

SPIRE Beam Steering Mirror Subsystem Specification Document

Version 3.6

Date: 24Apr03

Author: Ian Pain

DOCUMENT APPROVAL

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Record of Issue

| Date | Index | Remarks |
|-----------|-------|---|
| 13.Jun.00 | 1.0 | Issue for PDR |
| 06.Nov.00 | 2.0 | Update following additional technical data. Reformatting. |
| 31.May.01 | 3.0 | revising stability specification. ; Updated cross references ; Updated TBC's of mirror dimensions; Updated vibration environment; Added reliability and safety requirements; Expanded compliance matrix. Distributed internal to ATC for comment. |
| 19.Jun.01 | 3.1 | (working draft - internal to ATC). Confirmed 20msec risetime. Minor tweaks . updated vibration load and interfaces, updated outline description. |
| 10.Jul.01 | 3.2 | Amended reflectivity/ emmissivity spec (non measurable). Updated compliance & ICD tables. |
| 29.Jan.02 | 3.3 | Optical scaling factor and FoV change: chop now +/-2.53°. Added degraded modes |

| Date | Index | Remarks |
|--|----------------------------|--|
| <p>30.Nov.02 07.Apr.03</p> | <p>3.4</p> | <p>Close out of RID HR-SP-ATC-RID-05</p> <p>Added distribution list.</p> <p>Amended table of contents.</p> <p>Removed highlights except on TBC/D's.</p> <p>Updated AD table and moved mirrors specification to an AD</p> <p>§4.1.7 : updated inline with ECR: HR-SP-ATC-003.</p> <p>§4.1.8 : updated inline with ECR: HR-SP-ATC-003.</p> <p>§4.2.1 : corrected typographic error : 20mm should read 120mm.</p> <p>§4.2.6 noted ellipsoid specification, moved flatness to this area. Added tolerance to PCAL dia (rather than 'less than').</p> <p>§4.2.7 added area obscuration spec.</p> <p>§4.2.11 Changed Position of Rotation Axes per AD27 and achievable ATC targets</p> <p>§4.2.12 TBC changed to an ATC goal</p> <p>§4.3.2 removed TBC on OL5. 6</p> <p>§4.3.3 removed number of modes</p> <p>§4.3.7 removed TBC.</p> <p>§4.4.1 & 2 : updated telemetry in line with latest issue AD19</p> <p>§4.4.3 reworded micro-vibration export</p> <p>§4.4.4 added IID-A magnetic mask</p> <p>§4.4.5 referred to IID-A EMC requirements</p> <p>§4.5 added PCAL ICD doc number. Updated all document numbers.</p> |
| <p>23.Apr.03</p> | <p>3.5</p> | <p>§4.1.8 accuracy & resolution terminology clarified</p> <p>§4.1.9 settling angle on the sky added from IRD to improve traceability of requirement.</p> <p>§4.2.14 fail safe position wording changed. Added asymmetric FOV of spectrometer</p> <p>§4.2.11 added generic ATC tolerance goals on position of mirror centroid with respect to rotation axes (no formal requirements from SPIRE optical team).</p> |
| <p>24.Apr.03</p> | <p>3.6</p> | <p>Added Requirements numbering to aid traceability (format BSM-SSD-R-xx)</p> <p>§4.1.9 included both axes in settling time (ie covers cross talk too)</p> <p>§3.3 removed block diagram and replaced with RD8</p> |

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1. Scope

This specification defines the requirements applied to the performance, design and qualification of the Beam Steering Mechanism for the SPIRE photometer. It includes a brief description of the proposed design to meet these requirements. The complete design description is found in RD1.

The Beam Steering Mechanism forms a sub-system of the SPIRE instrument. This specification is applicable to the CQM, the PFM and the FS. Where relevant, it is also applicable to the STM (deliverable to SPIRE but not ESA).

2. Documents and Glossary

2.1 Applicable documents

| Ref | Title | Author | Reference | Date |
|------|--|--------------------------|--|---------------------------|
| AD1 | Instrument Requirements Document (IRD) | B.M.Swinyard | SPIRE-RAL-PRJ-000034 v1.1 | 10.Jan.02 |
| AD2 | SPIRE Structure Mechanical ICD | B.Winters | MSSL/SPIRE/SP004.11 (formerly SPIRE-MSS-PRJ-00617) | 29.Nov.01 |
| AD3 | ICD drawing: Structure: BSM | N/A | Drg No A2/5264/907 issue 6 | |
| AD4 | Optics - BSM ICD | T.Peacocke, I.Pain | SPIRE-ATC-PRJ-000713 v2.0 (SPIRE-ATC-PRJ-001171) | 07.Feb.02 |
| AD5 | Baffles - BSM ICD | T.Peacocke, I.Pain | SPIRE-ATC-PRJ-000713 v2.0 (SPIRE-ATC-PRJ-001171) | 07.Feb.02 |
| AD6 | Incorporated in AD2 | | | |
| AD7 | Incorporated in AD2 | | | |
| AD8 | Photometer Calibration Source - BSM ICD | I.Pain | SPIRE-ATC-PRJ-000713 v2.0 (SPIRE-ATC-PRJ-001171) | 07.Feb.02 |
| AD9 | Deleted | N/A | | |
| AD10 | On Board Software - BSM ICD | B.Stobie | SPIRE-ATC-PRJ-000713 v2.0 (SPIRE-ATC-PRJ-001171) | 07.Feb.02 |
| AD11 | deleted | | | |
| AD12 | Instrument Simulator - BSM ICD | B.Stobie | SPIRE-ATC-PRJ-000713 v1.0 | 07.Feb.02 |
| AD13 | Applicable Optical Configuration | T.Richards | PH154B , SP501E | Per AD26 |
| AD14 | Operating Modes for the SPIRE Instrument | B.M.Swinyard | SPIRE-RAL_PRJ 000320 issue 3.0 | 1.Oct.01 |
| AD15 | BSM Sub-system Development Plan | I.Pain | SPIRE-ATC-PRJ-000466 v5. 1 | 30.Jan.02 |
| AD19 | MCU-BSM ICD | I.Pain | SPIRE-ATC-PRJ-000713 v2.0 (SPIRE-ATC-PRJ-001171) MPU/DPU Command List ICD Iss3.0 15/01/03 | 07.Feb.02 |
| AD20 | SPIRE Product Assurance plan | D.Kelsh | SPIRE-RAL-PRJ-00017 v1.0 | 11.Apr.01 |

| Ref | Title | Author | Reference | Date |
|-----------------------|--|-----------------------------|--|---------------------------|
| AD21 | ATC Interface drawing | ATC | SPIRE-BSM -021-002-001 r.1 | 15.Jun.01 |
| AD22 | BSM Product Assurance Plan | Ian Pain | SPIRE-ATC-PRJ-000711 v1.2 | 15.Jul.02 |
| AD23 | Optical System Design Description | K.Dohlen, B.Swinyard | SPIRE-LAM-PRJ-000447 Draft 1 | 18.Dec.00 |
| AD 24 | SPIRE Cleanliness Plan | B.Swinyard | SPIRE-RAL-PRJ-1070 V1.0 | 09.Jan.02 |
| AD 25 | Identification of primary and secondary chop pixels in the SPIRE photometer arrays | B.Swinyard | SPIRE-RAL-NOT-001013 Issue: 1.0 | 15 Nov 01 |
| AD 26 | Angular Scaling Factors for the chop and jiggle movements of the BSM | T.Richards | SPIRE-RAL-NOT-001050 | 13.Dec.01 |
| AD 27 | Optical System Design Description | D.Pouliquen | SPIRE-LAM-PRJ-000457 (LAM.PJT.SPI.SPT.200007 Ind 7) | 12.Jul.01 |
| AD 28 | Email discussion of scratch/dig/obscuration | K.Dohlen | Re: BSM Sub-system Spec Doc. | 15.Nov.02 |
| AD 29 | Herschel/SPIRE revised random and static spec for SOB mounted sub-systems. | B.Winters | Email | 25Jan03 |

2.2 Reference documents

| Ref | Title | Author | Reference | Date |
|---------------------|---------------------------------------|---|---|---------------------------|
| RD1 | SPIRE BSM Design Description Document | Ian Pain | SPIRE-ATC-PRJ-000587 v4. 1 | 20.Feb.02 |
| RD2 | HERSCHEL Telescope Specification | | PT-RQ-04761 Issue 1/A SPIRE-ESA-DOC-000195 | Jan.98 |
| RD3 | SPIRE Systems Budgets | C.Cunningham | SPIRE-ATC-PRJ-000450 | latest |
| RD4 | Radiation environment memo: | J. Sørensen TOS-EMA , | réf. 00-010/JS, | 14 May 2001 |
| RD5 | Moved to AD27 | | | |
| RD6 | IID-A | HERSCHEL/Planck Project Team | SCI-PT-IIDA-04624 rev 3.0 | 24Jul02 |
| RD7 | IID-B | ESA HERSCHEL/ Planck Project Team | SCI-PT-IIDB/SPIRE-02124 rev 2/2 | 01Jul02 |
| RD8 | SPIRE Block Diagram | J.Delderfield | SPIRE-RAL-DWG-000646 (issue 5.3) | latest |

2.3 Glossary

| Abbrev | Meaning | Abbrev | Meaning |
|----------|---|---------|---|
| AD | Applicable Document | LAT | Lot Acceptance Tests |
| ADP | Acceptance Data Package | MAC | Multi Axis Controller |
| ATC | United Kingdom Astronomy Technology Centre | MAPTIS | Materials and Processes Technical Information Service |
| BSM | Beam Steering Mirror | MSFC | Marshall Space Flight Center |
| BSM | Beam Steering Mirror dummy | MCU | Mechanism Control Unit |
| BSMe | Beam Steering Mirror electronics | MIP | Mandatory Inspection Point |
| BSMm | Beam Steering Mirror mechanism | MGSE | Mechanical Ground Support Equipment |
| BSMs | Beam Steering Mirror structure | MPIA | Max Planck Institute for Astronomy |
| CAE | Computer Aided Engineering | MSSL | Mullard Space Science Laboratory |
| CDR | Critical Design Review | NASA | National Aeronautical Space Agency |
| CoG | Centre of Gravity | NA | Not Applicable |
| CIL | Critical Items List | NCR | Non Conformance Report |
| CQM | Cryogenic Qualification Model | NCRP | Non Conformance Review Panel |
| CTD | Change to Drawing/Document | OGSE | Optical Ground Support Equipment |
| DCL | Declared Components List | PA | Product Assurance |
| DDR | Detailed Design Review | PAD | Part Approval Document |
| DM | Development Model | PFM | Proto Flight Model |
| DML | Declared Materials List | PPARC | Particle Physics and Astronomy Research Council |
| DPA | Destructive Physical Analysis | PI | Principal Investigator |
| DSP | Digital Signal Processor | PID | Proportional – Integral - Derivative |
| ECSS | European Cooperation for Space Standardization | QA | Quality Assurance |
| EGSE | Electrical Ground Support Equipment | RAL | Rutherford Appleton Laboratory |
| ESA | European Space Agency | RAL SSD | RAL Space Science Department |
| FMEA | Failure Modes and Effects Analysis | RD | Reference Document |
| FMECA | Failure Modes, Effects and Criticality Analysis | rms | Root mean square |
| FPGA | Field Programmable Gate Array | SDOF | Single Degree of Freedom |
| FPU | Focal Plane Unit | SMEC | Spectrometer Mechanism |
| FS | Flight Spare | SPIRE | Spectral and Photometric Imaging REceiver |
| FSM | Flight Spare model | TBC | To Be Confirmed |
| GDFC | Goddard Flight Center | TBD | To Be Defined |
| GSE | Ground Support Equipment | TBW | To Be Written |
| HoS | Head of Specialism | UK ATC | United Kingdom Astronomy Technology Centre |
| Herschel | ESA Mission name (formerly FIRST) | UK SPO | UK SPIRE Project Office |
| ICD | Interface Control Document | WE | Warm Electronics |
| IBDR | Instrument Baseline Design Review | SOB | SPIRE Optical Bench |



HERSCHEL
SPIRE

**SPIRE Beam Steering Mirror Subsystem Specification
Document**

V 3.6

Ref: SPIRE-ATC-PRJ-000460

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Date : 24Apr03

Author: Ian Pain

| Abbrev | Meaning | Abbrev | Meaning |
|--------|---|--------|---------|
| KIP | Key Inspection Point | | |
| LAM | Laboratoire d'Astrophysique de Marseilles | | |

3. Subsystem description

3.1 Outline Description of the Beam Steering mirror mechanism subsystem

The Beam Steering Mirror mechanism subsystem (BSM) is a critical part of the SPIRE Instrument. It is used to steer the beam of the telescope on the photometer and spectrometer arrays in 2 orthogonal directions, for purposes of fully sampling the image, fine-pointing and signal modulation.

The BSM comprises 4 main deliverables:

1. **The cryogenic mechanism** (BSMm).
2. **The structural interface** (BSMs).
3. **The warm electronics** (BSMe)
4. **Mass and optical alignment dummies, and Ground Support Equipment (GSE) as required for SPIRE system level integration,** (BSMd)

The position of the BSMm & BSMs are indicated in Figure 1.

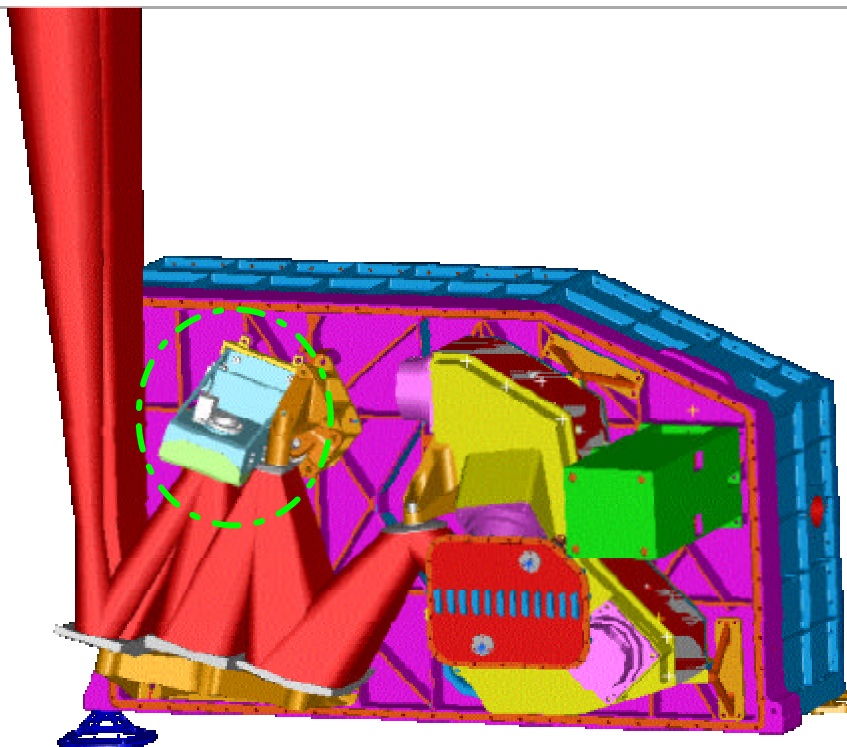


Figure 1 Photometer Layout, BSM, highlighted with green dashed oval

The BSMm consists of an aluminium alloy mirror, nominal diameter 32mm, machined as part of the chop axis. This is mounted orthogonally within a gimbal-type frame which provides for jiggle axis motion. The axes are suspended by flex-pivot mounts. The BSMm is a cryogenic device with nominal temperature 4-6K. Nominally, the chop axis provides 2.53 ° of mirror motion at 2 Hz and the jiggle axis provides 0.57° of motion at 1 Hz. The mirror also provides an aperture through which the Photometer Calibration Source is directed towards the detector arrays

The BSMs provides location of the BSMm on the SPIRE optical bench, and will also provide for a light tight enclosure and structural support for harnessing and thermometry. The BSMs integrates to the SPIRE Photometer

Calibration Source (PCAL), supplied by the University of Wales, Cardiff, a baffle (supplied by ATC) and the SPIRE optical bench (MSSL). The BSMs is a cryogenic structure with nominal temperature 4-6K.

The BSMe provides electrical actuators which are used to provide motion of the mirror. Electrical transducers are used to measure the mirror position to allow control of the mirror position. The BSMe baseline design makes use of cryogenic motors used in PACS and magneto-resistive sensors used in ISOPhot. Each axis houses a rare-earth (NdFeB [grade N42](#)) permanent magnet moving pole piece and is driven by a motor coil fixed to the mechanism housing/structure.

The cryogenic electronics are connected to the analogue power and amplifier electronics on the Warm Electronics (WE) by a cryogenic harness which will also feed out signal cables from thermocouples on the BSMs. The BSM operates under control of the Detector Readout and Control (HSDRC) sub-system's Mechanism Control Unit (MCU) supplied by LAM. The BSMe will be specified and designed by the UK ATC, then manufactured by LAM in conjunction with the SMEC electronics. Integration and test will be at LAM, with support from ATC.

The BSMd may comprise several actual dummies, with at least (1) an optical dummy for initial alignment work and (2) a mass-representative model for structural vibration tests. Designs for mass and optical alignment dummies will not be specified in detail until the BSMs/BSMm design is complete.

3.2 Mission profile

The BSM is developed as a sub-system and then integrated to the SPIRE FPU. The SPIRE instrument is subsequently integrated to Herschel. The instrument is to be cryogenically cooled, and will be cold during launch. Launch is scheduled for 2007 to an L2 orbit. The mission duration is a minimum of 4.25 years.

Per AD1, in normal operations the satellite is expected to have a 24-hour operational cycle with data being collected autonomously for 21 hours and a 3 hour ground contact period – the Data Transfer and Commanding Period (DTCP). During the DTCP the data will be telemetered to the ground and the commands for the next 24-hour period will be up-linked.

3.3 BSM Block Diagram

The SPIRE block diagram [showing the BSM](#) is [contained in a self contained document RD8 and](#) shows the relationships between the sub-systems of the SPIRE instrument.

3.4 Design Assumptions

3.4.1 Optical Scaling Factor

A scaling factor between the movement of the mirror and movement of the beam on the sky applies, as given in AD26.

Chop : 51.37 arc.sec/degree, or a scaling factor of 70.08:1

Jiggle : 52.36 arc.sec./degree, or a scaling factor of 68.75:1

3.4.2 Definition of Axes

The HERSCHEL spacecraft axes are defined in AD1, as follows:

- The X axis is the spacecraft boresight
- The Y axis is away from the HIFI instrument
- The Z axis is towards the sun shield.

The BSM is positioned in the SPIRE optical system such that the two rotation axes of the mirror produce nominal movements of the beam in the XY plane (around the Z axis) and in the XZ plane (around the Y axis) respectively.

The rotation axes of the BSM mirror shall be referred to as follows:

- Rotation producing a movement of the beam around the spacecraft Z axis - Chop axis
- Rotation producing a movement of the beam around the spacecraft Y axis - Jiggle axis

The mirror orientation is defined by two angles - the chop angle and the jiggle angle (θ_c, θ_j). The nominal zero position ($(\theta_c, \theta_j) = (0, 0)$) is defined as the orientation such that the centre of the photometer detector arrays are aligned along the nominal SPIRE boresight.

4. Functional Requirements

4.1 Performance requirements

These requirements are not dependent on the particular design of the BSM.

4.1.1 Angular Travel - Chop Axis

| | |
|---|---|
| <p><i>BSM-SSSD-R 1</i> The BSM shall allow angular movement of the mirror surface through an angle of ± 130 arc.sec on the sky. This is $\pm 2.53^\circ$ in the mirror chop axis. (see assumption 3.4 for corresponding on-sky motion).</p> | <p>AD1 : IRD-BSMP-R01 IID-B SRD-R9 IRD-PHOT-R17</p> |
| <p><i>BSM-SSSD-R 2</i> The minimum available chop throw shall be $\pm 0.1^\circ$ (see assumption 3.4 for corresponding on-sky motion).</p> | <p>AD1 : IRD-B SRD-R9</p> |
| <p><i>BSM-SSSD-R 3</i> The plate-scale varies from top to bottom and left to right of the image by a few percent, the maximum distance to the outer of these pixels is 129.5 arcsec if the arrays are well aligned. The maximum displacement of the arrays could be up to 2 arcsecs, therefore to use these pixels for point source chopping the BSM should have the capability chop to at least 132 arcsec.</p> | <p>AD25</p> |

4.1.2 Angular Travel - Jiggle Axis

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|--|---------------------------|
| <p><i>BSM-SSSD-R 4</i> The BSM shall allow angular movement of the mirror surface through an angle of ± 30 arc.sec on the sky. This is $\pm 0.573^\circ$ in the mirror jiggle axis. (see assumption 3.4 for corresponding on-sky motion).</p> | <p>AD1 : IRD-BSMP-R02</p> |
|--|---------------------------|

4.1.3 Minimum Step Size

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|--|---------------------------|
| <p><i>BSM-SSSD-R 5</i> The BSM shall allow movements of the mirror surface in both chop and jiggle axes in minimum increments of 2 arc.sec on the sky in either chop or jiggle. This is 0.038° jiggle, 0.039° chop. (see assumption 3.4 for corresponding on-sky motion).</p> | <p>AD1 : IRD-BSMP-R03</p> |
|--|---------------------------|

4.1.4 Chop Frequency

| | |
|--|---------------------------|
| <p><i>BSM-SSSD-R 6</i> The BSM shall allow movements of the mirror in the chop axis at any frequency, continuously variable or in 16 steps, up to 2Hz for nominal operation and power dissipation</p> | <p>AD1 : IRD-BSMP-R04</p> |
| <p><i>BSM-SSSD-R 7</i> As a goal, the BSM shall allow movements of the mirror in the chop axis at any frequency up to 5Hz. At frequencies above 2Hz, a degradation in power dissipation performance and settling time of the BSM is acceptable.</p> | <p>AD1 : IRD-BSMP-R04</p> |

4.1.5 Jiggle Frequency

| | |
|--|---------------------|
| <p>BSM-SSSD-R 8 The BSM shall allow movements of the mirror in the jiggle axis at any frequency up to 0.5Hz.</p> | AD1 : IRD-B SMP-R05 |
| <p>BSM-SSSD-R 9 As a goal, the BSM shall allow movements of the mirror in the jiggle axis at any frequency up to 1Hz. At frequencies above 0.5Hz, a degradation in power dissipation performance and settling time of the BSM is acceptable.</p> | AD1 : IRD-B SMP-R05 |

4.1.6 Holding position/ Drift Constraint

| | |
|---|--------------------|
| <p>BSM-SSSD-R 10 The BSM shall be capable of moving to, and holding at, any commanded position within its range of movement, to within 0.004 degrees rms, for periods of up to 4 hours</p> | AD1 : IRD-BSMP-R05 |
|---|--------------------|

4.1.7 Stability

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| <p>BSM-SSSD-R 11 <u>The angle on the sky must not vary by more than 0.2 arcsec (on the sky) per axis over 60 seconds at the commanded mirror position. The mirror position shall also have stability equivalent to 0.2 arcsec (rms) per axis in the 0.03 - 25Hz frequency band.</u></p> | AD1 : IRD-BSMP-R06 SPIRE-RAL-NOT-001457 ECR : HR-SP-ATC-003 |
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4.1.8 Position Measurement

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|---|---|
| <p>BSM-SSSD-R 12 The knowledge of the mirror position shall be <u>equal to or less than the equivalent of 0.025 arcsec on the sky in each axis</u>. <u>(Equivalent requirement on mirror position = 0.00049° chop axis and 0.00048° jiggle axis).</u></p> | AD1 : IRD-BSMP-R07 SPIRE-RAL-NOT-001457 ECR : HR-SP-ATC-003 |
| <p><u>In standard engineering terms, this requirement to define both 'accuracy' (0.004° on mirror) and 'resolution' (0.0005° on mirror)</u></p> | This document |

4.1.9 Settling Time

| | |
|---|--------------------|
| <p><i>BSM-SSSD-R 13</i> The angular position of the mirror surface shall be within <u>1 arc.sec on the sky (i.e. 0.019° on the mirror)</u> of the mean steady state position (<u>in both axes</u>) in less than 20 milliseconds from the application of a demand in the chop axis.</p> | AD1 : IRD-BSMP-R08 |
| <p><i>BSM-SSSD-R 14</i> The angular position of the mirror surface shall be within 0.019° of the mean steady state position (<u>in both axes</u>) in less than 0.100 sec from the application of a demand in the jiggle axis.</p> | This document |
| <p><i>BSM-SSSD-R 15</i> As a goal, the angular position of the mirror surface shall be within 0.019° of the mean steady state position (<u>in both axes</u>) in less than 0.050 sec from the application of a demand in the jiggle axis.</p> | This document |

4.1.10 Chop repeatability

| | |
|---|---------------|
| <p><i>BSM-SSSD-R 16</i> The steady state repeatability between successive chop cycles shall be less than 0.004° (rms) <u>on the mirror</u> over 4 hours.</p> | This document |
|---|---------------|

4.2 Technical Specifications

4.2.1 Mechanical Dimensions

| | |
|---|--------------------|
| <p><i>BSM-SSSD-R 17</i> The BSM shall fit within a volume of 130x130x30 mm (excluding mounting structure).</p> | AD1 : IRD-BSMP-R09 |
| <p><i>BSM-SSSD-R 18</i> The BSM, including mounting structure, shall fit within a volume of 132x95x<u>120</u>mm</p> | AD21 |
| <p><i>BSM-SSSD-R 19</i> The BSM mounting structure footprint is as defined in MSSL Interface drg. A2-5264-907 <u>and</u> ATC Interface drawing SPIRE-BSM-SPIRE-BSM-<u>024-002</u> (latest <u>revision</u>)</p> | AD2 AD21 |

4.2.2 Operating Temperature

| | |
|--|---|
| <p><i>BSM-SSSD-R 20</i> The operational temperature of the BSM shall be at Thermal Interface Level 1 per RD6: nominally 4K, but in the range 3.5-6.0K .</p> | AD1 : IRD-BSMP-R10 RD6 (Table 5.7.7.1-1) |
| <p><i>BSM-SSSD-R 21</i> The BSM shall be capable of operation (with reduced performance) at temperatures up to 300K.</p> | AD1 : IRD-BSMP-R10 |

4.2.3 Thermal Isolation

| | |
|---|--------------------|
| <p>BSM-SSSD-R 22 No part of the BSM visible to the optical path shall rise by no more than 1K from the nominal operating temperature of the surrounding structure after 1 hour of operation in any mode.</p> | AD1 : IRD-BSMP-R11 |
|---|--------------------|

4.2.4 Cold Power Dissipation

| | |
|---|--------------------|
| <p>BSM-SSSD-R 23 The average power dissipation of the BSM Cryogenic Mechanism (BSMm) and the BSM Support Structure (BSMs) shall be less than 4mW in any operating mode, when operating at the temperature defined in section 4.2.4</p> | AD1 : IRD-BSMP-R12 |
|---|--------------------|

4.2.5 Warm Electronics Power Dissipation

| | |
|---|--------------------|
| Removed : IRD issue 1.0, now in WE requirements | AD1 : IRD-BSMP-R13 |
|---|--------------------|

4.2.6 Mirror Surface Dimensions [& Form](#)

| | |
|--|---------------------------|
| <p>BSM-SSSD-R 24 The mirror clear diameter after allowing for any obscuration by the baffle shall be greater than 32mm. The clear diameter is the visible diameter (when viewed orthogonal to the mirror surface with the mirror held at the 0,0 position) .</p> | AD13 |
| <p>BSM-SSSD-R 25 The mirror shall include a central hole of no less than 2.8\pm0.1mm diameter to allow the Photometer Calibrator to be seen by the detectors.</p> <p>BSM-SSSD-R 26 <u>Goal – the design shall accommodate a central aperture up to 8mm without significant structural alteration being required.</u></p> | AD13 <u>(this)</u> |
| <p>BSM-SSSD-R 27 <u>The mirror shall encompass an ellipse 30x32mm</u></p> | <u>AD27</u> |
| <p>BSM-SSSD-R 28 <u>The mirror surface of the BSM shall be flat to <1μm rms (at the mirror, 2μm rms at the wavefront) at 4K .</u> <u>This should be validated by cold testing.</u></p> | <u>AD13, AD27</u> |

4.2.7 Mirror Surface Finish

| | |
|--|----------------------------|
| <p>BSM-SSSD-R 29 The mirror shall have a surface roughness of <10nm (rms) at 4K This may be established by room temperature testing.</p> | AD13, RD5 |
| <p>BSM-SSSD-R 30 The area obscuration due to combined scratch, dig and other defect shall be less than 0.1%.</p> | AD27, AD28 |

See also 4.6.3.1.

4.2.8 Mirror Surface Reflectivity

| | |
|---|-----------|
| <p>BSM-SSSD-R 31 The reflectivity of the mirror surface of the BSM shall be =99% in the wavelength range 200 - 670 μm by design. This requirement will not be measurable.</p> | AD13, RD5 |
|---|-----------|

See also 4.6.3.2.

4.2.9 Mirror Surface Emissivity

| | |
|---|-----------|
| <p>BSM-SSSD-R 32 The emissivity of the mirror surface of the BSM shall be <1% in the wavelength range 200 - 670 μm by design. This requirement is the complement of 4.2.8 and will not be measurable</p> | AD13, RD5 |
|---|-----------|

4.2.10 Baffle

| | |
|---|--------------------------------------|
| <p>The presence of a Baffle is assumed, and will be of the hole-in-plate type if internal component temperatures can meet the requirement of 0 .</p> <p>BSM-SSSD-R 33 The opening in the stray light baffle will be sufficient to allow the 20% oversized beam to cross it with a positive margin of no more than 0.5 mm.</p> | AD2 (section 2.5.9) This document |
|---|--------------------------------------|

4.2.11 Position of Rotation Axes

| | | |
|--|---------------------------------|---------------------|
| <p>BSM-SSSD-R 34</p> <p>The position of the Rotation Axes shall be established accurately <u>prior to delivery to RAL to better than 0.5 mm and 0.5°, allowing a positive allowance for machining of interface shoe on integration.</u></p> <p>BSM-SSSD-R 35</p> <p><u>After machining of the interface shoe on integration to SOB the BSM axes must be in the of nominal design position +/- 0.25mm and +/-0.05°.</u></p> | <p>This document</p> | |
| <p>BSM-SSSD-R 36</p> <p>The BSM shall be designed such that it may be repositioned on the SPIRE optical bench within a repeatability of <u>0.05 mm and 1 arc.minute 0.05° (TBC)</u></p> | <p>This document</p> | <p><u>AD 27</u></p> |
| <p>BSM-SSSD-R 37</p> <p><u>ATC Goal:</u> Rotational motions of the axes shall produce a <u>lateral</u> de-centre of the axis of rotation of less than 10 microns</p> | <p>This document</p> | |
| <p>BSM-SSSD-R 38</p> <p><u>ATC Goal: the mirror surface centroid shall be correctly assembled at the theoretical design point defined by intersection of the boresight with the axis of jiggle rotation to within 0.5mm spherical.</u></p> | <p><u>This document</u></p> | |
| <p>BSM-SSSD-R 39</p> <p><u>ATC Goal: the mirror surface centroid shall be correctly assembled at the theoretical design point defined by intersection of the boresight with the axis of chop rotation to within 0.3mm spherical.</u></p> | <p><u>This document</u></p> | |

4.2.12 Orthogonality of Rotation Axes

| | | |
|--|----------------------|--|
| <p>BSM-SSSD-R 40</p> <p><u>ATC Goal:</u> The orthogonality of the rotation axes shall be within <u>0.15° (TBC).</u></p> | <p>This document</p> | |
|--|----------------------|--|

4.2.13 Fail Safe (No Drive Signal) Position

| | | |
|--|----------------------|--|
| <p>BSM-SSSD-R 41</p> <p>When no drive signals are applied to the BSM, the mirror shall take up a position such that the mirror surface is perpendicular to the nominal (0,0) mirror position to within $\pm 0.18^\circ$. (For information, this is intended to place the BSM within 50% of the beam FWHM.)</p> | <p>This document</p> | |
|--|----------------------|--|

4.2.14 Fail Safe (Mechanical Failure) Position

| | | |
|--|---|--|
| <p>BSM-SSSD-R 42</p> <p><u>The BSM design shall mitigate against any single failure on launch making the beam unusable by the spectrometer instrument, i.e. That in the event of a failure of flex pivots the mirror surface is either retained, or can be returned, perpendicular to the nominal (0,0) mirror position to within $+0.573$ to -2.53° in the chop axis.</u></p> | <p>This document</p> <p><u>ECR HR-SP-ATC-002</u></p> | |
|--|---|--|

4.2.15 Mass

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|--|--|
| <p><i>BSM-SSSD-R 43</i> The BSM cryogenic mechanism (BSMm) and the BSM support (BSMs) shall have a combined mass of less than 1100g; including harness but excluding contingency and PCAL</p> | <p>IRD-SUBS-R03 (SPIRE Sub-system Budget Allocations)</p> |
|--|--|

4.2.16 Cool-down time

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|--|-----------------------|
| <p><i>BSM-SSSD-R 44</i> Upon integration to the SPIRE optical bench, the BSM shall reach a temperature of 4K within 15 hours of the commencement of cooldown. This assumes a maximum average cooldown rate of 20K/hour.</p> | <p>Source unknown</p> |
|--|-----------------------|

4.2.17 Reliability

| | |
|--|--------------------------|
| <p><i>BSM-SSSD-R 45</i> As far as possible the total failure of a single sub-system shall not lead to the total loss of instrument operations.</p> | <p>AD1 : IRD-REL-R01</p> |
| <p><i>BSM-SSSD-R 46</i> Backup modes of operation should be available for all nominal observing modes. These shall be designed to allow the continued use of that mode, albeit with degraded performance or efficiency.</p> | <p>AD1 : IRD-REL-R02</p> |
| <p><i>BSM-SSSD-R 47</i> Cold redundant hardware shall be provided wherever practicable within the instrument design.</p> | <p>AD1 : IRD-REL-R03</p> |

4.2.18 Failure Modes

| | |
|---|---------------------------|
| <p><i>BSM-SSSD-R 48</i> Failure of any sub-system, or one of its components, shall not affect the health of any other subsystem, the instrument or the interface with the satellite.</p> | <p>AD1 : IRD-SAFE-R08</p> |
| <p><i>BSM-SSSD-R 49</i> Failure of any component in a subsystem shall not damage any redundant or backup component designed to replace that component in the subsystem</p> | <p>AD1 : IRD-SAFE-R09</p> |
| <p><i>BSM-SSSD-R 50</i> No electronics sub-unit shall be capable of affecting instrument operations until it is in a defined state. This state shall be confirmed in the housekeeping telemetry.</p> | <p>AD1 : IRD-SAFE-R10</p> |

4.3 Operational Specification

4.3.1 Operational Safety

| | |
|---|---------------|
| <i>BSM-SSSD-R 51</i> The BSM shall operate safely in any normal operating mode. | This document |
|---|---------------|

4.3.2 Lifetime

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|--|--------------------|
| <i>BSM-SSSD-R 52</i> The BSM shall be capable of operation in any normal mode for periods in excess of 1/6 of the nominal mission lifetime. | AD1 |
| <i>BSM-SSSD-R 53</i> All sub-systems are required to demonstrate that they will operate successfully over the 4.25 years of expected mission operations. | AD1 : IRD-SUBS-R02 |
| <i>BSM-SSSD-R 54</i> Lifetime tests of items operating <100000 times will use factors as specified in RD 16; i.e. Lifetime tests of the chop/jiggle mode will use a multiplier of 1.25x for on-orbit cycles and 4x for ground test cycles. | RD16 |

| Life time breakdown | | | | |
|---------------------|--|-----|--------------------------------------|---|
| # | Parameter | IRD | Value | Note |
| OL1 | Ground Storage lifetime | | 2 years | A guess |
| OL2 | Ground Integrated lifetime | | 4 years | A guess |
| OL3 | Ground operational lifetime | | 1.5 years nominal | 6 months for subsystem acceptance 6 months for SPIRE acceptance 6 months for HERSCHEL acceptance Broken down, nominally: 1M cycles during BSM check out at ATC 1M cycles during BSM check out at RAL 1M cycles during system integration, e.g. checking for cross talk, vibration, EMC. 1M cycles during observing mode checkout. 1M cycles for ESA/Herschel integration. 0.3M cycles spare. |
| OL4 | On orbit operational (chop & jiggle mode) Lifetime | | Minimum 8.5 months cumulative time | Operating during 1/6 of the mission duration (4.25 years) |
| OL5 | On orbit de-powered operational | | Up to 3.5 years cumulative | Based on 5/6 of the mission duration |

| Life time breakdown | | | | |
|---------------------|--|-----|---------------------------------|---|
| # | Parameter | IRD | Value | Note |
| | Lifetime | | time | |
| OL6 | On Orbit powered but not chopping (servo control only) | | Up to 3.5 years cumulative time | This is the baseline design assumption and is required in the event that self-damping is inadequate in the spacecraft micro-vibration environment |

4.3.3 Operating modes

AD14 defines the required modes of operation in detail. There are [a number of](#) operational modes, but from the point of view of the BSM motion they fall into three categories :

| | |
|--|------|
| <i>BSM-SSSD-R 55</i> Jiggle | AD14 |
| <i>BSM-SSSD-R 56</i> Chopping | AD14 |
| <i>BSM-SSSD-R 57</i> Scan mapping | AD14 |
| <i>BSM-SSSD-R 58</i> Additionally holding the 'stare' position may require active servo control. | |

4.3.4 Jiggle Mode

Jiggle Mode is used to optimize the sampling of the detector arrays. In this mode, the mirror is stepped in small angular increments. Jiggling may be done in any angular orientation (i.e. jiggling is not confined to the jiggle axis, and will usually be a combination of movements in the chop and jiggle axes).

Jiggle movements may be demanded in both chop and jiggle axes simultaneously. The fine pointing mode is executed as a jiggle pattern, and the difference lies in the processing/use of the data.

Jiggle mode will be used with both the photometer and the FTS. When the FTS is in use no chop will be required. During a photometer jiggle operation the BSM is also required to chop. i.e. at each jiggle position a number of chop cycles will be executed.

4.3.5 Chopping Mode

Chopping Mode is used to provide removal of 1/f noise in the photometer detectors. The mirror is used to move the source of interest between two separate detectors.

Chopping is only required in one axis (the chop axis), and will only be used when the photometer is in use, not with the FTS

4.3.6 Scan mapping

Scan mapping with chopping may be required. The jiggle and chop axes are used to execute chopping either parallel to or perpendicular to the scan direction, with the frequency of chop set by the jiggle axis frequency limit.

4.3.7 Stare or 'holding' mode

Dependent on spacecraft vibration levels, the BSM may require active servo control in order to maintain the nominal 'power-off' hold position within adequate accuracy. This is [TBD the baseline](#).

4.3.8 Degraded modes

4.3.8.1 Slow Chop Mode

AD 14, section 6.2 : If the BSM suffers a failure that prevents it from chopping at the default frequency due to sticking or excessive dissipation, it may be that it may have to be chopped very much more slowly. This implies that :

| | |
|---|----------------------|
| <p><i>BSM-SSSD-R 59</i> the control circuitry and algorithms must be capable of driving the BSM at any frequency from DC up to the maximum allowable by the design. A range of chop frequencies must be identified and the instrument response at these frequencies characterised before launch.</p> | <p>This document</p> |
|---|----------------------|

4.3.8.2 BSM Open Loop

AD 14, section 6.3: In the event of a failure of the position sensor on the BSM chop axis, it must still be possible to operate the BSM by commanding the current to the actuators directly. This mode of operation may lead to a loss of efficiency as the chopping mirror will not be under control and may take some time to become stable after movement.

| | |
|--|----------------------|
| <p><i>BSM-SSSD-R 60</i> The behaviour of the BSM under open loop control must be characterized and suitable current demand algorithms devised to allow at least the chopped mode to be carried out in the event of loss of the chop axis position sensor.</p> | <p>This document</p> |
|--|----------------------|

4.3.8.3 Single Axis BSM Operation

AD 14, section 6.4 : It may be that one axis of the BSM stops working during the mission. In this case it must be possible to use the other axis on its own to chop or, if the chop axis is lost, at least to pixel-swap on one of the detector arrays. It may be that there is some mechanical cross_talk between the axes and demand will be required on both axes during nominal operation to achieve accurate positioning. If this is the case:

| | |
|---|----------------------|
| <p><i>BSM-SSSD-R 61</i></p> <p>the operation of each axis in the absence of the other must be possible and this mode of operation fully characterized before launch.</p> | <p>This document</p> |
|---|----------------------|

4.3.9 Combinations of Modes

BSM-SSSD-R 62

The following combinations of the basic modes are required.

1. Chopping and Jiggling
2. Removal of optical or mechanical cross coupling during Chop-only or Jiggle-only operations.

4.4 Interface requirements

4.4.1 Data Outputs

The following data is provided by the BSMe via the MCU.

| Data | Rate | Reference |
|---|---|--------------------|
| <p><i>BSM-SSSD-R 63</i> Chop axis position</p> | <p><u>@ 4.16 or 64 Hz depending on Instrument Scientific Mode</u></p> | <p><u>AD19</u></p> |
| <p><i>BSM-SSSD-R 64</i> Jiggle axis position</p> | <p><u>@ 4.16 or 64 Hz depending on Instrument Scientific Mode</u></p> | <p><u>AD19</u></p> |
| <p><i>BSM-SSSD-R 65</i> <u>Engineering/Trace data (e.g. Motor volts/current)</u></p> | <p><u>@ 2.778 kHz</u> <u><100Hz (TBC)</u></p> | <p><u>AD19</u></p> |

Thermometry data is passed directly to the thermometry sub system, for which no specification is placed on the BSM or MCU.

4.4.2 Data Inputs

The following inputs are required to operate the BSM.

| Data | Rate | Reference |
|---|--------------------------|-----------------|
| Chop axis demand position | On Demand, max. 5Hz | AD19 |
| Jiggle axis demand position | On Demand, max. 1Hz | AD19 |
| Control system parameters (PID terms) | occasional | AD19 |
| Trajectory parameters (3 for each axis) | deleted | AD19 |
| Unlatch signal, if required | One time only | AD19 |
| <u>Sensor Power on/off</u> | <u>On/off</u> | <u>AD19</u> |

4.4.3 Exported vibration

| | |
|--|-------------------------------|
| <u>The BSM will produce vibration in the form of a couple and out-of-balance force, with a rise time of less than 5ms repeating every 250ms for 2Hz chopping-chopping. Harmonics and their amplitude will depend on SOB stiffness as well as the BSM structure.</u> | This document |
| <i>BSM-SSSD-R 66</i> <u>At the BSM mounting position, the torque reaction about the chop axis to be less than 25 x10⁻⁶ Nm (averaged over the chop rise time).</u> | This document |
| <i>BSM-SSSD-R 67</i> <u>At the BSM mounting position, the torque reaction about the chop axis to be less than 20 x10⁻⁶ Nm (averaged over the jiggle rise time).</u> | This document |

4.4.4 Stray Magnetic fields (H field radiated susceptibility)

| | |
|--|-------------------------------------|
| <i>BSM-SSSD-R 68</i> <u>The BSM shall not be susceptible to spurious signal generation due to a-magnetic field strength ≥ 0.01 mT <u>in the freq range 30Hz-50kHz.</u> <u>(Note this is calculated from IID-A radiated susceptibility mask at 140 dBpT)</u></u> | IID-A sec.5.14.3.12 |
|--|-------------------------------------|

4.4.5 Electro-Magnetic Compatibility

| | |
|--|--|
| <p><i>BSM-SSSD-R 69</i></p> <p>The BSM shall comply with the general requirements of the IID-A on EMC. Notably:</p> <ul style="list-style-type: none"> • <u>The cryogenic subsystem is to be grounded at the warm electronics</u> • <u>The signal and power wires of the BSM shall be electrically isolated from the Chassis of the FPU with more than TBD MO</u> • <u>H Field Radiated Emission: Narrow-band electric fields generated by the subsystem equipment and measured at 1 m distance shall not exceed 60dBpT in the frequency range 30Hz to 50KHz.</u> • <u>Narrow-band electric fields generated by the subsystem equipment and measured at 1 m distance shall not exceed 50 dBµV/min the frequency range 14kHz -0.5MHz, rising to 74 dBµV/mat 0.5-18GHz:</u> | <p>IID-A sec.5.14.</p> |
|--|--|

4.4.6 ICD's

The BSM interfaces with the following other subsystems in the SPIRE instrument. The interface to each subsystem is specified in the relevant Interface Control Document.

4.5 BSM interface reference table

The master reference table is located in RD1.

| ID | Sub-System | Organization responsible ¹ | External ICD document | Internal ATC ICD document | Internal ATC ICD drawing/ file |
|-----|-------------------------------------|---------------------------------------|---|---|--|
| 1 | BSM-SPIRE | RAL | Instrument Requirements Document (IRD). SPIRE-RAL-PRJ-000034 v0.30 May.00 | SPIRE-ATC-PRJ- 001171 | SPIRE-BSM- 024-002 Rev2 |
| 2.1 | Structure – BSM | MMSL | MSSL/SPIRE/SP004.11 (formerly SPIRE-MSS-PRJ-00617) Drg No A2/5264/907 issue 6 | SPIRE-ATC-PRJ- 001171 Latest 3D model. | SPIRE-BSM- 024-002 Rev2 |
| 2.2 | Structure – BSM | MMSL | | | SPIRE-BSM- 023-001_ASM.IGS / .STP -(IGES/ STEP file) (needs update to 024 series?) |
| 2.3 | Thermometry | RAL | N/A (lakeshore data sheets) | | Wiring: SPIRE-BSM-??? |
| 3 | Photometer Calibration Source - BSM | UoW, Cardiff | SPIRE Ref.: SPIRE-UCF-PRJ-001150 Cardiff Ref.: HSO-CDF-ICD-013 Issue: 2.0 dated 06.Feb.02 | SPIRE-ATC-PRJ- 001171 | SPIRE-BSM- 020-001-004 Rev1 (needs update to 024 series?) |
| 4 | Launch Latch – BSM | LAM (TBC) | Spectrometer mirror mechanism design description LAM.SPI.PJT.NOT.200008 Ind 3 | SPIRE-ATC-PRJ- 001171 | SPIRE-BSM-020-001-007 rev 2 |
| 5.1 | Optics – external finish | LAM | AD27. AD28 | SPIRE-ATC-PRJ- 001171 | SPIRE BSM 023-004-001 Rev2 |
| 5.2 | Optics – BSM | RAL | AD26. AD13 | | No up to date model exists |
| 5.3 | Baffles – BSM | RAL | AD13 | | No up to date model exists |
| 6 | Cryo-Harness | RAL / MSSL | SPIRE Harness Definition. SPIRE-RAL-PRJ-000608 | SPIRE-ATC-PRJ- 001171 | FPU Subsystem Harness Procurement Spec SPIRE-RAL-DOC-001362 |
| 7.1 | MCU-BSM | LAM | TBW | SPIRE-ATC-PRJ- | Various D-space files under |

¹ i.e. responsible for feeding ICD info upwards to SPIRE system design

| ID | Sub-System | Organization responsible ¹ | External ICD document | Internal ATC ICD document | Internal ATC ICD drawing/ file |
|-----|---|---------------------------------------|---|--------------------------------------|--------------------------------|
| 7.2 | On Board Software - BSM | LAM | TBW | 001171 | config control |
| 8 | Photometer Bolometer Arrays - BSM (micro-vibration) | MSSL | No Document - sign off of this document suffices. | SPIRE-ATC-PRJ-001171 | N/A |
| 9 | Spectrometer Bolometer Arrays - BSM (micro-vibration) | MSSL | No Document - sign off of this document suffices. | SPIRE-ATC-PRJ-001171 | N/A |
| 10 | FPU Simulator - BSM | RAL | TBD | SPIRE-ATC-PRJ-001171 | TBD |
| 11 | Instrument Simulator - BSM | RAL | TBD | SPIRE-ATC-PRJ-001171 | TBD |

4.6 Design, manufacture and test requirements

This section details additional requirements which are placed on the sub-system which are not necessary to meet the functional or operational requirements, but are necessary to enable the sub-system to be designed, manufactured or tested. These are encapsulated as Product Assurance requirements and are fully covered in the BSM Product Assurance Plan, AD22

4.6.1 Design requirements

UK Astronomy Technology Centre design procedures shall be adopted as applicable.

4.6.2 Electronics Card Format

BSM-SSSD-R 70

All electronics associated with the BSM shall be mounted on double eurocards [AD19].

4.6.3 Product Assurance Plan

The BSM deliverables will comply with the Spire Product Assurance Plan, AD20, and the BSM Product Assurance Plan AD22 . Specific requirements are noted below, otherwise AD22 will be adopted.

4.6.3.1 Mirror Flatness

BSM-SSSD-R 71

[Per AD27](#) : to facilitate optical laboratory testing, the mirror surface shall have a [surface shape error <1.0 micron rms](#). [ATC shall also apply acceptance criteria of roughness](#) of <10nm [rms and](#) P-V [< 100nm](#)

4.6.3.2 Mirror Reflectivity

BSM-SSSD-R 72

To facilitate optical testing laboratory testing, the mirror surface shall have a reflectivity of >80% at 633nm by design.

4.6.3.3 Cleanliness

BSM-SSSD-R 73

The BSM shall be assembled to class 1000 cleanliness, but shall be class 100 compatible by design. Contamination on delivery for integration to SPIRE shall be on delivery: [AD24].

- Particulate <440ppm (general) and <125ppm (mirror)
- Molecular contamination <1x10⁻⁴ g/cm²

4.6.3.4 Material selection

BSM-SSSD-R 74

Structures will be a 6082 grade aluminium alloy to UK standards, and will be selected in consultation with the optical bench design body (MSSL). The BSM mirror may be specified in grade 6061-T6/T651 to ensure adequate thermal stability based on ATC practice.

BSM-SSSD-R 75

Fasteners will be cryogenic grade stainless steel. Where practicable they will be of a self locking type. Fasteners may include UNS thread types where required on the grounds of availability in small sizes, or as required by ICD, otherwise will be metric thread. In cases where a self locking fastener is not available, [Eccobond 286](#), Stycast or Scotchweld 1838 will be used in visible applications under fastener heads.

4.6.3.5 Storage

BSM-SSSD-R 76

The BSM shall not suffer any performance degradation following storage in a dry nitrogen atmosphere for a period of up to 5 years. Storage temperatures shall be in the range +5°C to +30°C.

4.7 Environmental requirements

These requirements describe the environment the subsystem will encounter during its life.

4.7.1 Operating environment

This section defines the environment for the BSM during operation. The BSM must meet all of the functional and operational requirements specified in section 4 when operating under this environment.

| | |
|--|--------------|
| All subsystems are required to undergo an environmental test programme that demonstrates the design and build standard of the sub-system models will be compatible with the environmental test programme to be carried out on the appropriate integrated instrument model. | IRD-SUBS-R01 |
|--|--------------|

4.7.1.1 Shock

| | |
|-----------------------------------|-----|
| No Shock specification is applied | AD2 |
|-----------------------------------|-----|

4.7.1.2 Quasi Static Loads

| | | | | |
|--|--------|--------|--------|-------------------|
| For the BSM sub-system these are derived from the random vibration specification (see 4.7.1.4) using the Miles SDOF approximation to estimate rms and peak acceleration. | | | | AD2 |
| BSM-SSSD-R 77 | | | | AD22, table 1.4-1 |
| For the SPIRE instrument as a whole the following Quasi-Static flight limit load are given. Per AD22 “ <i>All subsystems will be subjected to the same environment as defined above. The in table 1.4-1 defined accelerations are very important for limiting interface loads for the various sub-systems subjected to either sine, random or shock loads</i> ”. | | | | |
| Quasi Static levels | Case 1 | Case 2 | Case 3 | |
| x-direction | 25 g | - | - | |
| y-direction | - | 14 g | - | |
| z-direction | - | - | 14 g | |

Per AD29 Static is now reduced from 40 g to 25 g in any direction

4.7.1.3 Sine Vibration

| | | | |
|---|-----------------|----------------------|---------------|
| BSM-SSSD-R 78 | | | AD22 |
| The provisional Qualification sine input (2 oct/min) specification is (As specified in AD2, AD22 these include the qualification factor of 1.5) : | | | Table 2.9.6-1 |
| Sine vibration levels | Frequency range | Input at base (QUAL) | |
| X-direction | 5-30 Hz | 11 mm (0-peak) | |
| | 30-100 Hz | 40 g | |
| Y-direction | 5-30 Hz | 11 mm (0-peak) | |
| | 30-100 Hz | 25 g | |
| Z-direction | 5-30 Hz | 11 mm (0-peak) | |
| | 30-100 Hz | 25 g | |

4.7.1.4 Random Vibration

BSM-SSSD-R 79

Per AD 29 random vibration input is :

| Axis (S/C) | ramp up | Plateau | ramp down | g-rms |
|----------------------------------|---------------------|--|--------------------------------|------------|
| X <u>Launch direction</u> | +3 dB/oct 20-100 Hz | <u>0.185</u> g ² /Hz 100 - <u>350</u> Hz | -12 dB/oct <u>350</u> -2000 Hz | ~ <u>2</u> |
| Y <u>perpendicular to SOB</u> | +3 dB/oct 20-100 Hz | 0. <u>117</u> g ² /Hz 100 - <u>400</u> Hz | -12 dB/oct 400-2000 Hz | ~ <u>2</u> |
| Z <u>Sun pointing</u> | +3 dB/oct 20-100 Hz | 0. <u>117</u> g ² /Hz 100 - <u>300</u> Hz | -12 dB/oct 200-2000 Hz | ~ <u>2</u> |

Duration of qualification run 120 seconds.

4.7.1.5 Vacuum Level

| | |
|--|----------------------------------|
| BSM-SSSD-R 80 Less than 10^{-4} Pa | HR-SP-ATC-RID-05 |
|--|----------------------------------|

4.7.1.6 Vacuum Outgassing

| | |
|---|------|
| BSM-SSSD-R 81 Materials shall have a low outgassing rate with Total Mass Loss (TML) <1% and Volatile Condensable Material Loss (VCM) = 0.1% | AD22 |
|---|------|

4.7.1.7 Temperature

| | |
|---|-----|
| BSM-SSSD-R 82 The BSM shall perform within specification at the operational temperature cited in 4.2.2. In addition, the BSM will operate with reduced performance at temperatures from 4-300K. | RD1 |
|---|-----|

4.7.1.8 ~~Deleted (see §4.4.4) Magnetic Fields~~

4.7.1.9 Survival Temperature

| | |
|--|-----|
| BSM-SSSD-R 83 The BSM shall remain fully operational following exposure to temperatures of 80°C for periods of up to 72 hours. (bakeout) | AD1 |
|--|-----|

4.7.1.10 Radiation environment

| | |
|--|----------------------------|
| BSM-SSSD-R 84 The integrated dose for silicon behind 2 mm of aluminium is estimated at 12 kRad and behind 5 mm of aluminium as 3.5 kRad. These figures will be taken as the radiation tolerance for components in the warm electronics boxes and inside the cryostat respectively. | AD1 section 2.1.4.9 RD2 |
|--|----------------------------|

| BSM-SSSD-R 85 | | | | RD4 |
|--------------------------------------|----------|----------|----------|-----|
| Non-ionizing energy loss [MeV/g(Si)] | | | | |
| Shield thickness | 3 Years | 5 Years | 10 Years | |
| 2mm Aluminium | 1.83E+08 | 1.86E+08 | 2.62E+08 | |
| 5mm Aluminium | 7.57E+07 | 7.66E+07 | 1.03E+08 | |

| BSM-SSSD-R 86 | | | | RD4 |
|---|----------|----------|----------|-----|
| Total ionizing radiation dose in Si [rad] | | | | |
| Shield thickness | 3 Years | 5 Years | 10 Years | |
| 2mm Aluminium | 1.01E+04 | 1.04E+04 | 1.46E+04 | |



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| | | | | |
|---------------|----------|----------|----------|--|
| 5mm Aluminium | 3.79E+03 | 3.88E+03 | 5.11E+03 | |
|---------------|----------|----------|----------|--|

4.8 Verification requirements

The BSM Development Plan (AD15) contains more detail on the actual tests to be carried out on the BSM. The table below shows how each of the functional and operational requirements in this document is to be demonstrated, for each of the deliverable BSM models. The deliverable models include the STM (deliverable to RAL but not ESA), CQM, PFM, FS

Key:

| | | | |
|----------------|--|---|---|
| Test | | T | |
| Measurement | | M | |
| Analysis | , Reference to calculations and previous tests, assumption | | A |
| Inspection | | I | |
| Not Applicable | | X | |

Notes:

- The STM model [is to be](#) delivered as a fixed mass with a fixed mirror . The minimum requirements verification is specified accordingly.
- Tests and measurements are distinguished in that measurements are simple procedures e.g. to measure dimensions, mass etc. A test will in most cases include some combination of measurement devices, set up procedures, inspection, calibration, calculation, etc in order to demonstrate a requirement.

4.8.1 Performance Requirements

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-----------|------------------------------|-----|-----|-----|----|-------|
| 4.1.1 | Angular Travel - Chop Axis | X | T | T | T | |
| 4.1.2 | Angular Travel - Jiggle Axis | X | T | T | T | |
| 4.1.3 | Minimum Step Size | X | T | T | T | |
| 4.1.4 | Chop Frequency | X | T | T | T | |
| 0 | Jiggle Frequency | X | T | T | T | |
| 4.1.6 | Holding position | X | T | T | T | |
| 4.1.7 | Stability | X | T | T | T | |
| 4.1.8 | Position Measurement | X | T | T | T | |
| 4.1.9 | Settling Time | X | T | T | T | |
| 4.1.10 | Chop repeatability | X | T | T | T | |

4.8.2 System Requirements

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-------------------|---|---------|--------|--------|--------|---|
| 4.2.1 | Mechanical Dimensions | M | M | M | M | |
| 4.2.2 | Operating Temperature | T | T | T | T | |
| 0 | Thermal Isolation | T | T | T | T | |
| 4.2.4 | Cold Power Dissipation | X | T (a) | T | T | (a) Cold power dissipation of the CQM may not be compliant if non-space rated components are used for motor coils |
| 4.2.5 | Warm Electronics Power Dissipation | X | T | T | T | |
| 4.2.6 | Mirror Surface Dimensions | M (b) | M | M | M | (b) X if STM has no mirror |
| 4.2.7 | Mirror Surface Finish | I/M (c) | I/M | I/M | I/M | (c) X if STM has no mirror |
| 4.2.11 & 4.2.8 | Mirror Surface Reflectivity | A(d) | A | A | A | (d) X if STM has no mirror |
| 4.2.9 | Mirror Surface Emissivity | X | X | X | X | Complement of 4.2.11 & 4.2.8 |
| 4.2.10 | Baffle | X | M/T | M/T | M/T | Measurement will be against design drawings. Tests only performed on integration at RAL |
| 4.2.11 | Position of Rotation Axes | M/I (e) | M/I | M/I | M/I | (e) X if STM has no mirror |
| 4.2.12 | Orthogonality of Rotation Axes | X | T | T | T | |
| 4.2.13 | Fail Safe (No Drive Signal) Position | X | T/A(f) | T/A(f) | T/A(f) | (f) May require supporting analysis of rest position in 1 g field is not (0,0) |
| 4.2.14 | Fail Safe (Mechanical Failure) Position | X | X | T/A(g) | T/A(g) | (g) Demonstrated on tests on QM or DM |
| 4.2.15 | Mass | M | M | M | M | |
| 4.2.16 | Cool-down time | T | T | T | T | Cooldown times will be dependent on cryostat configuration. |

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-----------|---------------|-----|-----|------|------|---|
| 4.2.17 | Reliability | X | X | A(h) | A(h) | (h) demonstrated by QM programme and by design/analysis |
| 4.2.18 | Failure Modes | X | X | A(j) | A(j) | (j) demonstrated by QM programme and by design/analysis |

4.8.3 Operational Specification

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-----------|-------------------------|-----|------|------|------|---|
| 4.3.1 | Operational Safety | A | A | A | A | Demonstrated by analysis/design/risk assessment |
| 4.3.2 | Lifetime | X | X | A(k) | A(k) | (k) demonstrated by QM programme |
| 4.3.3 | Operating modes | X | T(l) | T | T | (l) CQM will not have redundant modes |
| 4.3.4 | Jiggle Mode | X | T | T | T | |
| 4.3.5 | Chopping Mode | X | T | T | T | |
| 4.3.6 | Scan mapping | X | X | X | X | Only applicable on spacecraft |
| 4.3.7 | Stare or 'holding' mode | X | T | T | T | |
| 4.3.8 | Degraded modes | X | T | T | T | |
| 4.3.9 | Combinations of Modes | X | T | T | T | |

4.8.4 Interface requirements

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-----------|--------------------------------|-------|-------|-------|-------|---|
| 4.4.1 | Data Outputs | X | T | T | T | Fully demonstrated only on integration at LAM/ RAL . ATC tests will demonstrate compliance to ICD |
| 4.4.2 | Data Inputs | X | T | T | T | Fully demonstrated only on integration at LAM/ RAL . ATC tests will demonstrate compliance to ICD |
| 4.4.3 | Exported vibration | X | T | T | T | On integration to SPIRE at RAL |
| 4.4.4 | Stray Magnetic fields | X | T | T | T | On integration to SPIRE at RAL |
| 4.4.5 | Electro-Magnetic Compatibility | X | A/T | T | T | On integration to SPIRE at RAL |
| 4.4.6 | ICD's | I/M/T | I/M/T | I/M/T | I/M/T | |

4.8.5 Design, manufacture and test requirements

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-----------|-------------------------|------|-----|-----|----|---|
| 4.6.1 | Design requirements | A | A | A | A | Compliance indicated in ADP |
| 4.6.2 | Electronics Card Format | X | I | I | I | Inspection of LAM deliverables |
| 4.6.3.1 | Mirror Flatness | M(m) | M | M | M | (m) X if STM has no mirror |
| 4.6.3.2 | Mirror Reflectivity | A(n) | A | A | A | (n) X if STM has no mirror |
| 4.6.3.3 | Cleanliness | I | I | I | I | Compliance indicated in ADP |
| 4.6.3.4 | Material selection | I | I | I | I | Compliance indicated in ADP |
| 4.6.3.5 | Storage | A | A | A | A | Compliance indicated in ADP |

4.8.6 Environmental requirements

| Reference | Requirement | STM | CQM | PFM | FS | Notes |
|-----------|--|-----|-----|------|------|--|
| 4.7.1.1 | Shock | X | X | X | X | No requirement |
| 4.7.1.2 | Quasi Static Loads | T | X | A(o) | A(o) | (o) demonstrated by QM programme |
| 4.7.1.3 | <u>Per AD29 Static is now reduced from 40 g to 25 g in any direction</u> Sine Vibration | T | X | A(p) | A(p) | (p) demonstrated by QM programme |
| 4.7.1.4 | Random Vibration | T | X | A(q) | A(q) | (q) demonstrated by QM programme |
| 4.7.1.5 | Vacuum Level | T | T | T | T | |
| 4.7.1.6 | Vacuum Outgassing | A | A | A | A | Demonstrated via materials selection and Compliance indicated in ADP |
| 4.7.1.7 | Temperature | T | T | T | T | |
| 4.7.1.8 | <u>Deleted (see §4.4.4)</u> | X | TBD | TBD | TBD | EMC tests performed when integrated at RAL. Tests deleted from ATC plan |
| 4.7.1.9 | Survival Temperature | T | T | T | T | <u>Demonstrated by bakeout at ATC in the course of assembly & test</u> |
| 4.7.1.10 | Radiation environment | X | X | TBD | TBD | EMC tests performed when integrated at RAL. Tests TBD |



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