

Long, JA (Judy)

Subject: FW: SPIRE-COM : check of BSM load response



bsm-random-vib-input_
v2.xls

SPIRE-ATC-COM-000748

-----Original Message-----

From: Ian Pain
Sent: Tuesday, July 10, 2001 17:01
To: 'bw@mssl.ucl.ac.uk'
Subject: SPIRE-COM : check of BSM load response

Hi Berend,

I have re-worked the Miles approximations we discussed at Cardiff. Spreadsheet attached, but my specific questions are in the text below:

I have used :

$$\text{rms accel} = (\pi \cdot F_n \cdot W_x(F_n)) / 4L^{0.5}$$

where,

F_n = natural frequency

$W_x(F_n)$ = structure input accel from the PSD at the frequency

L = damping ratio = $1/\sqrt{\text{Frequency}}$

In Cardiff, we had used

$$\text{equiv accel} = 3 \cdot (\pi \cdot F_n \cdot W_x(F_n)) \cdot \text{ampl}/2^{0.5}$$

as $\text{ampl} = 1/2L$ these expressions are identical apart from the factor of 3.

I have used a multiplier to estimate the 50% probability peak response compared to the rms (about a factor of 4.6) and a further multiplier (1.27) to give 3-sigma peak response. These are based on formula in my 'bible' - Sarafin (Spacecraft Structures & Mechanisms, NASA/DoD). However, I suspect that your factor of 3 is the MSSSL pragmatic equivalent of my $4.6 \times 1.27 = 5.8$

I am a bit concerned that the assumed damping is too good if we use $1/\sqrt{\text{freq}}$. This yields values of ~ 0.047 . I would suspect values of 0.01 would be more realistic (and Sarafin would advise $1/4 \cdot \sqrt{\text{freq}}$). However they would double my load values so I do not want to take this on lightly and have stayed with the $1/\sqrt{\text{freq}}$ you recommended.

Further to this, I re-calculate the flex pivot safe loads. Assuming that they retain a margin of 1.5 IN ADDITION to the Qualification load factor you have inserted (1.5), then I have a problem with flex pivots - the margin on the chop stage pivot is 0.7. The Jiggle stage pivot is OK.

Q1. Can you confirm whether the 3 is a multiplier intended to indicate peak design loads.

Q2. If so, should I be using 3 or 5.8 to go from rms to peak loads?

Q3. Do you have any supporting data to allow me to use $1/\sqrt{\text{freq}}$ for damping, or would you advise another value based on experience?

Q4. Have I applied my safety margins correctly? Or, put another way should I remove the 1.5x on my components, to produce a margin on qualification 3 sigma load of the chop stage pivot of $0.7 \times 1.5 = 1.05 = :-)$

Best Regards,

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