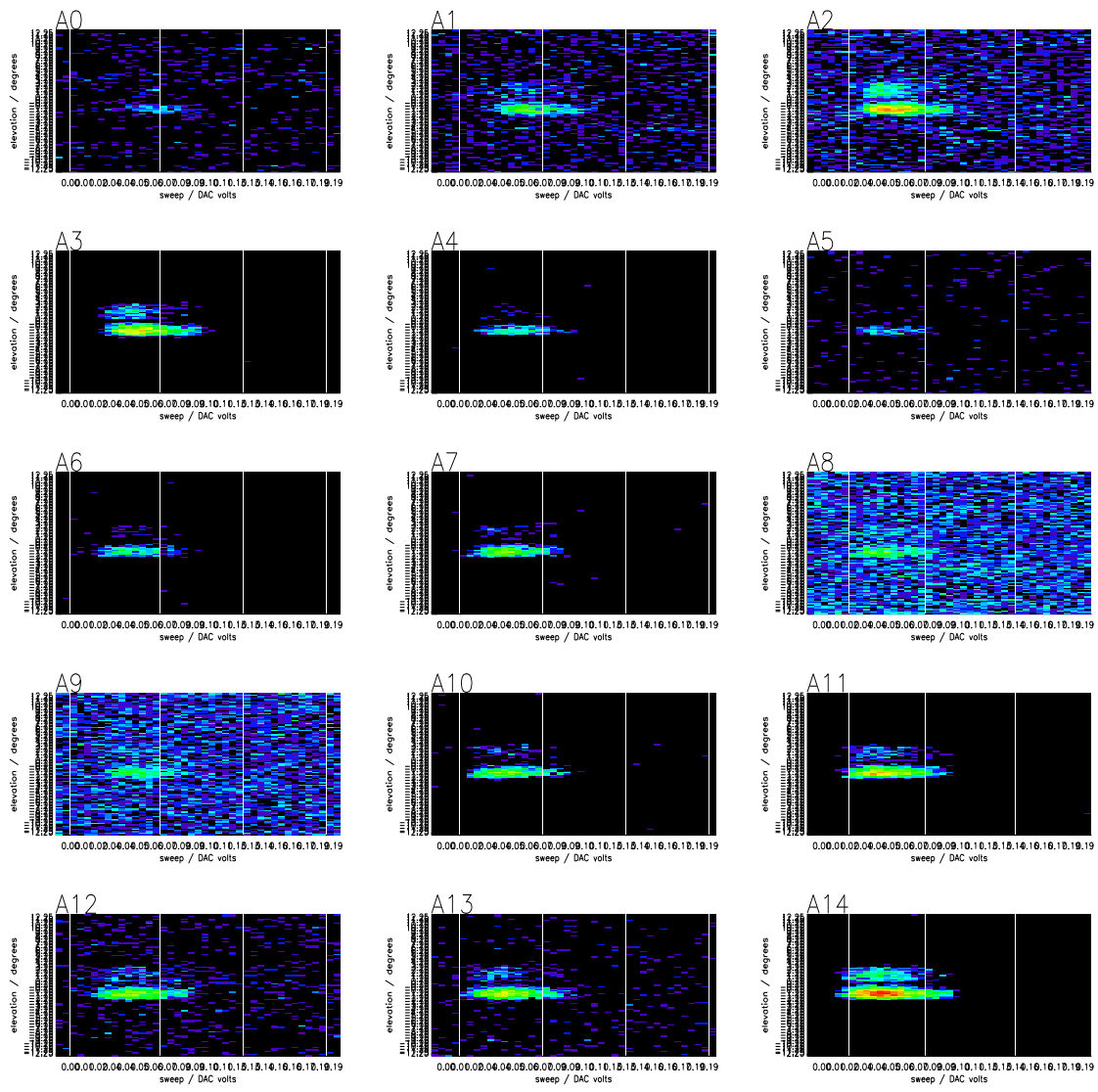
**Figure 8: MCP voltage versus normalised counts at 3 energies (30eV: blue, 300eV: green & 10keV: red)**

## 12. UV response

The response of the instrument to UV light has been studied by irradiation of a Krypton UV lamp on the entrance aperture (Alsop et al, 1998). Figure 9 shows the energy angle response of the 16 anodes to UV with the lamp facing Anode 1. As can be seen, most of the counts are observed at very low energies and are primarily due to low energy secondary electrons emitted by the incident light and eventually striking the MCP.

## 13. Anode selection

Anodes 5-12 have unobstructed views. Anodes 11 and 12 provide the best views and are the most commonly used in data analysis.



Counts per 0.1 sec

**Figure 9: Energy-angle scans for UV response measurement test**



## 14. References

C. Alsop et al, Measurement Techniques In Space Plasmas: Particles, AGU Geophysical Monograph 102, 1998, 269-274

Barabash, S., R. Lundin, H. Andersson, J. Gimholt, M. Holmström, O. Norberg, M. Yamauchi, K. Asamura, A. J. Coates, D. R. Linder, D. O. Kataria, C. C. Curtis, K. C. Hsieh, B. R. Sandel, A. Fedorov, A. Grigoriev, E. Budnik, M. Grande, M. Carter, D. H. Reading, H. Koskinen, E. Kallio, P. Riihela, T. Säles, J. Kozyra, N. Krupp, S. Livi, J. Woch, J. Luhmann, S. McKenna-Lawlor, S. Orsini, R. Cerulli-Irelli, M. Maggi, A. Morbidini, A. Mura, A. Milillo, E. Roelof, D. Williams, J.-A. Sauvaud, J.-J. Thocaven, T. Moreau, D. Winningham, R. Frahm, J. Scherrer, J. Sharber, P. Wurz, and P. Bochsler, ASPERA-3: Analyser of space plasmas and energetic atoms for Mars Express, In *Mars Express – The Scientific Payload*, ESA SP-1240, 121-139, 2004.

A.D. Johnstone, A.J. Coates et al, J.Phys.E:Sci Instrum. **20** (1987), 795-805

Marshall F. J., Hardy D. A. et al, Calibration system for electron detectors in the range from 10 eV to 50 keV, Rev. Sci. Instrum., 57(2), 229-235, 1986.